Drainage Strategy Richmond-upon-Thames College - Sports Centre 5141939-REP-002

12 May 2017

# Notice

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This document has 17 pages including the cover.

### **Document history**

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# 1. Introduction

This statement has been prepared with the purpose of supporting the Reserve Matters Applications of the Outline Planning Application for the Richmond-upon-Thames College Phase 2 Sports Centre Development.

This document is supported by the following additional documentation:

- Soiltechnics Ground Investigation Report (Rev 01, 2008)
- Soiltechnics Ground Investigation Report (Rev 02, 2015)
- CSI Sustainable Drainage Assessment (June 2015)

The redevelopment of Richmond upon Thames College is being undertaken in three phases. Phase 2 Sports Centre refers to the Sports Centre building and adjacent car park. A Reserve Matters Application has previously been submitted for the Phase 1 development of Richmond upon Thames College. Phase 1 refers to the College building refer to 5137894-ATK-00-XX-DR-C-0301 for clarification of phasing areas.

# 2. Existing Drainage

## 2.1. Existing Foul Water

The existing foul water discharge network servicing the existing Richmond-upon-Thames College (College) on site is split into two sections. The discharge collected from the western portion of the site incorporates several pumping stations and rising mains for the eventual discharge via gravity main into the Thames Water network on Craneford Way. This network also collects discharge from the neighbouring Nuffield Health Fitness & Wellbeing Centre.

The discharge collected from the eastern portion of the existing college is conveyed via a gravity fed system for discharge in two locations to the Thames Water network along the southern end of Egerton Road.

## 2.2. Existing Surface Water

The existing College site utilises infiltration and soakaway techniques to manage the surface water generated by rainfall events and directs them to the local secondary aquifer within the Kempton Park gravel strata. While no official surface water connections have been recorded from the site, on inspection of the network there is evidence of several soakaways overflowing into the foul network on a regular basis. This is more evident in the southern site area.

The groundwater level on site has been monitored and within the Phase 2 Sports Centre development boundary has been recorded to be at depths ranging from 7.92 to 8.40 m AOD (approximately 1.3 to 0.65m below existing ground level).

Existing soakaways local to the Phase 2 Sports Centre boundary have been surveyed and have recorded sump levels of between 6.53 m AOD and 6.46 m AOD. As such it is expected that the existing soakaways are permanently submerged in groundwater. This was confirmed via visual inspection of the network.

Furthermore, groundwater flooding has been observed in the foul water rising main chambers within the Phase 2 Sports Centre boundary.

# 3. Proposed Drainage

Surface and foul water have been proposed to drain as per the layouts provided in Appendix A. Relevant design calculations have been included for reference in Appendix B.

## 3.1. Proposed Foul Water

### 3.1.1. Phase 2 Sports Centre Strategy

The foul water is expected to discharge from the Phase 2 Sports site at a calculated peak flow of 6.2 l/s. The shallow invert level of the local Thames Water foul sewer network (990 mm cover below road level) has necessitated a gravity fed/pumping solution to discharge the foul water.

The discharge will be conveyed via gravity to a new pumping station. Capacity has been allowed within the network and pumping station for flows collected from the Sports Centre, College, STEM, Haymarket, Nuffield Health Centre (neighbour) and a portion of the Residential Development (79 units).

A design flow from the combined developments of 25.7I/s has been conservatively estimated. This is a small increase over what is expected to be the current discharge rate (20.2 I/s) through the connection in Craneford Way. Due to the shallow depth of the Thames Water sewer, a pressurised rising main will then transport the foul water southwards for eventual discharge into the Thames Water sewer network, utilising the existing gravity connection on Craneford Road.

The foul water network was designed and modelled using Micro Drainage in compliance with BS EN 752 (2008) and Sewers for Adoption (7<sup>th</sup> edition) minimum gradients to achieve acceptable self-cleansing flow velocities.

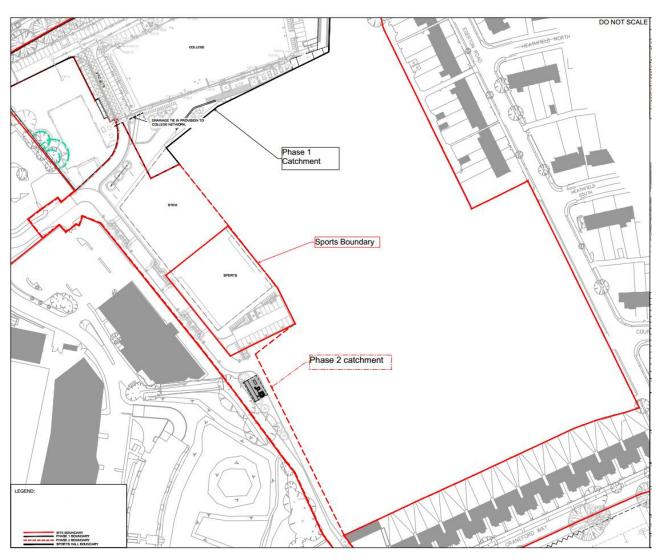
The foul pumping station will be located just to the south of the Sports Centre carpark and will be put forward for adoption by Thames Water along with the downstream rising main. The pumping station and downstream discharge network will be installed/constructed during Phase 1, together with the main private collection network within the access road to the west of the Sports Centre. This is to manage foul water discharge from the new College building, and Nuffield Health Centre buildings that have been established in Phase 1.

All design and emergency storage requirements will comply with Sewers for Adoption (7<sup>th</sup> edition).

## 3.2. Proposed Surface Water

### 3.2.1. Site Wide Drainage and Surface Water Management

An overarching sustainable drainage assessment and strategy was prepared by CSI (June 2015). Phase 2 specific updates resulting from the detailed design have been included within this document.



#### Figure 3-1 Catchment Areas

### 3.2.2. External areas

During exploratory investigations on site (Soiltechnics, 2008 & 2015), Kempton Park Gravel (sand and gravel) was encountered within the Phase 2 Sports Centre boundary between 0.44 to 0.95 m below existing ground level. Infiltration testing was undertaken at the approximate permeable pavement depth of 600 mm (Soiltechnics 2015) to confirm the infiltration rate at subgrade level. The infiltration rate recorded as being 8.4 x  $10^{-7}$  m/s. As such no infiltration (Type C) is proposed in accordance with CIRIA SuDS Manual C753.

Groundwater infiltration as a form of surface water discharge was furthermore discounted due to a high groundwater level recorded within the Phase 2 boundary. Levels were recorded to be as shallow as 8.40 m AOD (0.622 m below proposed ground level) within the Phase 2 Sports Centre development boundary. With a minimum finished level in the Sports Centre Carpark of 9.02 m AOD, insufficient freeboard can be achieved between the base of the infiltration system and the recorded seasonal ground water high.

In others areas on site, specifically Phase 1 boundary, permeable paving has been deemed a viable surface water management solution due to favourable groundwater levels and infiltration rates. But within the Phase 2 sports centre boundary, the design is constrained by the higher groundwater level, and borderline infiltration results.

Consequently, all external surfaces within the Sports Centre development boundary will be impermeable. The runoff will be collected from external areas via a series of gullies tailored to the site features and

constraints. All surfaces have been designed to transfer surface water laterally into the adjacent gullies. Runoff collected by the gullies will be retained in the shared attenuation tank, then conveyed by the surface water pipe network installed in Phase 1 to the Thames Water sewer.

For information, the Phase 1 attenuation tank has been sized to accommodate all the run-off within the Phase 2 Sports Centre development boundary. The attenuation tank is 450 m<sup>3</sup>, and will be located beneath the Haymarket/College car park. In line with the recommendations by the Environment Agency (Sustainable Drainage assessment, ESI June 2015), the proposed total discharge from the site will be restricted to the Greenfield runoff. In previous assessments, a SOIL type of 1 (SPR 0.1) has been assumed giving a Qbar rural of 0.14 I/s/ha (IH124 method). However, it is best practice (and as recommended in CIRIA C753) when permeable soil types are encountered to assume a minimum discharge of 5 I/s. This is because when using flow control devices it is not practical to restrict the control to a discharge rate below this value. As such for the 2.04 ha area (see Figure 3-1 for the assumed extent) a discharge rate of 5 I/s has been applied for all storm events. The Phase 2 development contributes 0.85 ha to this.

