

# Predicted Energy Assessment

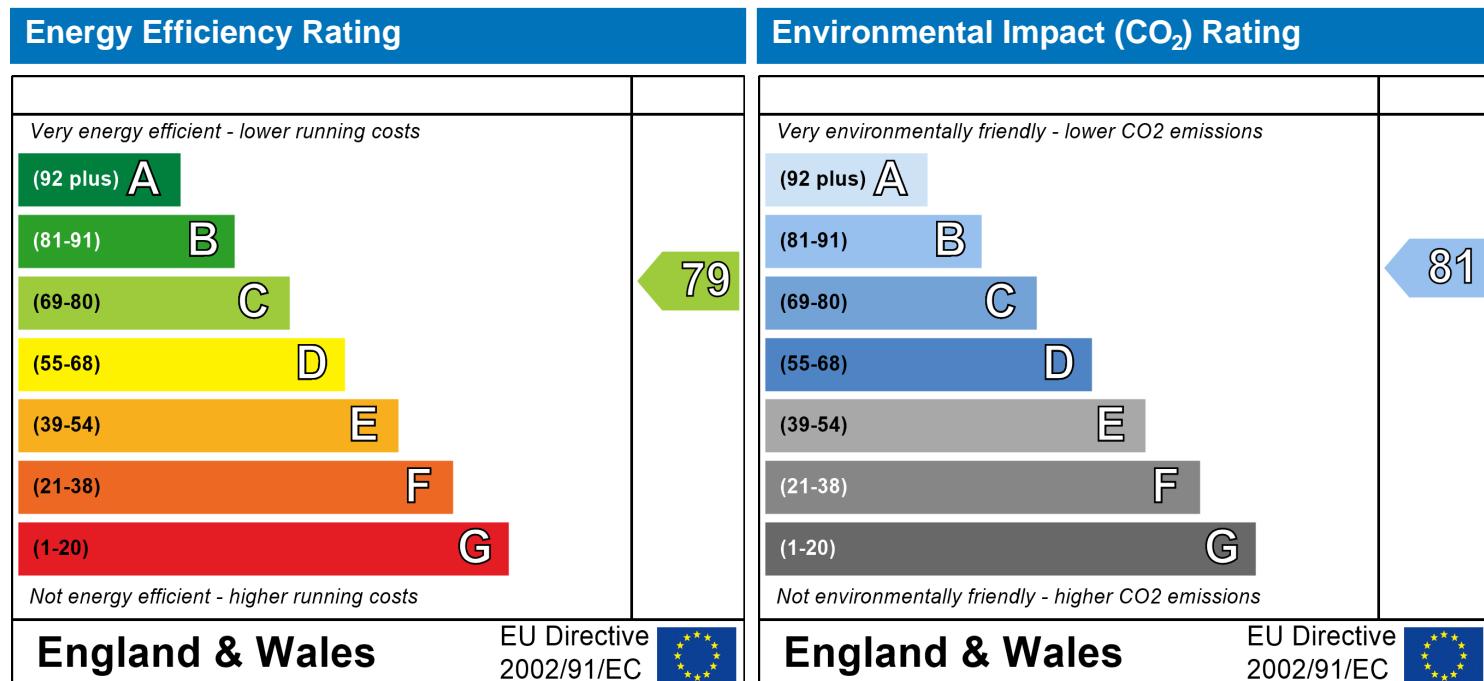


Dwelling type:  
Date of assessment:  
Produced by:  
Total floor area:

Semi-detached House  
31 March 2020  
Peter Mitchell  
88.16 m<sup>2</sup>

This is a Predicted Energy Assessment for a property which is not yet complete. It includes a predicted energy rating which might not represent the final energy rating of the property on completion. Once the property is completed, an Energy Performance Certificate is required providing information about the energy performance of the completed property.

Energy performance has been assessed using the SAP 2012 methodology and is rated in terms of the energy use per square metre of floor area, energy efficiency based on fuel costs and environmental impact based on carbon dioxide (CO<sub>2</sub>) emissions.



The energy efficiency rating is a measure of the overall efficiency of a home. The higher the rating the more energy efficient the home is and the lower the fuel bills are likely to be.

The environmental impact rating is a measure of a home's impact on the environment in terms of carbon dioxide (CO<sub>2</sub>) emissions. The higher the rating the less impact it has on the environment.

# SAP WorkSheet: New dwelling design stage

## User Details:

|                       |                  |                          |                   |
|-----------------------|------------------|--------------------------|-------------------|
| <b>Assessor Name:</b> | Peter Mitchell   | <b>Stroma Number:</b>    | STRO007945        |
| <b>Software Name:</b> | Stroma FSAP 2012 | <b>Software Version:</b> | Version: 1.0.4.25 |

Property Address: Unit 1 Clean ASHP

## Address :

1. Overall dwelling dimensions:

|   | <b>Area(m<sup>2</sup>)</b> | <b>Av. Height(m)</b>                 | <b>Volume(m<sup>3</sup>)</b> |
|---|----------------------------|--------------------------------------|------------------------------|
| Ground floor  | 52.9<br>(1a) x             | 2.37<br>(2a) =                       | 125.37<br>(3a)               |
| First floor   | 35.26<br>(1b) x            | 2.56<br>(2b) =                       | 90.27<br>(3b)                |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n) | 88.16<br>(4)               |                                      |                              |
| Dwelling volume   |                            | (3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) = | 215.64<br>(5)                |

2. Ventilation rate:

|                              | <b>main heating</b> | <b>secondary heating</b> | <b>other</b> | <b>total</b> | <b>m<sup>3</sup> per hour</b> |
|------------------------------|---------------------|--------------------------|--------------|--------------|-------------------------------|
| Number of chimneys           | 0                   | + 0                      | + 0          | = 0          | x 40 = 0<br>(6a)              |
| Number of open flues         | 0                   | + 0                      | + 0          | = 0          | x 20 = 0<br>(6b)              |
| Number of intermittent fans  |                     |                          |              | 2            | x 10 = 20<br>(7a)             |
| Number of passive vents      |                     |                          |              | 0            | x 10 = 0<br>(7b)              |
| Number of flueless gas fires |                     |                          |              | 0            | x 40 = 0<br>(7c)              |

## Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = 20 ÷ (5) = 0.09 (8)

If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)

Number of storeys in the dwelling (ns)

Additional infiltration

[(9)-1]x0.1 = 0  
(9)

0  
(10)

0  
(11)

Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction

if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35

If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0

If no draught lobby, enter 0.05, else enter 0

Percentage of windows and doors draught stripped

Window infiltration 0.25 - [0.2 x (14) ÷ 100] =

Infiltration rate (8) + (10) + (11) + (12) + (13) + (15) =

Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area

If based on air permeability value, then (18) = [(17) ÷ 20]+(8), otherwise (18) = (16)

Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used

Number of sides sheltered

Shelter factor (20) = 1 - [0.075 x (19)] =

Infiltration rate incorporating shelter factor (21) = (18) x (20) =

Infiltration rate modified for monthly wind speed

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Monthly average wind speed from Table 7

|            |   |     |     |     |     |     |     |   |     |     |     |
|------------|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|
| (22)m= 5.1 | 5 | 4.9 | 4.4 | 4.3 | 3.8 | 3.8 | 3.7 | 4 | 4.3 | 4.5 | 4.7 |
|------------|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|

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Wind Factor (22a)m = (22)m ÷ 4

|         |      |      |      |     |      |      |      |      |   |      |      |      |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|
| (22a)m= | 1.27 | 1.25 | 1.23 | 1.1 | 1.08 | 0.95 | 0.95 | 0.92 | 1 | 1.08 | 1.12 | 1.18 |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|

Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 0.37 | 0.36 | 0.36 | 0.32 | 0.31 | 0.28 | 0.28 | 0.27 | 0.29 | 0.31 | 0.33 | 0.34 |
|------|------|------|------|------|------|------|------|------|------|------|------|

Calculate effective air change rate for the applicable case

If mechanical ventilation:

|   |       |
|---|-------|
| 0 | (23a) |
|---|-------|

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

|   |       |
|---|-------|
| 0 | (23b) |
|---|-------|

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

|   |       |
|---|-------|
| 0 | (23c) |
|---|-------|

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24a)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24a)

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24b)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24b)

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b)m + 0.5 × (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24c)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24c)

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² × 0.5]

|         |      |      |      |      |      |      |      |      |      |      |      |      |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|
| (24d)m= | 0.57 | 0.57 | 0.56 | 0.55 | 0.55 | 0.54 | 0.54 | 0.54 | 0.54 | 0.55 | 0.55 | 0.56 |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|

(24d)

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

|        |      |      |      |      |      |      |      |      |      |      |      |      |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|
| (25)m= | 0.57 | 0.57 | 0.56 | 0.55 | 0.55 | 0.54 | 0.54 | 0.54 | 0.54 | 0.55 | 0.55 | 0.56 |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|

(25)

### 3. Heat losses and heat loss parameter:

| ELEMENT                                | Gross area (m <sup>2</sup> ) | Openings m <sup>2</sup> | Net Area A ,m <sup>2</sup> | U-value W/m <sup>2</sup> K | A X U (W/K) | k-value kJ/m <sup>2</sup> ·K | A X k kJ/K |
|--|------------------------------|-------------------------|----------------------------|----------------------------|-------------|------------------------------|------------|
| Windows Type 1                         |                              |                         | 6.01                       | x1/[1/( 1.2 )+ 0.04] =     | 6.88        |                              | (27)       |
| Windows Type 2                         |                              |                         | 6.3                        | x1/[1/( 1.2 )+ 0.04] =     | 7.21        |                              | (27)       |
| Windows Type 3                         |                              |                         | 1.59                       | x1/[1/( 1.2 )+ 0.04] =     | 1.82        |                              | (27)       |
| Windows Type 4                         |                              |                         | 0.61                       | x1/[1/( 1.2 )+ 0.04] =     | 0.7         |                              | (27)       |
| Rooflights Type 1                      |                              |                         | 1.41                       | x1/[1/(1.2) + 0.04] =      | 1.692       |                              | (27b)      |
| Rooflights Type 2                      |                              |                         | 1.25                       | x1/[1/(1.2) + 0.04] =      | 1.5         |                              | (27b)      |
| Rooflights Type 3                      |                              |                         | 2.04                       | x1/[1/(1.2) + 0.04] =      | 2.448       |                              | (27b)      |
| Floor                                  |                              |                         | 52.9                       | x 0.13 =                   | 6.877       |                              | (28)       |
| Walls                                  | 109.46                       | 16.71                   | 92.75                      | x 0.18 =                   | 16.7        |                              | (29)       |
| Roof Type1                             | 35.52                        | 1.25                    | 34.27                      | x 0.13 =                   | 4.46        |                              | (30)       |
| Roof Type2                             | 17.86                        | 3.45                    | 14.41                      | x 0.13 =                   | 1.87        |                              | (30)       |
| Total area of elements, m <sup>2</sup> |                              |                         | 215.74                     |                            |             |                              | (31)       |
| Party wall                             |                              |                         | 32.84                      | x 0 =                      | 0           |                              | (32)       |