Due to restrictive shallow levels on the external Thames Water surface water network (approximately 500 mm cover depth at proposed connection), a small submersible lifting chamber will be installed near the northern property boundary, to pump surface water up so that it can fall via gravity to the Thames Water network. Emergency storage requirements will be facilitated via the attenuation tank and will be agreed with the appointed Building Regulations Inspector. A pump failure (i.e. no outflow) in a 100 year event + 30 % climate change has been analysed in MicroDrainage. In a 24 hour storm the entire runoff volume can be attenuated resulting in minimal flooding across the site. It has been reasonably assumed that the pump will be able to be replaced within a 24 hour period.

#### 3.2.3. Roof runoff collection network

Runoff from roofs will be collected from the building rainwater downpipes (RWP) via the central surface water network, and conveyed to the shared attenuation tank before being discharged into the northern Thames Water network. This will help reduce both the long-term volumetric run-off and the peak discharge rate during short duration events.

Green roofs are being utilised on the Phase 2 Sports building as a part of the sustainable drainage and ecological enhancement strategies for the project. It is proposed that 70% of the available roof area will comprise of green roof. All other roof area is taken up by essential plant equipment (ventilation, vents, roof lights and the roof access hatch with additional space required for maintenance of these structures). Inside the parapet, this comprises 20% of the total roof area.

The green roof will comprise of an interlocking modular system containing pre-grown plants in a substrate with a depth of 80 mm. This will help reduce both the long-term volumetric run-off and the peak discharge rate during short duration rainfall events. The effects of the green roof have not been modelled when considering the 30 and 100 year events (+climate change respectively) as per the guidance in CIRIA C753.

#### 3.2.4. Management of discharge to controlled waters

Impermeable paving has been proposed within the Phase 2 Sports boundary for the car park and surrounding external areas. In accordance with industry best practice, Pollution Prevention Guidelines 3 (PPG3) indicates trapped gully pots can provide adequate protection for car parks that are too small to justify the installation of a separate, but they must be properly maintained. It should be noted the PPG3 has now been withdrawn however it remains industry best practice.

The policy PPG3 also defines the different sites that need to have measures in place to prevent polluting the environment – "*car parks typically larger than 800m*<sup>2</sup> *in area or for 50 or more car parking spaces*".

The car park within the Sports Centre development boundary is 435m<sup>2</sup> with less than 50 car parking spaces which would conclude a petrol interceptor is not required for this area of the site.

The CIRIA SuDS Manual 2015 (C753) - Table 26.2 also discusses the pollution hazard indices for different land use classifications, this table rates the pollution from non -residential car parking and infrequent change (e.g. school's offices < 300 traffic movement/day as a low pollution hazard level.

Further detail of the drainage design of future phases will be provided in the submission for the relevant phase.

# 4. Flood Risk and Mitigation

## 4.1. General

The Richmond-upon-Thames College Phase 2 Sports Centre development is located within Flood Zone 1 (similar to the neighbouring LBRuT Borough School development). It is acknowledged that the playing fields (located far south of the Phase 2 development) are within Flood Zone 2. Refer Appendix D1.

## 4.2. Sources of Flooding

The design has been strategised and undertaken in accordance with the National Planning Policy Framework (NPPF), Regional Planning Policy and Flood Risk Assessment (FRA), LBRuT Strategic FRA (March 2016), and local policy. The parameters assumed in the design have been described above in Sections 3.1 and 3.2 however key points include:

- Maximisation of an infiltration discharge solution
- Integrated SuDS features
- Discharge offsite restricted to greenfield
- No flooding in 100 year + 30% CC

On review of the sources of flood risk that may affect the site, the Flood Maps sourced from the Environment Agency and from within the LBRuT Strategic Flood Risk Assessment have been referenced. A compilation of maps have been appended to this report (Appendix D) however in summary the flood risk presented to the site is as follows:

SOURCE OF FLOODING	RISK	MITIGATION	REFERENCES
Tidal and Fluvial	Very Low – Flood Zone 1.	Implementation of a formalised drainage system in Phase 2 will improve drainage and mitigate risk.	Appendix D2
Surface Water	Mostly low risk flooding	Implementation of a formalised drainage system in Phase 2 will improve drainage and mitigate risk.	Section 3.2.2, 3.2.4 Appendix D3
		Network has been designed so that there is no resultant flooding in a 1 in 100 year event (+30% CC).	
Sewer	No flooding recorded on 2011 map Minimal incidents recorded 2011-2015	Implementation of a formalised drainage system in Phase 2 will improve drainage and mitigate risk. Thames Water have confirmed that the development will have negligible impact on their sewer network	Section 3.2.2, 3.2.4 Appendix D4 Section 5 Appendix E
Groundwater	LBRuT Maps show potential for flooding to occur. Seasonal groundwater monitoring has been undertaken within the vicinity of the Phase 2 development zone. This recorded a groundwater high level of	Non-infiltration system is to be implemented as an appropriate freeboard could not be achieved and ground parameters are less favourable towards an infiltration solution within the development boundary	Section 3.2.3, 3.2.5 Appendix D5

	1.04m below existing ground level 8.8m AOD.	
Reservoir	Nil	Appendix D6

## 4.3. Interaction with neighbouring developments

As aforementioned the critical 100 year event plus climate changes is to be attenuated within the development without flooding. In higher intensity storm events, Phase 2 site contours have been developed to direct the overland flow path away from all site buildings and key infrastructure into areas which do not create risk to people or property.

In terms of the Sports Pitches located to the far south of the site (and within Flood Zone 2); this area of the site is much lower than the proposed development and as such, given the improvements and formalisation of the drainage in Phase 2, the development will have nil effect on the southern site other than to improve flood risk through the reducing the overland flow.

An appropriate FRA will be submitted for this area when required.

## 4.4. Correspondence with LBRuT

As agreed with LBRuT asset coordinator Brian Humphries (refer to the correspondence attached in Appendix C), it is understood that the content within this strategy document is sufficient to close out any queries regarding flood risk and as such a formal Flood Risk Assessment is not required for Phase 2 of the Richmond-upon-Thames College development.

# 5. Thames Water Consultation

Where discharge into external sewer networks are proposed, Thames Water (has been consulted through the predevelopment enquiry process. At the time of the enquiry Thames Water has confirmed that no impact study is required for the foul water but have requested additional information to confirm that all other methods of disposal have been considered before they will accept discharge into their surface water network. This Drainage Strategy document is intended to inform this decision.

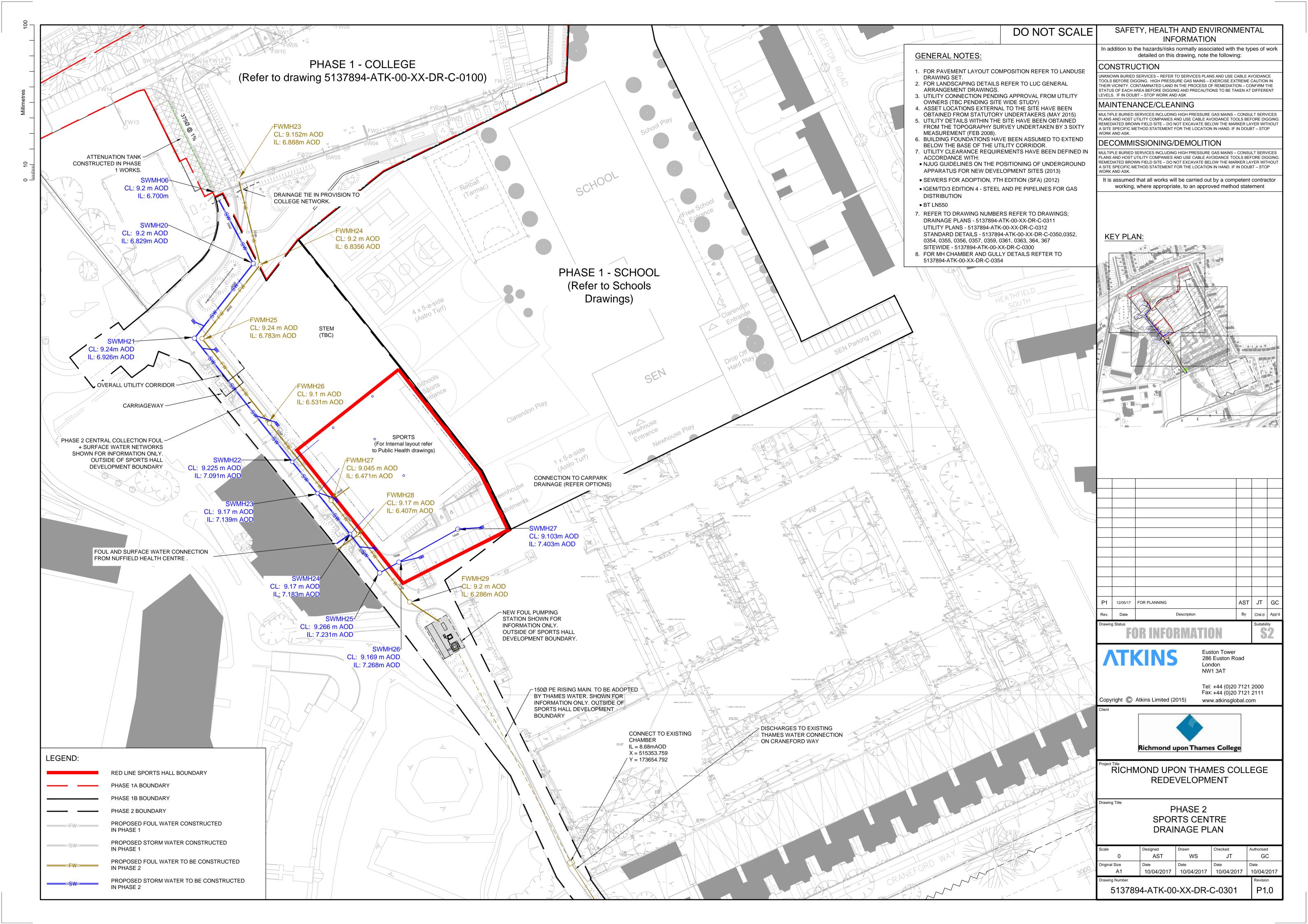
This letter has been appended to this document in Appendix E for reference.

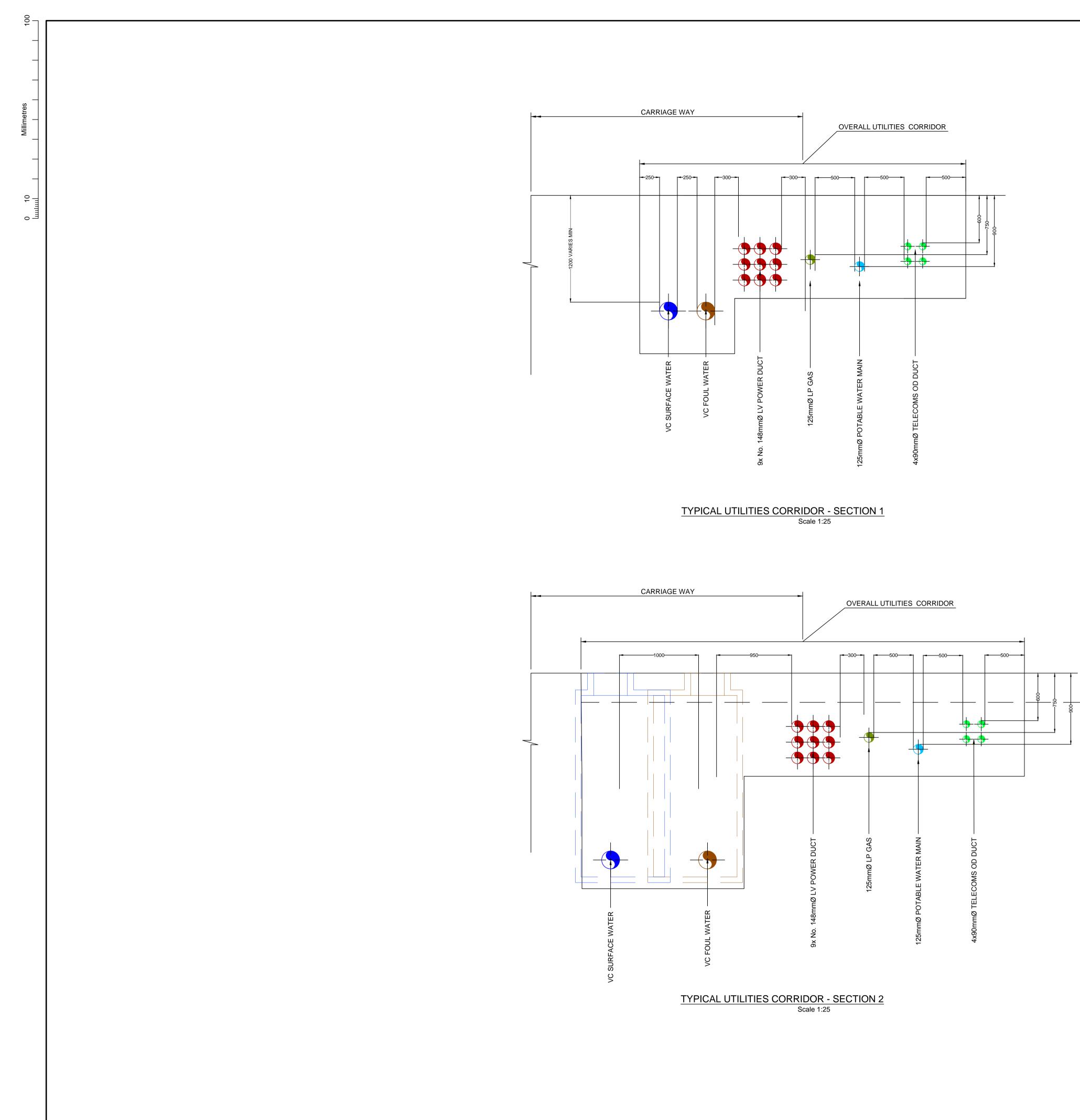
# Appendices



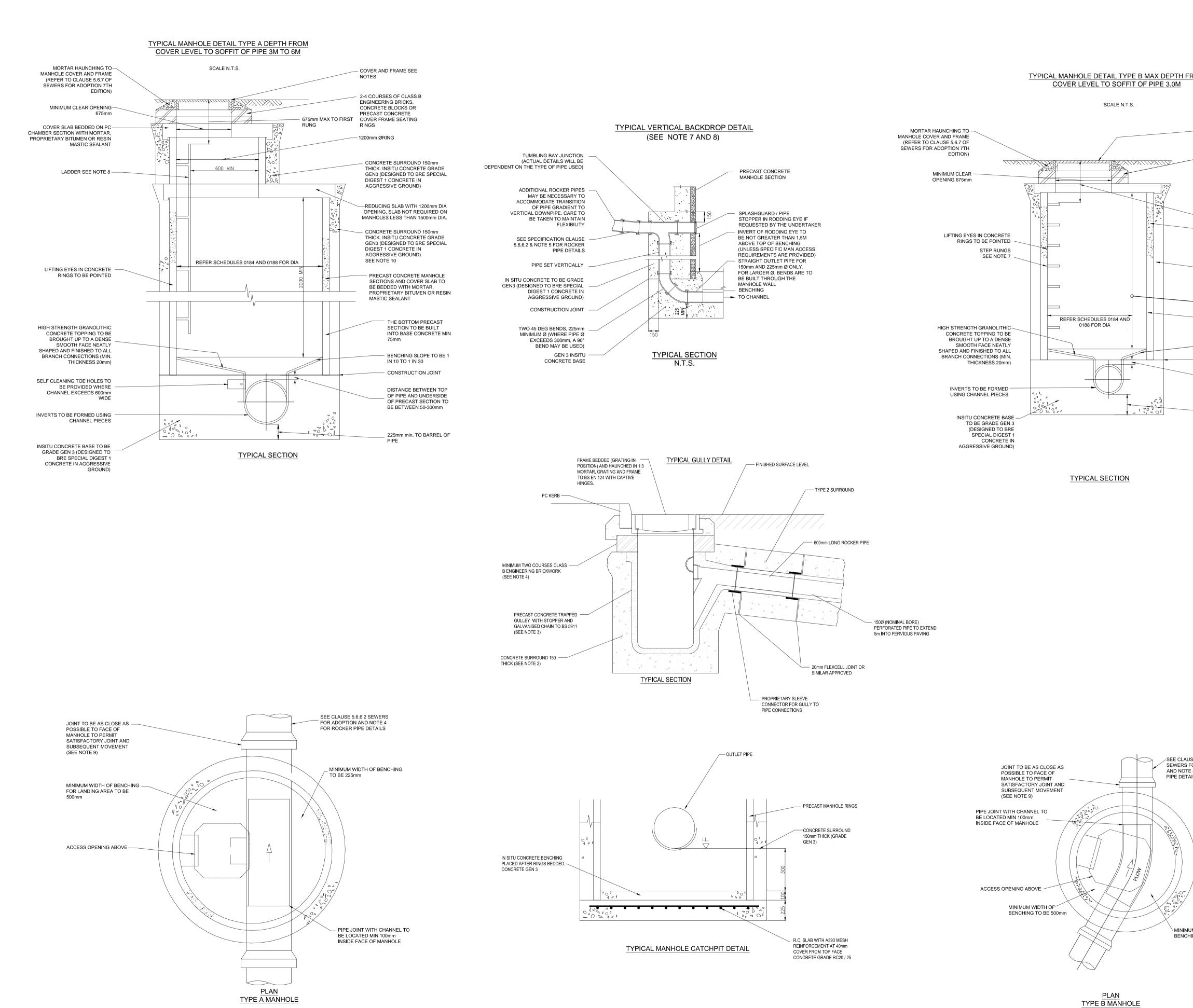
# Appendix A. Stage D Drainage Drawings

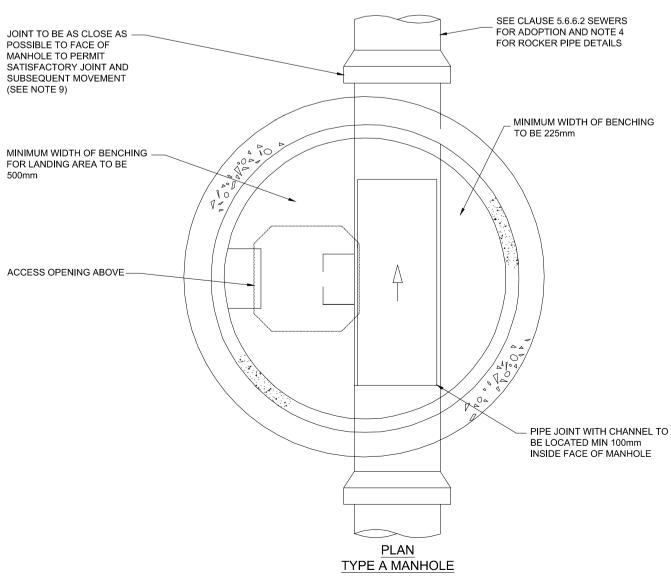
Document Number	Document Title
5137894-ATK-00-XX-DR-C-0301	Sports Centre Drainage Plan Reserve Matters
5137894-ATK-00-XX-DR-C-0350	Utility Corridor Typical Cross Sections
5137894-ATK-00-XX-DR-C-0354	Foul and Surface Water Drainage Manhole Details
5137894-ATK-00-XX-DR-C-0355	Foul and Surface Water Drainage Typical Pipe Bedding Details



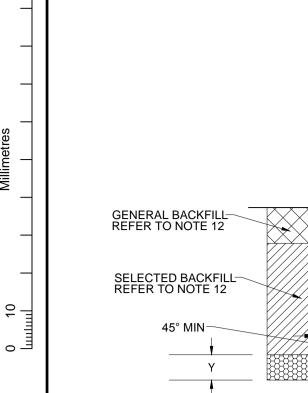


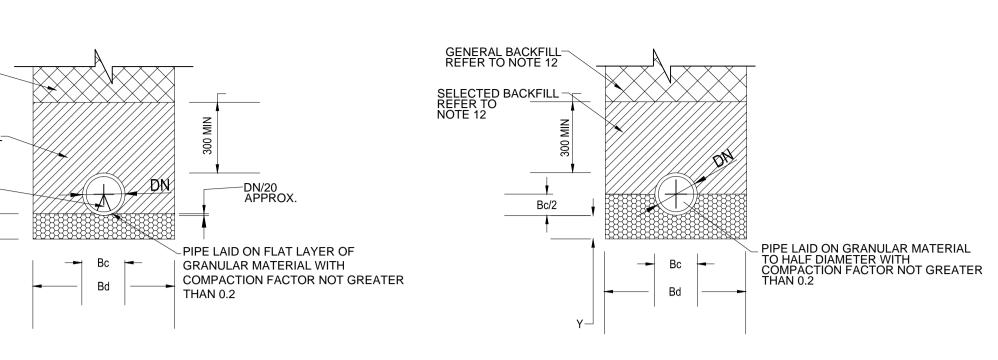
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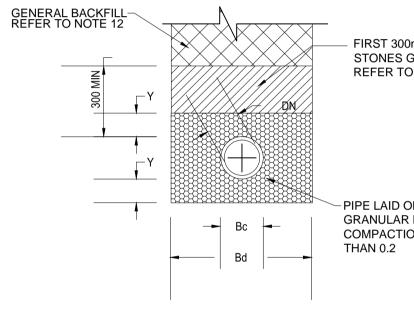