\* for windows and roof windows, use effective window U-value calculated using formula  $1/[(1/U\text{-value})+0.04]$  as given in paragraph 3.2

\*\* include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = 54.42 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) = 0 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m<sup>2</sup>K Indicative Value: Medium 250 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f

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can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K

19.03

(36)

if details of thermal bridging are not known (36) =  $0.05 \times (31)$

Total fabric heat loss

(33) + (36) =

73.44

(37)

Ventilation heat loss calculated monthly

(38)m =  $0.33 \times (25)m \times (5)$

| Jan          | Feb  | Mar   | Apr   | May   | Jun   | Jul   | Aug   | Sep  | Oct   | Nov  | Dec   |
|--------------|------|-------|-------|-------|-------|-------|-------|------|-------|------|-------|
| (38)m= 40.49 | 40.3 | 40.11 | 39.23 | 39.07 | 38.31 | 38.31 | 38.16 | 38.6 | 39.07 | 39.4 | 39.75 |

(38)

Heat transfer coefficient, W/K

(39)m = (37) + (38)m

|   |        |        |        |        |        |        |        |        |        |        |        |
|---|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| (39)m= 113.93                             | 113.74 | 113.55 | 112.68 | 112.51 | 111.75 | 111.75 | 111.61 | 112.04 | 112.51 | 112.84 | 113.19 |
| Average = Sum(39) <sub>1...12</sub> / 12= |        |        |        |        |        |        |        |        |        |        | 112.67 |

112.67

(39)

Heat loss parameter (HLP), W/m<sup>2</sup>K

(40)m = (39)m ÷ (4)

|   |      |      |      |      |      |      |      |      |      |      |      |
|---|------|------|------|------|------|------|------|------|------|------|------|
| (40)m= 1.29                               | 1.29 | 1.29 | 1.28 | 1.28 | 1.27 | 1.27 | 1.27 | 1.27 | 1.28 | 1.28 | 1.28 |
| Average = Sum(40) <sub>1...12</sub> / 12= |      |      |      |      |      |      |      |      |      |      | 1.28 |

(40)

Number of days in month (Table 1a)

| Jan       | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| (41)m= 31 | 28  | 31  | 30  | 31  | 30  | 31  | 31  | 30  | 31  | 30  | 31  |

(41)

4. Water heating energy requirement:

kWh/year:

Assumed occupancy, N

2.6

(42)

if TFA > 13.9,  $N = 1 + 1.76 \times [1 - \exp(-0.000349 \times (\text{TFA} - 13.9)2)] + 0.0013 \times (\text{TFA} - 13.9)$

if TFA £ 13.9,  $N = 1$

Annual average hot water usage in litres per day  $Vd,\text{average} = (25 \times N) + 36$

95.94

(43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Hot water usage in litres per day for each month  $Vd,m = \text{factor from Table 1c} \times (43)$

|                                     |       |       |       |       |       |       |       |       |       |       |         |
|-------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|
| (44)m= 105.54                       | 101.7 | 97.86 | 94.02 | 90.19 | 86.35 | 86.35 | 90.19 | 94.02 | 97.86 | 101.7 | 105.54  |
| Total = Sum(44) <sub>1...12</sub> = |       |       |       |       |       |       |       |       |       |       | 1151.31 |

(44)

Energy content of hot water used - calculated monthly =  $4.190 \times Vd,m \times nm \times DTm / 3600 \text{ kWh/month}$  (see Tables 1b, 1c, 1d)

|                                     |        |        |        |        |        |       |        |        |        |        |         |
|-------------------------------------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|---------|
| (45)m= 156.51                       | 136.88 | 141.25 | 123.15 | 118.16 | 101.96 | 94.49 | 108.42 | 109.72 | 127.87 | 139.58 | 151.57  |
| Total = Sum(45) <sub>1...12</sub> = |        |        |        |        |        |       |        |        |        |        | 1509.55 |

(45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

|              |       |       |       |       |       |       |       |       |       |       |       |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| (46)m= 23.48 | 20.53 | 21.19 | 18.47 | 17.72 | 15.29 | 14.17 | 16.26 | 16.46 | 19.18 | 20.94 | 22.74 |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|

(46)

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel

120

(47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

a) If manufacturer's declared loss factor is known (kWh/day):

0

(48)

Temperature factor from Table 2b

0

(49)

Energy lost from water storage, kWh/year  $(48) \times (49) =$

120

(50)

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day)

0.01

(51)

If community heating see section 4.3

Volume factor from Table 2a

1

(52)

Temperature factor from Table 2b

0.54

(53)

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Energy lost from water storage, kWh/year  $(47) \times (51) \times (52) \times (53) =$ 

|      |
|------|
| 0.75 |
| 0.75 |

 (54)  
Enter (50) or (54) in (55) 

|      |
|------|
| 0.75 |
| 0.75 |

 (55)

Water storage loss calculated for each month  $((56)m = (55) \times (41)m$ 

|      |       |      |       |      |       |      |      |       |      |       |      |
|------|-------|------|-------|------|-------|------|------|-------|------|-------|------|
| 23.2 | 20.95 | 23.2 | 22.45 | 23.2 | 22.45 | 23.2 | 23.2 | 22.45 | 23.2 | 22.45 | 23.2 |
|------|-------|------|-------|------|-------|------|------|-------|------|-------|------|

 (56)

If cylinder contains dedicated solar storage,  $(57)m = (56)m \times [(50) - (H11)] \div (50)$ , else  $(57)m = (56)m$  where (H11) is from Appendix H

$(57)m =$ 

|      |       |      |       |      |       |      |      |       |      |       |      |
|------|-------|------|-------|------|-------|------|------|-------|------|-------|------|
| 23.2 | 20.95 | 23.2 | 22.45 | 23.2 | 22.45 | 23.2 | 23.2 | 22.45 | 23.2 | 22.45 | 23.2 |
|------|-------|------|-------|------|-------|------|------|-------|------|-------|------|

 (57)

Primary circuit loss (annual) from Table 3 

|   |
|---|
| 0 |
|---|

 (58)

Primary circuit loss calculated for each month  $(59)m = (58) \div 365 \times (41)m$   
(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat) 

|       |       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 23.26 | 21.01 | 23.26 | 22.51 | 23.26 | 22.51 | 23.26 | 23.26 | 22.51 | 23.26 | 22.51 | 23.26 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|

 (59)

Combi loss calculated for each month  $(61)m = (60) \div 365 \times (41)m$ 

|   |   |   |   |   |   |   |   |   |   |   |   |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---|---|---|---|---|---|---|---|---|---|---|---|

 (61)

Total heat required for water heating calculated for each month  $(62)m = 0.85 \times (45)m + (46)m + (57)m + (59)m + (61)m$ 

|        |        |        |        |        |        |        |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 202.97 | 178.85 | 187.71 | 168.11 | 164.62 | 146.92 | 140.94 | 154.88 | 154.68 | 174.32 | 184.54 | 198.03 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|

 (62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)  
(add additional lines if FGHRs and/or WWHRs applies, see Appendix G) 

|   |   |   |   |   |   |   |   |   |   |   |   |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---|---|---|---|---|---|---|---|---|---|---|---|

 (63)

Output from water heater 

|        |        |        |        |        |        |        |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 202.97 | 178.85 | 187.71 | 168.11 | 164.62 | 146.92 | 140.94 | 154.88 | 154.68 | 174.32 | 184.54 | 198.03 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|

 Output from water heater (annual) 

|         |
|---------|
| 2056.57 |
|---------|

 (64)

Heat gains from water heating, kWh/month  $0.25 \times [0.85 \times (45)m + (61)m] + 0.8 \times [(46)m + (57)m + (59)m]$ 

|       |       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 89.21 | 79.08 | 84.13 | 76.91 | 76.46 | 69.87 | 68.58 | 73.22 | 72.45 | 79.68 | 82.38 | 87.56 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|

 (65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

## 5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts 

|        |        |        |        |        |        |        |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Jan    | Feb    | Mar    | Apr    | May    | Jun    | Jul    | Aug    | Sep    | Oct    | Nov    | Dec    |
| 155.98 | 155.98 | 155.98 | 155.98 | 155.98 | 155.98 | 155.98 | 155.98 | 155.98 | 155.98 | 155.98 | 155.98 |

 (66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5 

|       |       |       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 52.52 | 46.65 | 37.94 | 28.72 | 21.47 | 18.13 | 19.59 | 25.46 | 34.17 | 43.39 | 50.64 | 53.98 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|

 (67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5 

|        |        |        |        |        |        |        |        |        |        |        |       |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| 351.72 | 355.37 | 346.17 | 326.59 | 301.88 | 278.65 | 263.13 | 259.48 | 268.67 | 288.25 | 312.97 | 336.2 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|

 (68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5 

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 53.2 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2 |
|------|------|------|------|------|------|------|------|------|------|------|------|

 (69)

Pumps and fans gains (Table 5a) 

|   |   |   |   |   |   |   |   |   |   |   |   |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---|---|---|---|---|---|---|---|---|---|---|---|

 (70)

Losses e.g. evaporation (negative values) (Table 5) 

|         |         |         |         |         |         |         |         |         |         |         |         |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| -103.99 | -103.99 | -103.99 | -103.99 | -103.99 | -103.99 | -103.99 | -103.99 | -103.99 | -103.99 | -103.99 | -103.99 |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|

 (71)

Water heating gains (Table 5) 

|       |        |        |        |        |       |       |       |        |       |        |        |
|-------|--------|--------|--------|--------|-------|-------|-------|--------|-------|--------|--------|
| 119.9 | 117.68 | 113.08 | 106.83 | 102.76 | 97.04 | 92.18 | 98.41 | 100.62 | 107.1 | 114.41 | 117.69 |
|-------|--------|--------|--------|--------|-------|-------|-------|--------|-------|--------|--------|

 (72)

**Total internal gains =**  $(66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m$ 

|        |        |        |        |       |        |        |        |        |        |        |        |
|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|
| 629.33 | 624.89 | 602.38 | 567.33 | 531.3 | 499.01 | 480.09 | 488.54 | 508.66 | 543.93 | 583.21 | 613.07 |
|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|

 (73)