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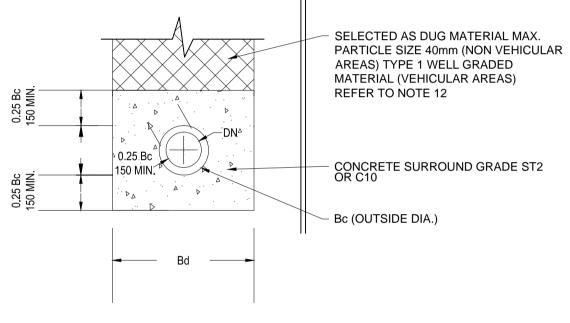
## TYPICAL PIPE BEDDING - CLASS F

## TYPICAL PIPE BEDDING - CLASS B



FIRST 300mm BACKFILL FREE FROM STONES GREATER THAN 40mm REFER TO NOTE 12

- PIPE LAID ON FLAT LAYER OF GRANULAR MATERIAL WITH COMPACTION FACTOR NOT GREATER



NOTE:- THE FLEXIBILITY OF PIPELINE SURROUNDED WITH CONCRETE SHOULD BE MAINTAINED BY THE PROVISION OF FLEXIBLE CONSTRUCTION JOINTS THROUGH THE CONCRETE AT EACH PIPE JOINT. THESE SHOULD BE MADE FROM BITUMEN IMPREGNATED INSULATING BOARD COMPLYING WITH BS 1142: 1989 OR OTHER EQUALLY COMPRESSIBLE MATERIAL

## TYPICAL PIPE BEDDING - CLASS S

## TYPICAL PIPE BEDDING UNREINFORCED CONCRETE SURROUND CLASS Z1

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Class B	2.5	1.9	5.5 - 10.0	5.0 - 10.0	4.0 - 7.0	2.5 - 10.0	2.6 - 4.5	2.3 - 4.2	1.2 - 3.9	2.4 - 4.5	1.2 - 4.3	1.2 - 4.5	1.9 - 4.5	1.9 - 3.8	1.
Class F	1.9	1.5	*1.2 - 5.5	*1.2 - 5.0	*1.2 - 4.0	*1.2 - 2.5	*1.2 - 2.6	*1.2 - 2.3	-	*1.2 - 2.4	1-	-	*1.2 - 1.9	*1.2 - 1.9	*1
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Class B	2.5	1.9	5.9 - 10.0	3.5 - 10.0	5.5 - 8.0	3.7 - 10.0	3.6 - 5.0	3.3 - 4.7	3.0 - 4.5	3.3 - 5.0	3.3 - 5.0	3.3 - 5.0	3.4 - 4.7	3.4 - 4.7	3.
Class F	1.9	1.5	0.65 - 5.9	0.65 - 3.5	0.65 - 5.5	0.65 - 3.7	0.65 - 3.6	0.8 - 3.3	0.8 - 3.0	0.8 - 3.3	0.8 - 3.3	0.8 - 3.3	0.6 - 3.4	0.6 - 3.4	0.
Class B	-	1.9	-	-	12	-	120 C	0.6 - 0.8	0.6 - 0.8	0.6 - 0.8	0.6 - 0.8	0.6 - 0.8	-	-	
Class Z1	Protecti	on (4.5)	< 0.6	< 0.6	< 0.6	< 0.6	< <mark>0.6</mark>	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< <mark>0.6</mark>	4
			1												
Wide Trench (ie															-
	Nominal		150	225	300	400	/375	450	525	600	675	750	825	900	10
	Material /		Vitrifie d	Vitrifie d	Vitrified	Vitrified	Concrete	Concrete	Concrete	Concrete	Reinforced	Reinforced	Reinforced	Reinforced	Rein
Bedding Type	Bedding	Factor	Clay	Clay	Clay	Clay	SC120	SC120	SC120	SC120	Concrete	Concrete	Concrete	Concrete	Co
Location:-	VC	Concrete	40KN/m	45KN/m	72KN/m	64KN/m					SC120	SC120	SC120	SC120	S
Trafficked / Pav	ved Areas						For depths of	f cover exce	eding 7.0m re	fer to Narrow	Trench sche	dule above			
Class Z1	4.5	4.5	-	-	-	-	4.0 - 7.0	4.5 - 7.0	4.7 - 7.0	4.6 - 7.0	3.9 - 7.0	4.0 - 7.0	4.2 - 7.0	4.2 - 7.0	4.
Class S	2.5	2.2	-	-		-	3.0 - 4.0	3.7 - 4.5	3.8 - 4.7	3.6 - 4.6	2.9 - 3.9	3.1 - 4.0	3.3 - 4.2	3.3 - 4.2	3.
Class B	2.5	1.9	5.5 - 7.0	5.0 - 7.0	4.0 - 7.0	<mark>6.0 - 7.0</mark>	1.2 - 3.0	2.0 - 3.7	1.2 - 3.8	2.2 - 3.6	1.2 - 2.9	1.2 - 3.1	1.2 - 3.3	1.9 - 3.3	2.
Class F	1.9	1.5	*1. <mark>2 - 5.5</mark>	*1.2 - 5.0	*1.2 - 4.0	*1.2 - 6.0	-	*1.2 - 2.0	-	*1.2 - 2.2	-	-	-	*1.2 - 1.9	*1.
Class Z1	Protecti	on (4.5)					-	1 2m for Bac	k of House ar	d <0.9m for	Front of House	& Concourse	Areas		

### TABLE A

BEDDING MATERIAL					
NOMINAL PIPE DIAMETER mm	SINGLE SIZE GRANULAR BEDDING MATERIAL mm	GRADED GRANULAR MATERIAL mm			
150	10,14	14 TO 5			
225 - 300	10, 14 OR 20	14 TO 5, 20 TO 5			
375 - 525	14, 20	14 TO 5, 20 TO 5			
OVER 525	14, 20, 40	14 TO 5, 20 TO 5, 40 TO 5			

TABLE B	
SELECT	ED FILL
NOMINAL PIPE DIAMETER mm	MAXIMUM STONE SIZE mm
150	15
200 - 525	20
OVER 525	40

TABLE C				
DN/Ø	Вс			
150/160	210			
225/200	300			
300	375			
375/400	490			
450	575			
525	670			
600	775			
675	815			
750	905			
825	985			
900	1070			
1050	1265			
1200	1430			
1350	1615			
1500	1745			
1600	1910			
1800	2090			

1050	1200	1400
einforced concrete SC120	Reinforced Concrete SC120	Reinforced Concrete SC120
5.5 - 10.0	5.6 - 10.0	5.6 - 9.0
4.1 - 5.5	4.1 - 5.6	4.1 - 5.6
1.9 - 4.1	2.0 - 4.1	2.0 - 4.1
1.2 - 1.9	*1.2 - 2.0	*1.2 - 2.0
7.0 - 10.0	7.0 - 10.0	7.0 - 10.0
4.9 - 7.0	5.0 - 7.0	5.0 - 7.0
3.4 - 4.9	3.5 - 5.0	3.5 - 5.0
0.6 - 3.4	0.6 - 3.5	0.6 - 3.5
-	-	-
< 0.6	< 0.6	< 0.6

mao monon (it																	
	Nominal	Diameter	150	225	300	400	/375	450	525	600	675	750	825	900	1050	1200	1400
		/strength	Vitrified	Vitrifie d	Vitrified	Vitrified	Concrete	Concrete	Concrete	Concrete		Reinforced			And the second second second second	Reinforced	and a second second second second
Bedding Type		g Factor	Clay	Clay	Clay	Clay	SC120	SC120	SC120	SC120	Concrete	Concrete	Concrete	Concrete	Concrete	Concrete	Concrete
Location:-	VC	Concrete	40KN/m	45KN/m	72KN/m	64KN/m					SC120	SC120	SC120	SC120	SC120	SC120	SC120
Trafficked / Pav	ved Areas		For depths of cover exceeding 7.0m refer to Narrow Trench schedule above														
Class Z1	4.5	4.5	-	-		-	4.0 - 7.0	4.5 - 7.0	4.7 - 7.0	4.6 - 7.0	3.9 - 7.0	4.0 - 7.0	4.2 - 7.0	4.2 - 7.0	4.2 - 7.0	<b>4.1 - 7.0</b>	5.0 - 7.0
Class S	2.5	2.2	-	-		Η.	3.0 - 4.0	3.7 - 4.5	3.8 - 4.7	3.6 - 4.6	2.9 - 3.9	3.1 - 4.0	3.3 - 4.2	3.3 - 4.2	3.3 - 4.2	3.2 - 4.1	4.0 - 5.0
Class B	2.5	1.9	5.5 - 7.0	5.0 - 7.0	4.0 - 7.0	<u>6.0 - 7.0</u>	1.2 - <mark>3.</mark> 0	2.0 - 3.7	1.2 - 3.8	2.2 - 3.6	1.2 - 2.9	1.2 - 3.1	1.2 - 3.3	1.9 - 3.3	2.0 - 3.3	2.0 - 3.2	2.0 -4.0
Class F	1.9	1.5	*1.2 - 5.5	*1.2 - 5.0	*1.2 - 4.0	*1.2 - 6.0	-	*1.2 - 2.0	-	*1.2 - 2.2	-	-	-	*1.2 - 1.9	*1.2 - 2.0	*1.2 - 2.0	*1.2 - 2.0
Class Z1	Protect	tion (4.5)		< 1.2m for Back of House and <0.9m for Front of House & Concourse Areas													
Un-Paved / Lan	dscape Are	as					For depths o	f cover exce	eding 7.0m re	fer to Narrow	Trench sche	dule above					
Class Z1	4.5	4.5	H	-	-	-	5.0 - 7.0	4.9 - 7.0	5.0 - 7.0	5.0 - 7.0	4.4 - 7.0	4.5 - 7.0	4.6 - 7.0	4.6 - 7.0	4.7 - 7.0	4.6 - 7.0	6.0 - 7.0
Class S	2.5	2.2	-	-	-	-	4.0 - 5.0	4.0 - 4.9	4.0 - 5.0	4.0 - 5.0	3.7 - 4.4	3.8 - 4.5	3.9 - 4.6	3.9 - 4.6	4.0 - 4.7	3.9 - 4.6	5.0 - 6.0
Class B	2.5	1.9	5.9 - 7.0	3.5 - 7.0	5.5 - 7.0	3.7 - 7.0	3.0 - 4.0	3.0 - 4.0	3.0 - 4.0	3.0 - 4.0	2.8 - 3.7	2.9 - 3.8	3.0 - 3.9	3.0 - 3.9	3.0 - 4.0	3.0 - 3.9	3.0 - 5.0
Class F	1.9	1.5	0.65 - 5.9	0.65 - 3.5	0.65 - 5.5	0.65 - 3.7	0.65 - 3.0	0.8 - 3.0	0.8 - 3.0	0.8 - 3.0	0.8 - 2.8	0.8 - 2.9	0.8 - 3.0	0.8 - 3.0	0.6 - 3.0	0.6 - 3.0	0.6 - 3.0
Class B	-	1.9	-	-	<b>1</b> -	-	-	0.6 - 0.8	0.6 - 0.8	0.6 - 0.8	0.6 - 0.8	0.6 - 0.8	0.6 - 0.8	0.6 - 0.8	-	-	-
Class Z1	Protect	tion (4.5)	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6