## 6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

# SAP WorkSheet: New dwelling design stage

| Orientation: | Access Factor<br>Table 6d | Area<br>m <sup>2</sup> | Flux<br>Table 6a | g<br>Table 6b | FF<br>Table 6c | Gains<br>(W)  |
|--------------|---------------------------|------------------------|------------------|---------------|----------------|---------------|
| North        | 0.9x 0.77                 | x 6.01                 | x 10.63          | x 0.76        | x 0.7          | = 23.56 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 10.63          | x 0.76        | x 0.7          | = 24.7 (74)   |
| North        | 0.9x 0.77                 | x 1.59                 | x 10.63          | x 0.76        | x 0.7          | = 12.47 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 20.32          | x 0.76        | x 0.7          | = 45.03 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 20.32          | x 0.76        | x 0.7          | = 47.2 (74)   |
| North        | 0.9x 0.77                 | x 1.59                 | x 20.32          | x 0.76        | x 0.7          | = 23.82 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 34.53          | x 0.76        | x 0.7          | = 76.51 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 34.53          | x 0.76        | x 0.7          | = 80.2 (74)   |
| North        | 0.9x 0.77                 | x 1.59                 | x 34.53          | x 0.76        | x 0.7          | = 40.48 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 55.46          | x 0.76        | x 0.7          | = 122.89 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 55.46          | x 0.76        | x 0.7          | = 128.82 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 55.46          | x 0.76        | x 0.7          | = 65.03 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.72          | x 0.76        | x 0.7          | = 165.55 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.72          | x 0.76        | x 0.7          | = 173.54 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.72          | x 0.76        | x 0.7          | = 87.6 (74)   |
| North        | 0.9x 0.77                 | x 6.01                 | x 79.99          | x 0.76        | x 0.7          | = 177.23 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 79.99          | x 0.76        | x 0.7          | = 185.78 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 79.99          | x 0.76        | x 0.7          | = 93.77 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.68          | x 0.76        | x 0.7          | = 165.46 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.68          | x 0.76        | x 0.7          | = 173.45 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.68          | x 0.76        | x 0.7          | = 87.55 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 59.25          | x 0.76        | x 0.7          | = 131.27 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 59.25          | x 0.76        | x 0.7          | = 137.61 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 59.25          | x 0.76        | x 0.7          | = 69.46 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 41.52          | x 0.76        | x 0.7          | = 91.99 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 41.52          | x 0.76        | x 0.7          | = 96.43 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 41.52          | x 0.76        | x 0.7          | = 48.67 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 24.19          | x 0.76        | x 0.7          | = 53.6 (74)   |
| North        | 0.9x 0.77                 | x 6.3                  | x 24.19          | x 0.76        | x 0.7          | = 56.18 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 24.19          | x 0.76        | x 0.7          | = 28.36 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 13.12          | x 0.76        | x 0.7          | = 29.07 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 13.12          | x 0.76        | x 0.7          | = 30.47 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 13.12          | x 0.76        | x 0.7          | = 15.38 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 8.86           | x 0.76        | x 0.7          | = 19.64 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 8.86           | x 0.76        | x 0.7          | = 20.59 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 8.86           | x 0.76        | x 0.7          | = 10.39 (74)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 46.75          | x 0.76        | x 0.7          | = 21.03 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 76.57          | x 0.76        | x 0.7          | = 34.44 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 97.53          | x 0.76        | x 0.7          | = 43.87 (78)  |

# SAP WorkSheet: New dwelling design stage

|            |      |      |   |      |   |        |   |      |   |     |   |        |      |
|------------|------|------|---|------|---|--------|---|------|---|-----|---|--------|------|
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.23 | x | 0.76 | x | 0.7 | = | 49.58  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 114.87 | x | 0.76 | x | 0.7 | = | 51.67  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.55 | x | 0.76 | x | 0.7 | = | 49.72  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 108.01 | x | 0.76 | x | 0.7 | = | 48.58  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 104.89 | x | 0.76 | x | 0.7 | = | 47.18  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 101.89 | x | 0.76 | x | 0.7 | = | 45.83  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 82.59  | x | 0.76 | x | 0.7 | = | 37.15  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 55.42  | x | 0.76 | x | 0.7 | = | 24.93  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 40.4   | x | 0.76 | x | 0.7 | = | 18.17  | (78) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 30.32  | x | 0.76 | x | 0.7 | = | 20.47  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 31.5   | x | 0.76 | x | 0.7 | = | 18.85  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 30.32  | x | 0.76 | x | 0.7 | = | 29.61  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 60.64  | x | 0.76 | x | 0.7 | = | 40.94  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 62.43  | x | 0.76 | x | 0.7 | = | 37.36  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 60.64  | x | 0.76 | x | 0.7 | = | 59.23  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 103.31 | x | 0.76 | x | 0.7 | = | 69.75  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 105.22 | x | 0.76 | x | 0.7 | = | 62.98  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 103.31 | x | 0.76 | x | 0.7 | = | 100.91 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 156.31 | x | 0.76 | x | 0.7 | = | 105.53 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 157.83 | x | 0.76 | x | 0.7 | = | 94.46  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 156.31 | x | 0.76 | x | 0.7 | = | 152.68 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 196.72 | x | 0.76 | x | 0.7 | = | 132.8  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 197.69 | x | 0.76 | x | 0.7 | = | 118.32 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 196.72 | x | 0.76 | x | 0.7 | = | 192.14 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 203.69 | x | 0.76 | x | 0.7 | = | 137.51 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 204.35 | x | 0.76 | x | 0.7 | = | 122.31 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 203.69 | x | 0.76 | x | 0.7 | = | 198.95 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 192.96 | x | 0.76 | x | 0.7 | = | 130.27 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 193.73 | x | 0.76 | x | 0.7 | = | 115.95 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 192.96 | x | 0.76 | x | 0.7 | = | 188.48 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 162.28 | x | 0.76 | x | 0.7 | = | 109.56 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 163.49 | x | 0.76 | x | 0.7 | = | 97.85  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 162.28 | x | 0.76 | x | 0.7 | = | 158.51 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 121.97 | x | 0.76 | x | 0.7 | = | 82.35  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 123.75 | x | 0.76 | x | 0.7 | = | 74.06  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 121.97 | x | 0.76 | x | 0.7 | = | 119.14 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 72.85  | x | 0.76 | x | 0.7 | = | 49.18  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 74.68  | x | 0.76 | x | 0.7 | = | 44.69  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 72.85  | x | 0.76 | x | 0.7 | = | 71.15  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 38.04  | x | 0.76 | x | 0.7 | = | 25.68  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 39.41  | x | 0.76 | x | 0.7 | = | 23.59  | (82) |



# SAP WorkSheet: New dwelling design stage

## 9a. Energy requirements – Individual heating systems including micro-CHP)

### Space heating:

Fraction of space heat from secondary/supplementary system

0 (201)

Fraction of space heat from main system(s)

(202) = 1 - (201) =  
1 (202)

Fraction of total heating from main system 1

(204) = (202) × [1 - (203)] =  
1 (204)

Efficiency of main space heating system 1

237.4 (206)

Efficiency of secondary/supplementary heating system, %

0 (208)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |          |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------|
|     |     |     |     |     |     |     |     |     |     |     |     | kWh/year |

Space heating requirement (calculated above)

|        |        |        |       |       |   |   |   |   |        |        |        |  |
|--------|--------|--------|-------|-------|---|---|---|---|--------|--------|--------|--|
| 799.45 | 593.47 | 430.31 | 173.9 | 45.11 | 0 | 0 | 0 | 0 | 235.32 | 547.39 | 828.62 |  |
|--------|--------|--------|-------|-------|---|---|---|---|--------|--------|--------|--|

(211)m = {[ (98)m × (204) ] } × 100 ÷ (206) (211)

|        |        |        |       |    |   |   |   |   |       |        |        |  |
|--------|--------|--------|-------|----|---|---|---|---|-------|--------|--------|--|
| 336.75 | 249.98 | 181.26 | 73.25 | 19 | 0 | 0 | 0 | 0 | 99.12 | 230.58 | 349.03 |  |
|--------|--------|--------|-------|----|---|---|---|---|-------|--------|--------|--|

Total (kWh/year) = Sum(211)<sub>1...5,10...12</sub> = 1538.97 (211)

Space heating fuel (secondary), kWh/month

= {[ (98)m × (201) ] } × 100 ÷ (208)

|   |   |   |   |   |   |   |   |   |   |   |   |  |
|---|---|---|---|---|---|---|---|---|---|---|---|--|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|---|---|---|---|---|---|---|---|---|---|---|---|--|

Total (kWh/year) = Sum(215)<sub>1...5,10...12</sub> = 0 (215)

### Water heating

Output from water heater (calculated above)

|        |        |        |        |        |        |        |        |        |        |        |        |  |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|
| 202.97 | 178.85 | 187.71 | 168.11 | 164.62 | 146.92 | 140.94 | 154.88 | 154.68 | 174.32 | 184.54 | 198.03 |  |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|

Efficiency of water heater

119.34 (216)

|        |        |        |        |        |        |        |        |        |        |        |        |  |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|
| 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 |  |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|

Fuel for water heating, kWh/month

(219)m = (64)m × 100 ÷ (217)m

|        |        |        |        |        |        |       |        |        |        |        |        |  |
|--------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|--|
| 170.07 | 149.86 | 157.29 | 140.86 | 137.94 | 123.11 | 118.1 | 129.78 | 129.61 | 146.07 | 154.63 | 165.94 |  |
|--------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|--|

Total = Sum(219a)<sub>1...12</sub> = 1723.29 (219)

### Annual totals

Space heating fuel used, main system 1

kWh/year

1538.97

Water heating fuel used

1723.29

Electricity for pumps, fans and electric keep-hot

Total electricity for the above, kWh/year sum of (230a)...(230g) = 0 (231)

Electricity for lighting 371.02 (232)

## 10a. Fuel costs - individual heating systems:

|  | Fuel<br>kWh/year | Fuel Price<br>(Table 12) | Fuel Cost<br>£/year   |
|--|------------------|--------------------------|-----------------------|
| Space heating - main system 1  | (211) ×          | 13.19                    | x 0.01 = 202.99 (240) |
| Space heating - main system 2  | (213) ×          | 0                        | x 0.01 = 0 (241)      |
| Space heating - secondary  | (215) ×          | 13.19                    | x 0.01 = 0 (242)      |
| Water heating cost (other fuel)  | (219)            | 13.19                    | x 0.01 = 227.3 (247)  |
| Pumps, fans and electric keep-hot  | (231)            | 13.19                    | x 0.01 = 0 (249)      |
| (if off-peak tariff, list each of (230a) to (230g) separately as applicable and apply fuel price according to Table 12a) |                  |                          |                       |
| Energy for lighting  | (232)            | 13.19                    | x 0.01 = 48.94 (250)  |