												CALE		SAFET	Y, HEALTH	H AND EN	IVIRONMEN	ITAL	
													In ad		e hazards/risks		ociated with the t	/pes of	work
												_	CON		detailed on this	drawing, note	e the following:		
												E	BURIED PLANS A	SERVICES INC	CLUDING POSSIBIL LE AVOIDANCE TOO	OLS BEFORE DIG			
												1	MATERI. POSSIBI	IALS. ILITY OF UNEX			NCLUDING ASBESTO H DURING GROUND V		NING
												-				NING			
													AND FO		VHEN EXCAVATING		IS, USE CABLE AVOID	ANCE TO	OLS
												-	DEC	OMMIS	SIONING/I				
												T L	MULTIPI USE CAI	LE BURIED SE		SERVICES PLAN	IS, HOST UTILITY CO	/IPANIES /	AND
																	ut by a competer oved method sta		
												1	2. ALL MAT	_ BEDDING DIN TERIALS ARE E	ENCOUNTERED SE	R UNIFORM SOIL.	WHERE ROCK OR AF ADVICE ON INCREA	TIFICIAL I SE TO 'Y'	HARD
												3	3. NOT DN -	IENSIONS IN TATION: - BORE OF PIP	Έ				
													Bd - Y - E	- TRENCH WID BEDDING DEPT	METER OF PIPE BA TH TH (NO PACKING IS LEVEL OF PIPE). T	TO BE			
													SHC	OWS MINIMUM ERE A MINIMU	'Y' EXCEPT UNDER M OF 50mm APPLIE CEED A MAXIMUM (	R SOCKETS S. NOTE THAT			
												4			AND PIPE STRENG <sup>-</sup> CLAY, CONCRETE #		ON HEPWORTH OR E STIC PIPE.	QUAL PIPI	E
												Ę	DIM	IENSIONS SHA		ANCE WITH TABL	H BS EN 13242 AND E E D, BASED ON COVE IDTH.		
												e	6. TRE UNL	ENCH WIDTH (TLESS CONSTR	TABLE D) SHALL GE UCTION COMPLEXI	ENERALLY BE CC	NSTRUCTED 'NARRO HERWISE. IN PARTIC	ULAR, WH	
												7	BED 7. GEN	DDING REQUIR NERAL BACKFI	REMENTS SHALL BE ILL;	E PROVIDED.	G A TRENCH, 'WIDE T		600
													SEF NOM	RIES. IT SHALL MINAL.	BE FREE FROM LU	JMPS OF CLAY O	R STONES GREATER	THAN 40m	
												7	7.3 ELS	SEWHERE, GEN	REQUIREMENTS FO	HALL BE CLASS 8	3.		750
												٤ د	SHA	ALL BE FURTH	ER RESTRICTED IN	I ACCORDANCE \	CEPT THE MAXIMUM WITH TABLE B. GGED TRENCHES, WA		
												Ň	MEN	MBRANE TO CO	OMPLY WITH BS 81 ITH MANUFACTURE	02, SHW CLAUSE ERS INSTRUCTIO	514 x 514 AND TO BE NS. MEMBRANE SHAL ALL ALSO BE USED A	INSTALLI L BE	ED IN
												1	10. PIPI				ND 225mm DIA PIPES mm.	AND CON	ICRETE
	NGINEER'S ADVICE HOULD BE SOUGHT IF	-																	
P	ERCHED WATER IS NCOUNTERED						-	TABLE C											
							-	DN/Ø	Вс	Bd Y	OTE 3								
				TABLE B				150/160 225/200 300	210 300 375	600100700110750110	)	-							
	BEDDING MATERIAL							375/400 450 525	490 575 670	105011011501101200120	)								
BEDDING	E GRANULAR MATERIAL Im	GRADED GRANULAR MATERIAL mm		NOMINAL PIPE DIAMETER mm	MAXIMU STONE S mm			600 675 750	775 815 905	1200         120           1350         130           1450         150           1500         160		_							
10,14	L	14 TO 5		150	15			825 900	985 1070	1600 170 1900 190	)								
10, 14		14 TO 5, 20 TO 5		200 - 525	20			1050 1200 1350	1265 1430 1615	205022023002502450280	)								
14, 20,		14 TO 5, 20 TO 5 14 TO 5, 20 TO 5, 40 TO 5		OVER 525	40			1500 1600 1800	1745 1910 2090	260030024003402950370	)	-							
							l					-							
												-	P1	12/05/17	FOR TENDER		AS	ГЈТ	GC
												-	Rev.	Date		Description	Ву		App'd
													Drawing	l Status	FOR TE	NDER		Suitabi	ility <b>2</b>
												ľ	Λ	ТК	INS	Eu 28	uston Tower 36 Euston Road andon		
																	W1 3AT		
													Convr	right 🔿 At	tkins Limited (2	Fa	el: +44 (0)20 712 x: +44 (0)20 712	1 2111	
TABLEE	THERMOPLAST		G REQUIREME		of onvor (	nto 6 Oma)	for stated r		ata 600mm				Client			015) W	ww.atkinsglobal.c	om	
Bedding Class	Material Type	Location	Nominal pipe diameter (mm)	150	225	300 300	375	bipe size up	450	500	600								
Class S	single size granular	Trafficked/ Paved Areas		0.6 - 6.0	0.8 - 3.6	1.0 - 3.4	0.7 - 3.6	0.7 - 3.4	0.7 - 3.2	0.8 - 3.0	0.9 - 2.6			F	Richmond u	pon Tham	es College		
Class S	single size granular	Un-Paved /		0.6 - 6.0	0.6 - 5.0	0.6 - 4.0	0.6 - 4.0	0.6 - 4.0	0.6 - 4.0	0.6 - 3.8	0.6 - 3.4	-	Project T			אייד ואר			
Class S	graded granular	Trafficked/ Paved Areas	Installation depths (m)	0.9 - 3.4	1.0 - 2.8	1.1 - 2.2	1.0 - 2.2	1.1 - 2.2	1.1 - 2.0	1.2 - 1.9	-		F	τις ΗΜ		JN THAI VELOPN	MES COLL /IENT	.cGE	
Class S	graded granular	Un-Paved / Landscape Areas	-	0.6 - 4.0		0.6 - 3.2	0.6 - 3.2	0.6 - 3.2	0.6 - 3.2	0.6 - 3.0	0.6 - 3.0	-	Drawing	Title					
Class Z2				< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6	< 0.6			OUL AN			TER DRA		θE
												ļ	0			5		A .:	
														1:500	Designed AST	Drawn AY	JT	Authorise G(	
												L	Original :	A1	Date 11/04/2017	Date 11/04/2017		Date 11/04/2	
													0	5137894	4-ATK-00	-XX-DR	-C-0355	Revisio P1	
																		1	

# **Appendix B. Relevant Calculations**

## B.1. Drainage network capacity and flooding assessment

Atkins		Page 1							
Woodcote Grove	Richmond upon Thames College								
Ashley Road	SW Network	4							
Epsom Surrey KT18 5BW		Micco							
Date 15/12/15	Designed by HS								
File PHASE 2 + EXTERNALS.MDX	Checked by JST	Diamage							
XP Solutions	Network 2015.1								
STORM SEWER DESIGN by the Modified Rational Method Design Criteria for Storm									
Pipe Sizes STANDARD Manhole Sizes STANDARD									
FSR Rainfall Model - England and Wales									
Return Period (years)	2 Add Flow / Climate Chan	5							
	20.000 Minimum Backdrop Heig								
Ratio R	1 5								
Maximum Rainiali (MM/Mr) Maximum Time of Concentration (mins)	250 Min Design Depth for Optimisati 30 Min Vel for Auto Design only								
Foul Sewage (1/s/ha)									
Volumetric Runoff Coeff.		(1.11) 500							
Design	ed with Level Soffits								

Woodcote								Page 2				
	Grove			Richr	mond upon Tha	ames Coll	ege					
Ashley Ro	ad			SW Ne	etwork			Y				
Epsom Sur	rey K	T18 5BW						Micco				
Date 15/1	2/15			Desi	gned by HS							
File PHAS	E 2 +	EXTERNALS	.MDX		Checked by JST Drainage							
XP Soluti	ons				ork 2015.1							
<u>Sum</u>	_		<u>.</u>	Simulatio	Maximum Leve on Criteria Additional Fl							
	111.00	Hot Star				or * 10m³/						
	le Head	ot Start Le <sup>.</sup> loss Coeff	vel (mm) (Global)	0.500	Flow per Persor		oeffiecient (l/per/day)					
FOU.	I Sewage	e per hecta	re (I/S)	0.000								
	N	umber of On	line Co	ntrols 1	Number of Sto Number of Tim Number of Rea	e/Area Dia	grams O					
			Svnt	hetic Ra	infall Details							
		Rainfall	Model		FSR R	atio R 0.4						
				ngland a	nd Wales Cv (S							
		M5-60	(mm)		20.000 Cv (W	inter) 0.8	40					
	Margir	for Flood	Risk Wa	.rning (m	m)		300.0					
	-		Analysi	s Timest	ep 2.5 Second	Increment	(Extended)					
				DTS Stat			OFF					
				DVD Stat tia Stat			ON ON					
			THET	tia Stat	45		010					
		Prof	1 - ( - )									
	5		- ( - )	1 - 0	0 00 100 10		r and Wint					
	Dı		- ( - )		0, 60, 120, 18 , 960, 1440, 2	0, 240, 36	0, 480, 60	0,				
	Dı		- ( - )		0, 60, 120, 18 , 960, 1440, 2	0, 240, 36 160, 2880,	0, 480, 60	0, 0,				
F	Return B	eriod(s)	(mins) years)			0, 240, 36 160, 2880,	0, 480, 60 4320, 576 8640, 100 1	0, 0, 80 00				
F	Return B	uration(s)	(mins) years)			0, 240, 36 160, 2880,	0, 480, 60 4320, 576 8640, 100 1	0, 0, 80				
F	Return B	eriod(s)	(mins) years)			0, 240, 36 160, 2880,	0, 480, 60 4320, 576 8640, 100 1	0, 0, 80 00				
	Return H Cl <b>US/MH</b>	Period(s) (y	(mins) years) ge (%) Return	720 Climate	, 960, 1440, 2 First (X)	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
F PN	Return H Cl	Period(s) (y	(mins) years) ge (%) Return	720	, 960, 1440, 2 First (X)	0, 240, 36 160, 2880, 7200,	0, 480, 60 4320, 576 8640, 100 1	0, 0, 80 00 30 <b>Overflow</b>				
<b>PN</b> S7.000	Return H Cl US/MH Name S19	Period(s) (y Limate Chang Storm 480 Winter	(mins) (mins) ge (%) Return Period 100	720 Climate Change +30%	<pre>, 960, 1440, 2      First (X)      Surcharge 100/15 Summer</pre>	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
<b>PN</b> S7.000 S7.001	Return H Cl US/MH Name S19 Srwp11	Period(s) (y Limate Chang Storm 480 Winter 480 Winter	(mins) (mins) ge (%) Return Period 100 100	720 Climate Change +30% +30%	<pre>, 960, 1440, 2     First (X)     Surcharge 100/15 Summer 100/15 Summer</pre>	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
<b>PN</b> \$7.000 \$7.001 \$8.000	Return H Cl US/MH Name S19 Srwp11 S7	Period(s) (y limate Change Storm 480 Winter 480 Winter 480 Winter	(mins) (mins) ge (%) Return Period 100 100 100	720 Climate Change +30% +30% +30%	<pre>, 960, 1440, 2     First (X)     Surcharge 100/15 Summer 100/15 Summer 100/15 Summer</pre>	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
<b>PN</b> S7.000 S7.001	Return H Cl US/MH Name S19 Srwp11 S7 S2	Period(s) (y Limate Chang Storm 480 Winter 480 Winter	(mins) (mins) ge (%) Return Period 100 100 100	720 Climate Change +30% +30% +30%	<pre>, 960, 1440, 2     First (X)     Surcharge 100/15 Summer 100/15 Summer</pre>	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
<b>PN</b> \$7.000 \$7.001 \$8.000 \$7.002 \$9.000	Return H Cl US/MH Name S19 Srwp11 S7 S2 S9	Storm 480 Winter 480 Winter 480 Winter 480 Winter 480 Winter	(mins) (mins) ge (%) Return Period 100 100 100 100	720 Climate Change +30% +30% +30% +30%	<pre>, 960, 1440, 2     First (X)     Surcharge 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer</pre>	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
PN \$7.000 \$7.001 \$8.000 \$7.002 \$9.000 \$7.003 \$10.000	Return H Cl US/MH Name S19 Srwp11 S7 S2 S9 Srwp05 S8	Storm 480 Winter 480 Winter 480 Winter 480 Winter 480 Winter 480 Winter 480 Winter 480 Winter 480 Winter	(mins) (mins) ge (%) Return Period 100 100 100 100 100 100	720 <b>Climate</b> <b>Change</b> +30% +30% +30% +30% +30% +30%	<pre>, 960, 1440, 2     First (X)     Surcharge 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer</pre>	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
PN \$7.000 \$7.001 \$8.000 \$7.002 \$9.000 \$7.003 \$10.000 \$7.004	Return H Cl US/MH Name S19 Srwp11 S7 S2 S9 Srwp05 S8 Srwp04	Storm 480 Winter 480 Winter	(mins) (mins) ge (%) Return Period 100 100 100 100 100 100 100	720 <b>Climate</b> <b>Change</b> +30% +30% +30% +30% +30% +30% +30%	<pre>, 960, 1440, 2 First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer</pre>	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
PN \$7.000 \$7.001 \$8.000 \$7.002 \$9.000 \$7.003 \$10.000 \$7.004 \$11.000	Return H Cl US/MH Name S19 Srwp11 S7 S2 S9 Srwp05 S8 Srwp04 S14	Storm 480 Winter 480 Winter	(mins) (mins) ge (%) Return Period 100 100 100 100 100 100 100	720 <b>Climate</b> <b>Change</b> +30% +30% +30% +30% +30% +30% +30% +30%	<pre>, 960, 1440, 2 First (X) Surcharge 100/15 Summer 100/15 Summer</pre>	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
PN \$7.000 \$7.001 \$8.000 \$7.002 \$9.000 \$7.003 \$10.000 \$7.004	Return H Cl US/MH Name S19 Srwp11 S7 S2 S9 Srwp05 S8 Srwp04 S14 S14 S16	Storm 480 Winter 480 Winter	(mins) (mins) ge (%) Return Period 100 100 100 100 100 100 100 100	720 <b>Climate</b> <b>Change</b> +30% +30% +30% +30% +30% +30% +30% +30% +30%	<pre>, 960, 1440, 2 First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer 100/15 Summer</pre>	0, 240, 36 160, 2880, 7200, First (Y)	0, 480, 60 4320, 576 8640, 100 1 First (Z)	0, 0, 80 00 30 <b>Overflow</b>				
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Atkins		Page 3
Woodcote Grove	Richmond upon Thames College	
Ashley Road	SW Network	<u>Y</u>
Epsom Surrey KT18 5BW		Micco
Date 15/12/15	Designed by HS	Drainare
File PHASE 2 + EXTERNALS.MDX	Checked by JST	Diamaye
XP Solutions	Network 2015.1	

Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name	Water Level (m)	Surcharged Depth (m)		Flow / Cap.	Overflow (1/s)	Pipe Flow (l/s)	Status	Level Exceeded
S7.000	S19	8.197	0.592	0.000	0.01		0.1	SURCHARGED	
S7.001	Srwp11	8.197	0.709	0.000	0.06		1.7	SURCHARGED	
S8.000	S7	8.197	0.622	0.000	0.01		0.1	SURCHARGED	
S7.002	S2	8.197	0.740	0.000	0.11		3.3	SURCHARGED	
S9.000	S9	8.197	0.725	0.000	0.01		0.1	SURCHARGED	
S7.003	Srwp05	8.197	0.836	0.000	0.13		4.7	SURCHARGED	
S10.000	S8	8.196	0.801	0.000	0.01		0.1	SURCHARGED	
S7.004	Srwp04	8.196	0.928	0.000	0.15		5.9	SURCHARGED	
S11.000	S14	8.194	0.890	0.000	0.01		0.1	SURCHARGED	
S12.000	S16	8.194	0.962	0.000	0.02		0.1	SURCHARGED	
S7.005	S16	8.194	1.079	0.000	0.22		6.8	SURCHARGED	
S13.000	S18	8.193	1.010	0.000	0.01		0.1	SURCHARGED	
S7.006	Srwp02	8.193	1.184	0.000	0.19		7.9	SURCHARGED	
S14.000	S27	8.400	-0.150	0.000	0.00		0.0	OK	
S15.000	S1	8.345	-0.150	0.000	0.00		0.0	OK	
S15.001	S5	8.192	-0.225	0.000	0.00		0.0	OK	
S15.002	S5	8.193	-0.150	0.000	0.01		0.2	OK	
S16.000	S23	8.193	-0.087	0.000	0.01		0.1	OK	