# SAP WorkSheet: New dwelling design stage

Additional standing charges (Table 12)

0 (251)

Appendix Q items: repeat lines (253) and (254) as needed

**Total energy cost**  $(245)\dots(247) + (250)\dots(254) =$

479.23 (255)

## 11a. SAP rating - individual heating systems

Energy cost deflator (Table 12)

0.42 (256)

Energy cost factor (ECF)  $[(255) \times (256)] \div [(4) + 45.0] =$

1.51 (257)

## SAP rating (Section 12)

78.91 (258)

## 12a. CO2 emissions – Individual heating systems including micro-CHP

|   | Energy<br>kWh/year              | Emission factor<br>kg CO2/kWh | Emissions<br>kg CO2/year            |
|---|---------------------------------|-------------------------------|-------------------------------------|
| Space heating (main system 1)                     | (211) x                         | <input type="text"/> 0.519    | <input type="text"/> = 798.73 (261) |
| Space heating (secondary)                         | (215) x                         | <input type="text"/> 0.519    | <input type="text"/> = 0 (263)      |
| Water heating                                     | (219) x                         | <input type="text"/> 0.519    | <input type="text"/> = 894.39 (264) |
| Space and water heating                           | (261) + (262) + (263) + (264) = |                               | <input type="text"/> 1693.11 (265)  |
| Electricity for pumps, fans and electric keep-hot | (231) x                         | <input type="text"/> 0.519    | <input type="text"/> = 0 (267)      |
| Electricity for lighting                          | (232) x                         | <input type="text"/> 0.519    | <input type="text"/> = 192.56 (268) |
| Total CO2, kg/year                                |                                 | sum of (265)...(271) =        | <input type="text"/> 1885.67 (272)  |
| <b>CO2 emissions per m<sup>2</sup></b>            |                                 | (272) ÷ (4) =                 | <input type="text"/> 21.39 (273)    |
| EI rating (section 14)                            |                                 |                               | <input type="text"/> 81 (274)       |

## 13a. Primary Energy

|   | Energy<br>kWh/year              | Primary<br>factor         | P. Energy<br>kWh/year                |
|---|---------------------------------|---------------------------|--------------------------------------|
| Space heating (main system 1)                     | (211) x                         | <input type="text"/> 3.07 | <input type="text"/> = 4724.64 (261) |
| Space heating (secondary)                         | (215) x                         | <input type="text"/> 3.07 | <input type="text"/> = 0 (263)       |
| Energy for water heating                          | (219) x                         | <input type="text"/> 3.07 | <input type="text"/> = 5290.49 (264) |
| Space and water heating                           | (261) + (262) + (263) + (264) = |                           | <input type="text"/> 10015.13 (265)  |
| Electricity for pumps, fans and electric keep-hot | (231) x                         | <input type="text"/> 3.07 | <input type="text"/> = 0 (267)       |
| Electricity for lighting                          | (232) x                         | <input type="text"/> 0    | <input type="text"/> = 1139.02 (268) |
| 'Total Primary Energy                             |                                 | sum of (265)...(271) =    | <input type="text"/> 11154.15 (272)  |
| <b>Primary energy kWh/m<sup>2</sup>/year</b>      |                                 | (272) ÷ (4) =             | <input type="text"/> 126.52 (273)    |

# TFEE WorkSheet: New dwelling design stage

## User Details:

|                                     |                  |                          |                   |
|-------------------------------------|------------------|--------------------------|-------------------|
| <b>Assessor Name:</b>               | Peter Mitchell   | <b>Stroma Number:</b>    | STRO007945        |
| <b>Software Name:</b>               | Stroma FSAP 2012 | <b>Software Version:</b> | Version: 1.0.4.25 |
| Property Address: Unit 1 Clean ASHP |                  |                          |                   |

## Address :

1. Overall dwelling dimensions:

|   | <b>Area(m<sup>2</sup>)</b> | <b>Av. Height(m)</b>                 | <b>Volume(m<sup>3</sup>)</b> |
|---|----------------------------|--------------------------------------|------------------------------|
| Ground floor  | 52.9<br>(1a) x             | 2.37<br>(2a)                         | 125.37<br>(3a)               |
| First floor   | 35.26<br>(1b) x            | 2.56<br>(2b)                         | 90.27<br>(3b)                |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n) | 88.16<br>(4)               |                                      |                              |
| Dwelling volume   |                            | (3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) = | 215.64<br>(5)                |

2. Ventilation rate:

|                              | <b>main heating</b> | <b>secondary heating</b> | <b>other</b> | <b>total</b> | <b>m<sup>3</sup> per hour</b> |
|------------------------------|---------------------|--------------------------|--------------|--------------|-------------------------------|
| Number of chimneys           | 0                   | +                        | 0            | = 0          | x 40 = 0<br>(6a)              |
| Number of open flues         | 0                   | +                        | 0            | = 0          | x 20 = 0<br>(6b)              |
| Number of intermittent fans  |                     |                          |              | 3            | x 10 = 30<br>(7a)             |
| Number of passive vents      |                     |                          |              | 0            | x 10 = 0<br>(7b)              |
| Number of flueless gas fires |                     |                          |              | 0            | x 40 = 0<br>(7c)              |

## Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = 30 ÷ (5) = 0.14 (8)

If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)

Number of storeys in the dwelling (ns)

Additional infiltration

Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction

if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35

If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0

If no draught lobby, enter 0.05, else enter 0

Percentage of windows and doors draught stripped

Window infiltration  $0.25 - [0.2 \times (14) \div 100] =$

Infiltration rate  $(8) + (10) + (11) + (12) + (13) + (15) =$

Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area

If based on air permeability value, then (18) = [(17) ÷ 20]+(8), otherwise (18) = (16)

Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used

Number of sides sheltered

Shelter factor  $(20) = 1 - [0.075 \times (19)] =$

Infiltration rate incorporating shelter factor  $(21) = (18) \times (20) =$

Infiltration rate modified for monthly wind speed

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Monthly average wind speed from Table 7

|        |     |   |     |     |     |     |     |     |   |     |     |     |
|--------|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|
| (22)m= | 5.1 | 5 | 4.9 | 4.4 | 4.3 | 3.8 | 3.8 | 3.7 | 4 | 4.3 | 4.5 | 4.7 |
|--------|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|

# Tfee Worksheet: New dwelling design stage

Wind Factor (22a)m = (22)m ÷ 4

|         |      |      |      |     |      |      |      |      |   |      |      |      |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|
| (22a)m= | 1.27 | 1.25 | 1.23 | 1.1 | 1.08 | 0.95 | 0.95 | 0.92 | 1 | 1.08 | 1.12 | 1.18 |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|

Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 0.42 | 0.41 | 0.41 | 0.36 | 0.36 | 0.31 | 0.31 | 0.31 | 0.33 | 0.36 | 0.37 | 0.39 |
|------|------|------|------|------|------|------|------|------|------|------|------|

Calculate effective air change rate for the applicable case

If mechanical ventilation:

|   |       |
|---|-------|
| 0 | (23a) |
|---|-------|

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

|   |       |
|---|-------|
| 0 | (23b) |
|---|-------|

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

|   |       |
|---|-------|
| 0 | (23c) |
|---|-------|

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24a)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24a)

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24b)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24b)

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b)m + 0.5 × (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24c)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24c)

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² × 0.5]

|         |      |      |      |      |      |      |      |      |      |      |      |      |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|
| (24d)m= | 0.59 | 0.59 | 0.58 | 0.57 | 0.56 | 0.55 | 0.55 | 0.55 | 0.56 | 0.57 | 0.58 | 0.58 |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|

(24d)

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

|        |      |      |      |      |      |      |      |      |      |      |      |      |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|
| (25)m= | 0.59 | 0.59 | 0.58 | 0.57 | 0.56 | 0.55 | 0.55 | 0.55 | 0.56 | 0.57 | 0.58 | 0.58 |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|

(25)

### 3. Heat losses and heat loss parameter:

| ELEMENT                                | Gross area (m <sup>2</sup> ) | Openings m <sup>2</sup> | Net Area A ,m <sup>2</sup> | U-value W/m <sup>2</sup> K | A X U (W/K) | k-value kJ/m <sup>2</sup> ·K | A X k kJ/K |
|--|------------------------------|-------------------------|----------------------------|----------------------------|-------------|------------------------------|------------|
| Windows Type 1                         |                              |                         | 6.01                       | x1/[1/( 1.4 )+ 0.04] =     | 7.97        |                              | (27)       |
| Windows Type 2                         |                              |                         | 6.3                        | x1/[1/( 1.4 )+ 0.04] =     | 8.35        |                              | (27)       |
| Windows Type 3                         |                              |                         | 1.59                       | x1/[1/( 1.4 )+ 0.04] =     | 2.11        |                              | (27)       |
| Windows Type 4                         |                              |                         | 0.61                       | x1/[1/( 1.4 )+ 0.04] =     | 0.81        |                              | (27)       |
| Rooflights Type 1                      |                              |                         | 1.41                       | x1/[1/(1.7) + 0.04] =      | 2.397       |                              | (27b)      |
| Rooflights Type 2                      |                              |                         | 1.25                       | x1/[1/(1.7) + 0.04] =      | 2.125       |                              | (27b)      |
| Rooflights Type 3                      |                              |                         | 2.04                       | x1/[1/(1.7) + 0.04] =      | 3.468       |                              | (27b)      |
| Floor                                  |                              |                         | 52.9                       | x 0.13 =                   | 6.877       |                              | (28)       |
| Walls                                  | 109.46                       | 16.71                   | 92.75                      | x 0.18 =                   | 16.7        |                              | (29)       |
| Roof Type1                             | 35.52                        | 1.25                    | 34.27                      | x 0.13 =                   | 4.46        |                              | (30)       |
| Roof Type2                             | 17.86                        | 3.45                    | 14.41                      | x 0.13 =                   | 1.87        |                              | (30)       |
| Total area of elements, m <sup>2</sup> |                              |                         | 215.74                     |                            |             |                              | (31)       |
| Party wall                             |                              |                         | 32.84                      | x 0 =                      | 0           |                              | (32)       |

\* for windows and roof windows, use effective window U-value calculated using formula  $1/[(1/U\text{-value})+0.04]$  as given in paragraph 3.2

\*\* include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = 59.54 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) = 0 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m<sup>2</sup>K Indicative Value: Medium 250 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f

# Tfee Worksheet: New dwelling design stage

can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K

13.12 (36)

if details of thermal bridging are not known (36) =  $0.05 \times (31)$

Total fabric heat loss

$(33) + (36) =$

72.66 (37)