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Woodcote Grove	Richmond upon Thames College	
Ashley Road	SW Network	L.
Epsom Surrey KT18 5BW		Micco
Date 15/12/15	Designed by HS	
File PHASE 2 + EXTERNALS.MDX	Checked by JST	Dialinatic
XP Solutions	Network 2015.1	1

Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name	Storm		Climate Change	First Surch	•••	First (Y) Flood	First (Z) Overflow	Overflow Act.
s15.003	S33	480 Winter	100	+30%					
S14.001	Srwp08	480 Winter	100	+30%	100/360	Winter			
S17.000	S27	15 Winter	100	+30%	100/15	Summer	100/15 Winter		
S17.001	S27	15 Winter	100	+30%	100/15	Summer			
S17.002	S27	480 Winter	100	+30%	100/15	Summer			
S17.003	S8	480 Winter	100	+30%	100/15	Summer			
S18.000	S9	15 Winter	100	+30%	100/15	Summer			
S14.002	S7	480 Winter	100	+30%	100/15	Summer			
S7.007	S8	480 Winter	100	+30%	100/15	Summer			
S7.008	S9	480 Winter	100	+30%					

PN	US/MH Name	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (1/s)	Pipe Flow (l/s)	Status	Level Exceeded
S15.003	S33	8.193	-0.020	0.000	0.03		1.0	OK	
S14.001	Srwp08	8.193	0.079	0.000	0.05		1.8	SURCHARGED	
S17.000	S27	9.000	1.175	0.323	1.54		61.5	FLOOD	1
S17.001	S27	8.611	1.011	0.000	1.44		158.4	SURCHARGED	
S17.002	S27	8.196	0.919	0.000	0.22		34.6	SURCHARGED	
S17.003	S8	8.195	1.018	0.000	0.23		34.3	SURCHARGED	
S18.000	S9	8.239	0.114	0.000	1.90		54.6	SURCHARGED	
S14.002	S7	8.193	1.085	0.000	0.19		41.9	SURCHARGED	
S7.007	S8	8.191	1.327	0.000	0.04		5.4	SURCHARGED	
S7.008	S9	6.433	-0.398	0.000	0.03		5.4	OK	

# Appendix C. Communications with London Borough of Richmondupon-Thames

C.1. Flood Risk Assessment

#### Jessica

Your proposal are acceptable. As I said, I will be leaving Richmond in the near future, so please ensure that all that we have previously agreed is included, to ensure that anyone else dealing with it can easily find it.

**Regards Brian** 

#### **Brian Humphris**

Highway Asset Co-ordinator Serving Richmond and Wandsworth Councils

Environment Directorate London Borough of Richmond upon Thames 2nd Floor Civic Centre 44 York Street Twickenham TW1 3BZ

020 8891 7738

brian.humphris@richmond.gov.uk www.richmond.gov.uk / www.wandsworth.gov.uk

From: Taylor, Jessica [mailto:Jessica.Taylor@atkinsglobal.com]
Sent: 07 December 2016 16:22
To: Brian Humphris
Cc: 'Robert Mackenzie-Grieve'
Subject: RE: Richmond-upon-Thames College

Hi Brian,

If we could kindly get you to confirm your agreement with our below comments it would be very much appreciated. We plan to submit the Reserve Matters application for the sight shortly and would like to confirm your stance for consistency going forward.

Thanks very much for your assistance with this to date.

Best regards,

Jess Taylor Civil Engineer, Infrastructure ATKINS

020 7121 2305

From: Taylor, Jessica
Sent: 06 December 2016 11:20
To: Brian Humphris <<u>brian.humphris@richmond.gov.uk</u>>
Cc: Robert Mackenzie-Grieve <<u>robert.mackenzie-grieve@cgms.co.uk</u>>
Subject: RE: Richmond-upon-Thames College

Hi Brian,

Thank you for your time this morning.

As discussed, the Phase 1 area of the Richmond-upon-Thames College development is located in a relatively low flood risk zone from all relevant sources (rivals, tidal, surface water, sewer).

As agreed we will incorporate a section to address the flood risk for the site within the Drainage Strategy document to be submitted with the Reserve Matters application. However a formal FRA will not be required.

If you could please respond and confirm this reflects our conversation this morning it would be very much appreciated.

Best regards,

Jess

Best regards,

#### Jess Taylor

Civil Engineer, Infastructure

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Euston Tower, 286 Euston Road, London NW1 3AT | Tel: +44 (0)20 7121 2305 | Mob: +44 (0) 7482 623583 Email: <u>jessica.taylor@atkinsglobal.com</u> Web: <u>www.atkinsglobal.com</u> Careers: <u>www.atkinsglobal.com/careers</u>

From: Brian Humphris [mailto:brian.humphris@richmond.gov.uk]
Sent: 05 December 2016 15:08
To: Taylor, Jessica <<u>Jessica.Taylor@atkinsglobal.com</u>>
Subject: RE: Richmond-upon-Thames College

#### Hi Jessica

I think it would be preferable for you to submit a formal FRA, including a summary of what has already been agreed, although this could be included within the Reserved Matters.

#### **Regards Brian**

**Brian Humphris** Highway Asset Co-ordinator Serving Richmond and Wandsworth Councils

Environment Directorate London Borough of Richmond upon Thames 2nd Floor Civic Centre 44 York Street Twickenham TW1 3BZ

020 8891 7738

brian.humphris@richmond.gov.uk www.richmond.gov.uk / www.wandsworth.gov.uk

From: Taylor, Jessica [mailto:Jessica.Taylor@atkinsglobal.com] Sent: 02 December 2016 12:10 To: Brian Humphris Subject: Richmond-upon-Thames College

Hi Brian,

I hope this finds you well.

Just tried to give you a ring in relation to the below, but I missed you.

To recap - back in May of this year we were in touch to discuss the surface water management and discharge strategy for the Richmond-upon-Thames College redevelopment.

Atkins has undertaken the drainage design for the new Richmond-upon-Thames College Phase 1 main building build (site MasterPlan attached for reference). I have attached our original correspondence describing the surface water strategy however to summarise we are using a combination of infiltration (through permeable paving) into the underlying Kempton Park Gravels Strata and discharge (at greenfield) into the local Thames Water Surface Water sewer. We have approached Thames Water regarding the surface water connection, who have confirmed that no Impact Study is required.

We are now contacting you to confirm the requirements for the College Phase 1 development in terms of a Flood Risk Assessment.

Similar to the neighbouring School development the College Phase 1 site is within Flood Zone 1. We acknowledge that the playing fields located within the southern portion of the site are within Flood Zone 2. However his area of the site is much lower than the proposed development and as such this development will have no effect on their site other than to improve drainage in the area and therefore flooding.

Given that a detailed summary of the Drainage Strategy, flood mitigation and the SuDs employed

in Phase 1 of the development will be submitted with the Reserve Matters, we feel that an FRA may not be required for this area of the site. This is similar to the strategy employed by the School.



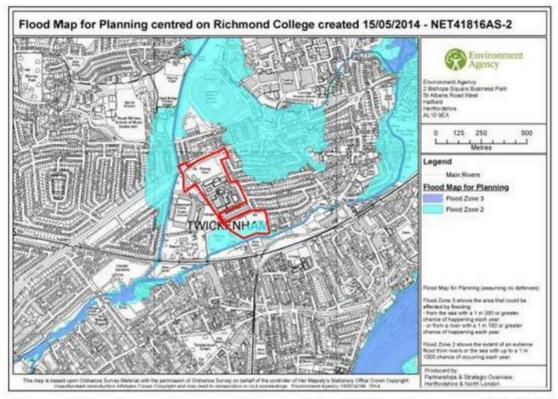


Figure 3.1 Environment Agency River and Coastal Flood Zone map (EA, 2014)

We appreciate that you are yet to sight our official drainage strategy documents however we just wanted to clarify this aspect of the drainage with you prior to prevent delays on submission of the Reserve Matters Application.

If you could please give me a ring back to discuss this in detail it would be greatly appreciated.

Best regards,

Jess Taylor Civil Engineer, Infastructure

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# Appendix D. Flood Risk Maps

- D.1. Flood Map (EA)
- D.2. Fluvial and Tidal Flood Maps (EA and LBRuT)
- D.3. Surface Water Flood Map (EA and LBRuT)
- D.4. Sewer Flood Map (EA and LBRuT)
- D.5. Groundwater Flood Map (EA and LBRuT)
- D.6. Reservoir Flood Map (EA)