Ventilation heat loss calculated monthly

$(38)m = 0.33 \times (25)m \times (5)$

| Jan          | Feb   | Mar   | Apr   | May   | Jun   | Jul   | Aug   | Sep   | Oct   | Nov   | Dec   |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| (38)m= 41.91 | 41.66 | 41.42 | 40.29 | 40.08 | 39.09 | 39.09 | 38.91 | 39.47 | 40.08 | 40.51 | 40.95 |

(38)

Heat transfer coefficient, W/K

$(39)m = (37) + (38)m$

|  |        |        |        |        |        |        |        |        |        |        |             |
|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------------|
| (39)m= 114.57  | 114.32 | 114.08 | 112.95 | 112.74 | 111.75 | 111.75 | 111.57 | 112.13 | 112.74 | 113.17 | 113.61      |
| $\text{Average} = \text{Sum}(39)_{1\dots 12} / 12 =$ |        |        |        |        |        |        |        |        |        |        | 112.95 (39) |

Heat loss parameter (HLP), W/m<sup>2</sup>K

$(40)m = (39)m \div (4)$

|  |     |      |      |      |      |      |      |      |      |      |           |
|--|-----|------|------|------|------|------|------|------|------|------|-----------|
| (40)m= 1.3   | 1.3 | 1.29 | 1.28 | 1.28 | 1.27 | 1.27 | 1.27 | 1.27 | 1.28 | 1.28 | 1.29      |
| $\text{Average} = \text{Sum}(40)_{1\dots 12} / 12 =$ |     |      |      |      |      |      |      |      |      |      | 1.28 (40) |

Number of days in month (Table 1a)

| Jan       | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| (41)m= 31 | 28  | 31  | 30  | 31  | 30  | 31  | 31  | 30  | 31  | 30  | 31  |

(41)

4. Water heating energy requirement:

kWh/year:

Assumed occupancy, N

2.6 (42)

if TFA > 13.9,  $N = 1 + 1.76 \times [1 - \exp(-0.000349 \times (\text{TFA} - 13.9)2)] + 0.0013 \times (\text{TFA} - 13.9)$

if TFA £ 13.9,  $N = 1$

Annual average hot water usage in litres per day  $Vd,\text{average} = (25 \times N) + 36$

95.94 (43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Hot water usage in litres per day for each month  $Vd,m = \text{factor from Table 1c} \times (43)$

|   |       |       |       |       |       |       |       |       |       |       |              |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------------|
| (44)m= 105.54                                 | 101.7 | 97.86 | 94.02 | 90.19 | 86.35 | 86.35 | 90.19 | 94.02 | 97.86 | 101.7 | 105.54       |
| $\text{Total} = \text{Sum}(44)_{1\dots 12} =$ |       |       |       |       |       |       |       |       |       |       | 1151.31 (44) |

Energy content of hot water used - calculated monthly =  $4.190 \times Vd,m \times nm \times DTm / 3600 \text{ kWh/month}$  (see Tables 1b, 1c, 1d)

|   |        |        |        |        |        |       |        |        |        |        |              |
|---|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------------|
| (45)m= 156.51                                 | 136.88 | 141.25 | 123.15 | 118.16 | 101.96 | 94.49 | 108.42 | 109.72 | 127.87 | 139.58 | 151.57       |
| $\text{Total} = \text{Sum}(45)_{1\dots 12} =$ |        |        |        |        |        |       |        |        |        |        | 1509.55 (45) |

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

|          |   |   |   |   |   |   |   |   |   |   |   |
|----------|---|---|---|---|---|---|---|---|---|---|---|
| (46)m= 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|----------|---|---|---|---|---|---|---|---|---|---|---|

(46)

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel  150 (47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

a) If manufacturer's declared loss factor is known (kWh/day):  0 (48)

Temperature factor from Table 2b  0 (49)

Energy lost from water storage, kWh/year  $(48) \times (49) =$   0 (50)

b) If manufacturer's declared cylinder loss factor is not known:  0 (51)

Hot water storage loss factor from Table 2 (kWh/litre/day)  0 (52)

If community heating see section 4.3  0 (53)

Volume factor from Table 2a  0 (52)

Temperature factor from Table 2b  0 (53)

# TFFEE WorkSheet: New dwelling design stage

Energy lost from water storage, kWh/year  $(47) \times (51) \times (52) \times (53) =$  0 (54)

Enter (50) or (54) in (55) 0 (55)

Water storage loss calculated for each month  $((56)m = (55) \times (41)m$

$(56)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (56)

If cylinder contains dedicated solar storage,  $(57)m = (56)m \times [(50) - (H11)] \div (50)$ , else  $(57)m = (56)m$  where (H11) is from Appendix H

$(57)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (57)

Primary circuit loss (annual) from Table 3 0 (58)

Primary circuit loss calculated for each month  $(59)m = (58) \div 365 \times (41)m$

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)  $(59)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (59)

Combi loss calculated for each month  $(61)m = (60) \div 365 \times (41)m$

$(61)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (61)

Total heat required for water heating calculated for each month  $(62)m = 0.85 \times (45)m + (46)m + (57)m + (59)m + (61)m$

$(62)m =$  133.03 116.35 120.06 104.67 100.44 86.67 80.31 92.16 93.26 108.69 118.64 128.83 (62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)  $(63)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (63)

Output from water heater  $(64)m =$  133.03 116.35 120.06 104.67 100.44 86.67 80.31 92.16 93.26 108.69 118.64 128.83 Output from water heater (annual) 1...12 1283.12 (64)

Heat gains from water heating, kWh/month  $0.25' [0.85 \times (45)m + (61)m] + 0.8 \times [(46)m + (57)m + (59)m]$   $(65)m =$  33.26 29.09 30.02 26.17 25.11 21.67 20.08 23.04 23.32 27.17 29.66 32.21 (65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

## 5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts  $(66)m =$  Jan Feb Mar Apr May Jun Jul Aug Sep Oct Nov Dec 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 (66)

$(66)m =$  129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 (66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5  $(67)m =$  21.01 18.66 15.17 11.49 8.59 7.25 7.83 10.18 13.67 17.35 20.25 21.59 (67)

$(67)m =$  21.01 18.66 15.17 11.49 8.59 7.25 7.83 10.18 13.67 17.35 20.25 21.59 (67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5  $(68)m =$  235.65 238.1 231.93 218.82 202.26 186.69 176.3 173.85 180.01 193.13 209.69 225.25 (68)

$(68)m =$  235.65 238.1 231.93 218.82 202.26 186.69 176.3 173.85 180.01 193.13 209.69 225.25 (68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5  $(69)m =$  36 36 36 36 36 36 36 36 36 36 36 36 (69)

$(69)m =$  36 36 36 36 36 36 36 36 36 36 36 36 (69)

Pumps and fans gains (Table 5a)  $(70)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (70)

$(70)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (70)

Losses e.g. evaporation (negative values) (Table 5)  $(71)m =$  -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 (71)

$(71)m =$  -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 (71)

Water heating gains (Table 5)  $(72)m =$  44.7 43.29 40.34 36.35 33.75 30.09 26.99 30.97 32.38 36.52 41.19 43.29 (72)

$(72)m =$  44.7 43.29 40.34 36.35 33.75 30.09 26.99 30.97 32.38 36.52 41.19 43.29 (72)

**Total internal gains =**  $(66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m$

$(73)m =$  363.36 362.04 349.45 328.65 306.59 286.03 273.11 277 288.06 309 333.13 352.13 (73)

## 6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

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| Orientation: | Access Factor<br>Table 6d | Area<br>m <sup>2</sup> | Flux<br>Table 6a | g<br>Table 6b | FF<br>Table 6c | Gains<br>(W)  |
|--------------|---------------------------|------------------------|------------------|---------------|----------------|---------------|
| North        | 0.9x 0.77                 | x 6.01                 | x 10.63          | x 0.63        | x 0.7          | = 19.53 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 10.63          | x 0.63        | x 0.7          | = 20.47 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 10.63          | x 0.63        | x 0.7          | = 10.33 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 20.32          | x 0.63        | x 0.7          | = 37.32 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 20.32          | x 0.63        | x 0.7          | = 39.13 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 20.32          | x 0.63        | x 0.7          | = 19.75 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 34.53          | x 0.63        | x 0.7          | = 63.42 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 34.53          | x 0.63        | x 0.7          | = 66.48 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 34.53          | x 0.63        | x 0.7          | = 33.56 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 55.46          | x 0.63        | x 0.7          | = 101.87 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 55.46          | x 0.63        | x 0.7          | = 106.79 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 55.46          | x 0.63        | x 0.7          | = 53.9 (74)   |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.72          | x 0.63        | x 0.7          | = 137.23 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.72          | x 0.63        | x 0.7          | = 143.85 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.72          | x 0.63        | x 0.7          | = 72.61 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 79.99          | x 0.63        | x 0.7          | = 146.91 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 79.99          | x 0.63        | x 0.7          | = 154 (74)    |
| North        | 0.9x 0.77                 | x 1.59                 | x 79.99          | x 0.63        | x 0.7          | = 77.73 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.68          | x 0.63        | x 0.7          | = 137.16 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.68          | x 0.63        | x 0.7          | = 143.78 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.68          | x 0.63        | x 0.7          | = 72.57 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 59.25          | x 0.63        | x 0.7          | = 108.82 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 59.25          | x 0.63        | x 0.7          | = 114.07 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 59.25          | x 0.63        | x 0.7          | = 57.58 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 41.52          | x 0.63        | x 0.7          | = 76.25 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 41.52          | x 0.63        | x 0.7          | = 79.93 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 41.52          | x 0.63        | x 0.7          | = 40.35 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 24.19          | x 0.63        | x 0.7          | = 44.43 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 24.19          | x 0.63        | x 0.7          | = 46.57 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 24.19          | x 0.63        | x 0.7          | = 23.51 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 13.12          | x 0.63        | x 0.7          | = 24.09 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 13.12          | x 0.63        | x 0.7          | = 25.26 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 13.12          | x 0.63        | x 0.7          | = 12.75 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 8.86           | x 0.63        | x 0.7          | = 16.28 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 8.86           | x 0.63        | x 0.7          | = 17.07 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 8.86           | x 0.63        | x 0.7          | = 8.61 (74)   |
| South        | 0.9x 0.77                 | x 0.61                 | x 46.75          | x 0.63        | x 0.7          | = 17.43 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 76.57          | x 0.63        | x 0.7          | = 28.55 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 97.53          | x 0.63        | x 0.7          | = 36.37 (78)  |

# TFEE WorkSheet: New dwelling design stage

|            |      |      |   |      |   |        |   |      |   |     |   |        |      |
|------------|------|------|---|------|---|--------|---|------|---|-----|---|--------|------|
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.23 | x | 0.63 | x | 0.7 | = | 41.1   | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 114.87 | x | 0.63 | x | 0.7 | = | 42.83  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.55 | x | 0.63 | x | 0.7 | = | 41.22  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 108.01 | x | 0.63 | x | 0.7 | = | 40.27  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 104.89 | x | 0.63 | x | 0.7 | = | 39.11  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 101.89 | x | 0.63 | x | 0.7 | = | 37.99  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 82.59  | x | 0.63 | x | 0.7 | = | 30.79  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 55.42  | x | 0.63 | x | 0.7 | = | 20.66  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 40.4   | x | 0.63 | x | 0.7 | = | 15.06  | (78) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 30.32  | x | 0.63 | x | 0.7 | = | 16.97  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 31.5   | x | 0.63 | x | 0.7 | = | 15.63  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 30.32  | x | 0.63 | x | 0.7 | = | 24.55  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 60.64  | x | 0.63 | x | 0.7 | = | 33.93  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 62.43  | x | 0.63 | x | 0.7 | = | 30.97  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 60.64  | x | 0.63 | x | 0.7 | = | 49.1   | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 103.31 | x | 0.63 | x | 0.7 | = | 57.82  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 105.22 | x | 0.63 | x | 0.7 | = | 52.2   | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 103.31 | x | 0.63 | x | 0.7 | = | 83.65  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 156.31 | x | 0.63 | x | 0.7 | = | 87.48  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 157.83 | x | 0.63 | x | 0.7 | = | 78.3   | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 156.31 | x | 0.63 | x | 0.7 | = | 126.56 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 196.72 | x | 0.63 | x | 0.7 | = | 110.09 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 197.69 | x | 0.63 | x | 0.7 | = | 98.08  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 196.72 | x | 0.63 | x | 0.7 | = | 159.28 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 203.69 | x | 0.63 | x | 0.7 | = | 113.99 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 204.35 | x | 0.63 | x | 0.7 | = | 101.38 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 203.69 | x | 0.63 | x | 0.7 | = | 164.92 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 192.96 | x | 0.63 | x | 0.7 | = | 107.99 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 193.73 | x | 0.63 | x | 0.7 | = | 96.12  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 192.96 | x | 0.63 | x | 0.7 | = | 156.24 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 162.28 | x | 0.63 | x | 0.7 | = | 90.82  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 163.49 | x | 0.63 | x | 0.7 | = | 81.11  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 162.28 | x | 0.63 | x | 0.7 | = | 131.4  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 121.97 | x | 0.63 | x | 0.7 | = | 68.26  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 123.75 | x | 0.63 | x | 0.7 | = | 61.39  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 121.97 | x | 0.63 | x | 0.7 | = | 98.76  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 72.85  | x | 0.63 | x | 0.7 | = | 40.77  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 74.68  | x | 0.63 | x | 0.7 | = | 37.05  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 72.85  | x | 0.63 | x | 0.7 | = | 58.98  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 38.04  | x | 0.63 | x | 0.7 | = | 21.29  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 39.41  | x | 0.63 | x | 0.7 | = | 19.55  | (82) |



## TFEE WorkSheet: New dwelling design stage

### 8c. Space cooling requirement

Calculated for June, July and August. See Table 10b

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Heat loss rate Lm (calculated using 25°C internal temperature and external temperature from Table 10)

|         |   |   |   |   |   |         |        |        |   |   |   |   |       |
|---------|---|---|---|---|---|---------|--------|--------|---|---|---|---|-------|
| (100)m= | 0 | 0 | 0 | 0 | 0 | 1050.47 | 826.96 | 847.93 | 0 | 0 | 0 | 0 | (100) |
|---------|---|---|---|---|---|---------|--------|--------|---|---|---|---|-------|

Utilisation factor for loss hm

|         |   |   |   |   |   |     |      |      |   |   |   |   |       |
|---------|---|---|---|---|---|-----|------|------|---|---|---|---|-------|
| (101)m= | 0 | 0 | 0 | 0 | 0 | 0.9 | 0.94 | 0.91 | 0 | 0 | 0 | 0 | (101) |
|---------|---|---|---|---|---|-----|------|------|---|---|---|---|-------|

Useful loss, hmLm (Watts) = (100)m x (101)m

|         |   |   |   |   |   |        |        |        |   |   |   |   |       |
|---------|---|---|---|---|---|--------|--------|--------|---|---|---|---|-------|
| (102)m= | 0 | 0 | 0 | 0 | 0 | 944.36 | 779.85 | 772.51 | 0 | 0 | 0 | 0 | (102) |
|---------|---|---|---|---|---|--------|--------|--------|---|---|---|---|-------|

Gains (solar gains calculated for applicable weather region, see Table 10)

|         |   |   |   |   |   |        |        |         |   |   |   |   |       |
|---------|---|---|---|---|---|--------|--------|---------|---|---|---|---|-------|
| (103)m= | 0 | 0 | 0 | 0 | 0 | 1303.1 | 1235.5 | 1097.95 | 0 | 0 | 0 | 0 | (103) |
|---------|---|---|---|---|---|--------|--------|---------|---|---|---|---|-------|

Space cooling requirement for month, whole dwelling, continuous ( kWh) =  $0.024 \times [(103)m - (102)m] \times (41)m$   
set (104)m to zero if (104)m <  $3 \times (98)m$

|         |                                   |   |   |   |   |        |     |        |   |   |   |   |                                 |
|---------|-----------------------------------|---|---|---|---|--------|-----|--------|---|---|---|---|---------------------------------|
| (104)m= | 0                                 | 0 | 0 | 0 | 0 | 258.29 | 339 | 242.13 | 0 | 0 | 0 | 0 | Total = Sum(104) = 839.43 (104) |
|         | f C = cooled area ÷ (4) = 1 (105) |   |   |   |   |        |     |        |   |   |   |   |                                 |

Cooled fraction

Intermittency factor (Table 10b)

|         |   |   |   |   |   |      |      |      |   |   |   |   |                            |
|---------|---|---|---|---|---|------|------|------|---|---|---|---|----------------------------|
| (106)m= | 0 | 0 | 0 | 0 | 0 | 0.25 | 0.25 | 0.25 | 0 | 0 | 0 | 0 | Total = Sum(106) = 0 (106) |
|---------|---|---|---|---|---|------|------|------|---|---|---|---|----------------------------|

Space cooling requirement for month = (104)m × (105) × (106)m

|         |                          |   |   |   |   |       |       |       |   |   |   |   |                                 |
|---------|--------------------------|---|---|---|---|-------|-------|-------|---|---|---|---|---------------------------------|
| (107)m= | 0                        | 0 | 0 | 0 | 0 | 64.57 | 84.75 | 60.53 | 0 | 0 | 0 | 0 | Total = Sum(107) = 209.86 (107) |
|         | (107) ÷ (4) = 2.38 (108) |   |   |   |   |       |       |       |   |   |   |   |                                 |

### 8f. Fabric Energy Efficiency (calculated only under special conditions, see section 11)

Fabric Energy Efficiency  $(99) + (108) = 53.37$  (109)

Target Fabric Energy Efficiency (TFEE)  $61.38$  (109)

# DFEE WorkSheet: New dwelling design stage

## User Details:

|                       |                  |                          |                   |
|-----------------------|------------------|--------------------------|-------------------|
| <b>Assessor Name:</b> | Peter Mitchell   | <b>Stroma Number:</b>    | STRO007945        |
| <b>Software Name:</b> | Stroma FSAP 2012 | <b>Software Version:</b> | Version: 1.0.4.25 |

Property Address: Unit 1 Clean ASHP

## Address :

1. Overall dwelling dimensions:

|   | <b>Area(m<sup>2</sup>)</b> | <b>Av. Height(m)</b>                 | <b>Volume(m<sup>3</sup>)</b> |
|---|----------------------------|--------------------------------------|------------------------------|
| Ground floor  | 52.9<br>(1a)               | x<br>(2a)                            | = 125.37<br>(3a)             |
| First floor   | 35.26<br>(1b)              | x<br>(2b)                            | = 90.27<br>(3b)              |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n) | 88.16<br>(4)               |                                      |                              |
| Dwelling volume   |                            | (3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) = | 215.64<br>(5)                |

2. Ventilation rate:

|                              | <b>main heating</b> | <b>secondary heating</b> | <b>other</b> | <b>total</b> | <b>m<sup>3</sup> per hour</b> |
|------------------------------|---------------------|--------------------------|--------------|--------------|-------------------------------|
| Number of chimneys           | 0                   | +                        | 0            | +            | 0 = 0 x 40 = 0<br>(6a)        |
| Number of open flues         | 0                   | +                        | 0            | +            | 0 = 0 x 20 = 0<br>(6b)        |
| Number of intermittent fans  |                     |                          |              |              | x 10 = 3<br>(7a)              |
| Number of passive vents      |                     |                          |              |              | x 10 = 0<br>(7b)              |
| Number of flueless gas fires |                     |                          |              |              | x 40 = 0<br>(7c)              |

## Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = 20 ÷ (5) = 0.09 (8)

If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)

Number of storeys in the dwelling (ns)

Additional infiltration

[(9)-1]x0.1 = 0  
(9)

Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction

if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35

If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0

If no draught lobby, enter 0.05, else enter 0

Percentage of windows and doors draught stripped

Window infiltration       $0.25 - [0.2 \times (14) \div 100] = 0$

Infiltration rate       $(8) + (10) + (11) + (12) + (13) + (15) = 0$

Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area

If based on air permeability value, then (18) = [(17) ÷ 20]+(8), otherwise (18) = (16)

Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used

Number of sides sheltered

Shelter factor       $(20) = 1 - [0.075 \times (19)] = 0.85$

Infiltration rate incorporating shelter factor       $(21) = (18) \times (20) = 0.29$

Infiltration rate modified for monthly wind speed

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Monthly average wind speed from Table 7

|        |     |   |     |     |     |     |     |     |   |     |     |     |
|--------|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|
| (22)m= | 5.1 | 5 | 4.9 | 4.4 | 4.3 | 3.8 | 3.8 | 3.7 | 4 | 4.3 | 4.5 | 4.7 |
|--------|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|

# DFEE WorkSheet: New dwelling design stage

Wind Factor (22a)m = (22)m ÷ 4

|         |      |      |      |     |      |      |      |      |   |      |      |      |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|
| (22a)m= | 1.27 | 1.25 | 1.23 | 1.1 | 1.08 | 0.95 | 0.95 | 0.92 | 1 | 1.08 | 1.12 | 1.18 |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|

Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 0.37 | 0.36 | 0.36 | 0.32 | 0.31 | 0.28 | 0.28 | 0.27 | 0.29 | 0.31 | 0.33 | 0.34 |
|------|------|------|------|------|------|------|------|------|------|------|------|

Calculate effective air change rate for the applicable case

If mechanical ventilation:

0 (23a)

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

0 (23b)

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

0 (23c)

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24a)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24b)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b)m + 0.5 × (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24c)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² × 0.5]

|         |      |      |      |      |      |      |      |      |      |      |      |      |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|
| (24d)m= | 0.57 | 0.57 | 0.56 | 0.55 | 0.55 | 0.54 | 0.54 | 0.54 | 0.54 | 0.55 | 0.55 | 0.56 |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

|        |      |      |      |      |      |      |      |      |      |      |      |      |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|
| (25)m= | 0.57 | 0.57 | 0.56 | 0.55 | 0.55 | 0.54 | 0.54 | 0.54 | 0.54 | 0.55 | 0.55 | 0.56 |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|

## 3. Heat losses and heat loss parameter:

| ELEMENT                                | Gross area (m <sup>2</sup> ) | Openings m <sup>2</sup> | Net Area A ,m <sup>2</sup> | U-value W/m <sup>2</sup> K | A X U (W/K) | k-value kJ/m <sup>2</sup> ·K | A X k kJ/K |
|--|------------------------------|-------------------------|----------------------------|----------------------------|-------------|------------------------------|------------|
| Windows Type 1                         |                              |                         | 6.01                       | x1/[1/( 1.2 )+ 0.04] =     | 6.88        |                              | (27)       |
| Windows Type 2                         |                              |                         | 6.3                        | x1/[1/( 1.2 )+ 0.04] =     | 7.21        |                              | (27)       |
| Windows Type 3                         |                              |                         | 1.59                       | x1/[1/( 1.2 )+ 0.04] =     | 1.82        |                              | (27)       |
| Windows Type 4                         |                              |                         | 0.61                       | x1/[1/( 1.2 )+ 0.04] =     | 0.7         |                              | (27)       |
| Rooflights Type 1                      |                              |                         | 1.41                       | x1/[1/(1.2) + 0.04] =      | 1.692       |                              | (27b)      |
| Rooflights Type 2                      |                              |                         | 1.25                       | x1/[1/(1.2) + 0.04] =      | 1.5         |                              | (27b)      |
| Rooflights Type 3                      |                              |                         | 2.04                       | x1/[1/(1.2) + 0.04] =      | 2.448       |                              | (27b)      |
| Floor                                  |                              |                         | 52.9                       | x 0.13 =                   | 6.877       |                              | (28)       |
| Walls                                  | 109.46                       | 16.71                   | 92.75                      | x 0.18 =                   | 16.7        |                              | (29)       |
| Roof Type1                             | 35.52                        | 1.25                    | 34.27                      | x 0.13 =                   | 4.46        |                              | (30)       |
| Roof Type2                             | 17.86                        | 3.45                    | 14.41                      | x 0.13 =                   | 1.87        |                              | (30)       |
| Total area of elements, m <sup>2</sup> |                              |                         | 215.74                     |                            |             |                              | (31)       |
| Party wall                             |                              |                         | 32.84                      | x 0 =                      | 0           |                              | (32)       |

\* for windows and roof windows, use effective window U-value calculated using formula  $1/[(1/U\text{-value})+0.04]$  as given in paragraph 3.2

\*\* include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = 54.42 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) = 0 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m<sup>2</sup>K Indicative Value: Medium 250 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f

# DFEE WorkSheet: New dwelling design stage

can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K

19.03 (36)

if details of thermal bridging are not known (36) =  $0.05 \times (31)$

Total fabric heat loss

$(33) + (36) =$

73.44 (37)

Ventilation heat loss calculated monthly

$(38)m = 0.33 \times (25)m \times (5)$

| Jan          | Feb  | Mar   | Apr   | May   | Jun   | Jul   | Aug   | Sep  | Oct   | Nov  | Dec   |
|--------------|------|-------|-------|-------|-------|-------|-------|------|-------|------|-------|
| (38)m= 40.49 | 40.3 | 40.11 | 39.23 | 39.07 | 38.31 | 38.31 | 38.16 | 38.6 | 39.07 | 39.4 | 39.75 |

(38)

Heat transfer coefficient, W/K

$(39)m = (37) + (38)m$

|  |        |        |        |        |        |        |        |        |        |        |        |
|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| (39)m= 113.93                              | 113.74 | 113.55 | 112.68 | 112.51 | 111.75 | 111.75 | 111.61 | 112.04 | 112.51 | 112.84 | 113.19 |
| Average = Sum(39) <sub>1...12</sub> / 12 = |        |        |        |        |        |        |        |        |        |        | 112.67 |

(39)

Heat loss parameter (HLP), W/m<sup>2</sup>K

$(40)m = (39)m \div (4)$

|  |      |      |      |      |      |      |      |      |      |      |      |
|--|------|------|------|------|------|------|------|------|------|------|------|
| (40)m= 1.29                                | 1.29 | 1.29 | 1.28 | 1.28 | 1.27 | 1.27 | 1.27 | 1.27 | 1.28 | 1.28 | 1.28 |
| Average = Sum(40) <sub>1...12</sub> / 12 = |      |      |      |      |      |      |      |      |      |      | 1.28 |

(40)

Number of days in month (Table 1a)

| Jan       | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| (41)m= 31 | 28  | 31  | 30  | 31  | 30  | 31  | 31  | 30  | 31  | 30  | 31  |

(41)

4. Water heating energy requirement:

kWh/year:

Assumed occupancy, N

2.6 (42)

if TFA > 13.9,  $N = 1 + 1.76 \times [1 - \exp(-0.000349 \times (\text{TFA} - 13.9)^2)] + 0.0013 \times (\text{TFA} - 13.9)$

if TFA £ 13.9,  $N = 1$

Annual average hot water usage in litres per day  $Vd,average = (25 \times N) + 36$

95.94 (43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Hot water usage in litres per day for each month  $Vd,m = \text{factor from Table 1c} \times (43)$

|                                     |       |       |       |       |       |       |       |       |       |       |         |
|-------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|
| (44)m= 105.54                       | 101.7 | 97.86 | 94.02 | 90.19 | 86.35 | 86.35 | 90.19 | 94.02 | 97.86 | 101.7 | 105.54  |
| Total = Sum(44) <sub>1...12</sub> = |       |       |       |       |       |       |       |       |       |       | 1151.31 |

(44)

Energy content of hot water used - calculated monthly =  $4.190 \times Vd,m \times nm \times DTm / 3600 \text{ kWh/month}$  (see Tables 1b, 1c, 1d)

|                                     |        |        |        |        |        |       |        |        |        |        |         |
|-------------------------------------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|---------|
| (45)m= 156.51                       | 136.88 | 141.25 | 123.15 | 118.16 | 101.96 | 94.49 | 108.42 | 109.72 | 127.87 | 139.58 | 151.57  |
| Total = Sum(45) <sub>1...12</sub> = |        |        |        |        |        |       |        |        |        |        | 1509.55 |

(45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

|          |   |   |   |   |   |   |   |   |   |   |   |
|----------|---|---|---|---|---|---|---|---|---|---|---|
| (46)m= 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|----------|---|---|---|---|---|---|---|---|---|---|---|

(46)

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel

120 (47)

(47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

a) If manufacturer's declared loss factor is known (kWh/day):

0 (48)

(48)

Temperature factor from Table 2b

0 (49)

(49)

Energy lost from water storage, kWh/year  $(48) \times (49) =$

0 (50)

(50)

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day)

0 (51)

(51)

If community heating see section 4.3

Volume factor from Table 2a

0 (52)

(52)

Temperature factor from Table 2b

0 (53)

(53)

# DFEE WorkSheet: New dwelling design stage

Energy lost from water storage, kWh/year  $(47) \times (51) \times (52) \times (53) =$  0 (54)

Enter (50) or (54) in (55) 0 (55)

Water storage loss calculated for each month  $((56)m = (55) \times (41)m$

$(56)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (56)

If cylinder contains dedicated solar storage,  $(57)m = (56)m \times [(50) - (H11)] \div (50)$ , else  $(57)m = (56)m$  where (H11) is from Appendix H

$(57)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (57)

Primary circuit loss (annual) from Table 3 0 (58)

Primary circuit loss calculated for each month  $(59)m = (58) \div 365 \times (41)m$

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat) (59)

$(59)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (59)

Combi loss calculated for each month  $(61)m = (60) \div 365 \times (41)m$

$(61)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (61)

Total heat required for water heating calculated for each month  $(62)m = 0.85 \times (45)m + (46)m + (57)m + (59)m + (61)m$

$(62)m =$  133.03 116.35 120.06 104.67 100.44 86.67 80.31 92.16 93.26 108.69 118.64 128.83 (62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)

$(63)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (63)

Output from water heater

$(64)m =$  133.03 116.35 120.06 104.67 100.44 86.67 80.31 92.16 93.26 108.69 118.64 128.83 Output from water heater (annual)  $1...12$  1283.12 (64)

Heat gains from water heating, kWh/month  $0.25 \times [0.85 \times (45)m + (61)m] + 0.8 \times [(46)m + (57)m + (59)m]$

$(65)m =$  33.26 29.09 30.02 26.17 25.11 21.67 20.08 23.04 23.32 27.17 29.66 32.21 (65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

## 5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

| Jan              | Feb    | Mar    | Apr    | May    | Jun    | Jul    | Aug    | Sep    | Oct    | Nov    | Dec    |
|------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| $(66)m =$ 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 |

(66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

$(67)m =$  21.01 18.66 15.17 11.49 8.59 7.25 7.83 10.18 13.67 17.35 20.25 21.59 (67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

$(68)m =$  235.65 238.1 231.93 218.82 202.26 186.69 176.3 173.85 180.01 193.13 209.69 225.25 (68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

$(69)m =$  36 36 36 36 36 36 36 36 36 36 36 36 (69)

Pumps and fans gains (Table 5a)

$(70)m =$  0 0 0 0 0 0 0 0 0 0 0 0 (70)

Losses e.g. evaporation (negative values) (Table 5)

$(71)m =$  -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 (71)

Water heating gains (Table 5)

$(72)m =$  44.7 43.29 40.34 36.35 33.75 30.09 26.99 30.97 32.38 36.52 41.19 43.29 (72)

**Total internal gains =**  $(66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m$

$(73)m =$  363.36 362.04 349.45 328.65 306.59 286.03 273.11 277 288.06 309 333.13 352.13 (73)

## 6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

# DFEE WorkSheet: New dwelling design stage

| Orientation: | Access Factor<br>Table 6d | Area<br>m <sup>2</sup> | Flux<br>Table 6a | g<br>Table 6b | FF<br>Table 6c | Gains<br>(W)  |
|--------------|---------------------------|------------------------|------------------|---------------|----------------|---------------|
| North        | 0.9x 0.77                 | x 6.01                 | x 10.63          | x 0.76        | x 0.7          | = 23.56 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 10.63          | x 0.76        | x 0.7          | = 24.7 (74)   |
| North        | 0.9x 0.77                 | x 1.59                 | x 10.63          | x 0.76        | x 0.7          | = 12.47 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 20.32          | x 0.76        | x 0.7          | = 45.03 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 20.32          | x 0.76        | x 0.7          | = 47.2 (74)   |
| North        | 0.9x 0.77                 | x 1.59                 | x 20.32          | x 0.76        | x 0.7          | = 23.82 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 34.53          | x 0.76        | x 0.7          | = 76.51 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 34.53          | x 0.76        | x 0.7          | = 80.2 (74)   |
| North        | 0.9x 0.77                 | x 1.59                 | x 34.53          | x 0.76        | x 0.7          | = 40.48 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 55.46          | x 0.76        | x 0.7          | = 122.89 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 55.46          | x 0.76        | x 0.7          | = 128.82 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 55.46          | x 0.76        | x 0.7          | = 65.03 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.72          | x 0.76        | x 0.7          | = 165.55 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.72          | x 0.76        | x 0.7          | = 173.54 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.72          | x 0.76        | x 0.7          | = 87.6 (74)   |
| North        | 0.9x 0.77                 | x 6.01                 | x 79.99          | x 0.76        | x 0.7          | = 177.23 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 79.99          | x 0.76        | x 0.7          | = 185.78 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 79.99          | x 0.76        | x 0.7          | = 93.77 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.68          | x 0.76        | x 0.7          | = 165.46 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.68          | x 0.76        | x 0.7          | = 173.45 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.68          | x 0.76        | x 0.7          | = 87.55 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 59.25          | x 0.76        | x 0.7          | = 131.27 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 59.25          | x 0.76        | x 0.7          | = 137.61 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 59.25          | x 0.76        | x 0.7          | = 69.46 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 41.52          | x 0.76        | x 0.7          | = 91.99 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 41.52          | x 0.76        | x 0.7          | = 96.43 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 41.52          | x 0.76        | x 0.7          | = 48.67 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 24.19          | x 0.76        | x 0.7          | = 53.6 (74)   |
| North        | 0.9x 0.77                 | x 6.3                  | x 24.19          | x 0.76        | x 0.7          | = 56.18 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 24.19          | x 0.76        | x 0.7          | = 28.36 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 13.12          | x 0.76        | x 0.7          | = 29.07 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 13.12          | x 0.76        | x 0.7          | = 30.47 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 13.12          | x 0.76        | x 0.7          | = 15.38 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 8.86           | x 0.76        | x 0.7          | = 19.64 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 8.86           | x 0.76        | x 0.7          | = 20.59 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 8.86           | x 0.76        | x 0.7          | = 10.39 (74)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 46.75          | x 0.76        | x 0.7          | = 21.03 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 76.57          | x 0.76        | x 0.7          | = 34.44 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 97.53          | x 0.76        | x 0.7          | = 43.87 (78)  |

# DFEE WorkSheet: New dwelling design stage

|            |      |      |   |      |   |        |   |      |   |     |   |        |      |
|------------|------|------|---|------|---|--------|---|------|---|-----|---|--------|------|
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.23 | x | 0.76 | x | 0.7 | = | 49.58  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 114.87 | x | 0.76 | x | 0.7 | = | 51.67  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.55 | x | 0.76 | x | 0.7 | = | 49.72  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 108.01 | x | 0.76 | x | 0.7 | = | 48.58  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 104.89 | x | 0.76 | x | 0.7 | = | 47.18  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 101.89 | x | 0.76 | x | 0.7 | = | 45.83  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 82.59  | x | 0.76 | x | 0.7 | = | 37.15  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 55.42  | x | 0.76 | x | 0.7 | = | 24.93  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 40.4   | x | 0.76 | x | 0.7 | = | 18.17  | (78) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 30.32  | x | 0.76 | x | 0.7 | = | 20.47  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 31.5   | x | 0.76 | x | 0.7 | = | 18.85  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 30.32  | x | 0.76 | x | 0.7 | = | 29.61  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 60.64  | x | 0.76 | x | 0.7 | = | 40.94  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 62.43  | x | 0.76 | x | 0.7 | = | 37.36  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 60.64  | x | 0.76 | x | 0.7 | = | 59.23  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 103.31 | x | 0.76 | x | 0.7 | = | 69.75  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 105.22 | x | 0.76 | x | 0.7 | = | 62.98  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 103.31 | x | 0.76 | x | 0.7 | = | 100.91 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 156.31 | x | 0.76 | x | 0.7 | = | 105.53 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 157.83 | x | 0.76 | x | 0.7 | = | 94.46  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 156.31 | x | 0.76 | x | 0.7 | = | 152.68 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 196.72 | x | 0.76 | x | 0.7 | = | 132.8  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 197.69 | x | 0.76 | x | 0.7 | = | 118.32 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 196.72 | x | 0.76 | x | 0.7 | = | 192.14 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 203.69 | x | 0.76 | x | 0.7 | = | 137.51 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 204.35 | x | 0.76 | x | 0.7 | = | 122.31 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 203.69 | x | 0.76 | x | 0.7 | = | 198.95 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 192.96 | x | 0.76 | x | 0.7 | = | 130.27 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 193.73 | x | 0.76 | x | 0.7 | = | 115.95 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 192.96 | x | 0.76 | x | 0.7 | = | 188.48 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 162.28 | x | 0.76 | x | 0.7 | = | 109.56 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 163.49 | x | 0.76 | x | 0.7 | = | 97.85  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 162.28 | x | 0.76 | x | 0.7 | = | 158.51 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 121.97 | x | 0.76 | x | 0.7 | = | 82.35  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 123.75 | x | 0.76 | x | 0.7 | = | 74.06  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 121.97 | x | 0.76 | x | 0.7 | = | 119.14 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 72.85  | x | 0.76 | x | 0.7 | = | 49.18  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 74.68  | x | 0.76 | x | 0.7 | = | 44.69  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 72.85  | x | 0.76 | x | 0.7 | = | 71.15  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 38.04  | x | 0.76 | x | 0.7 | = | 25.68  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 39.41  | x | 0.76 | x | 0.7 | = | 23.59  | (82) |



## DFEE WorkSheet: New dwelling design stage

### 8c. Space cooling requirement

Calculated for June, July and August. See Table 10b

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Heat loss rate Lm (calculated using 25°C internal temperature and external temperature from Table 10)

|         |   |   |   |   |   |         |        |       |   |   |   |   |       |
|---------|---|---|---|---|---|---------|--------|-------|---|---|---|---|-------|
| (100)m= | 0 | 0 | 0 | 0 | 0 | 1050.42 | 826.93 | 848.2 | 0 | 0 | 0 | 0 | (100) |
|---------|---|---|---|---|---|---------|--------|-------|---|---|---|---|-------|

Utilisation factor for loss hm

|         |   |   |   |   |   |      |      |      |   |   |   |   |       |
|---------|---|---|---|---|---|------|------|------|---|---|---|---|-------|
| (101)m= | 0 | 0 | 0 | 0 | 0 | 0.93 | 0.96 | 0.94 | 0 | 0 | 0 | 0 | (101) |
|---------|---|---|---|---|---|------|------|------|---|---|---|---|-------|

Useful loss, hmLm (Watts) = (100)m x (101)m

|         |   |   |   |   |   |        |       |        |   |   |   |   |       |
|---------|---|---|---|---|---|--------|-------|--------|---|---|---|---|-------|
| (102)m= | 0 | 0 | 0 | 0 | 0 | 978.59 | 796.5 | 796.12 | 0 | 0 | 0 | 0 | (102) |
|---------|---|---|---|---|---|--------|-------|--------|---|---|---|---|-------|

Gains (solar gains calculated for applicable weather region, see Table 10)

|         |   |   |   |   |   |         |         |         |   |   |   |   |       |
|---------|---|---|---|---|---|---------|---------|---------|---|---|---|---|-------|
| (103)m= | 0 | 0 | 0 | 0 | 0 | 1482.84 | 1404.84 | 1237.62 | 0 | 0 | 0 | 0 | (103) |
|---------|---|---|---|---|---|---------|---------|---------|---|---|---|---|-------|

Space cooling requirement for month, whole dwelling, continuous ( kWh) = 0.024 x [(103)m – (102)m] x (41)m

set (104)m to zero if (104)m < 3 x (98)m

|         |   |   |   |   |   |        |       |        |   |   |   |   |       |
|---------|---|---|---|---|---|--------|-------|--------|---|---|---|---|-------|
| (104)m= | 0 | 0 | 0 | 0 | 0 | 363.06 | 452.6 | 328.48 | 0 | 0 | 0 | 0 | (104) |
|---------|---|---|---|---|---|--------|-------|--------|---|---|---|---|-------|

$$\text{Total} = \text{Sum}(104) = 1144.14 \quad (104)$$

$$f C = \text{cooled area} \div (4) = 1 \quad (105)$$

Cooled fraction

Intermittency factor (Table 10b)

|         |   |   |   |   |   |      |      |      |   |   |   |   |       |
|---------|---|---|---|---|---|------|------|------|---|---|---|---|-------|
| (106)m= | 0 | 0 | 0 | 0 | 0 | 0.25 | 0.25 | 0.25 | 0 | 0 | 0 | 0 | (106) |
|---------|---|---|---|---|---|------|------|------|---|---|---|---|-------|

$$\text{Total} = \text{Sum}(106) = 0 \quad (106)$$

Space cooling requirement for month = (104)m x (105) x (106)m

|         |   |   |   |   |   |       |        |       |   |   |   |   |       |
|---------|---|---|---|---|---|-------|--------|-------|---|---|---|---|-------|
| (107)m= | 0 | 0 | 0 | 0 | 0 | 90.76 | 113.15 | 82.12 | 0 | 0 | 0 | 0 | (107) |
|---------|---|---|---|---|---|-------|--------|-------|---|---|---|---|-------|

$$\text{Total} = \text{Sum}(107) = 286.03 \quad (107)$$

Space cooling requirement in kWh/m<sup>2</sup>/year

$$(107) \div (4) = 3.24 \quad (108)$$

### 8f. Fabric Energy Efficiency (calculated only under special conditions, see section 11)

Fabric Energy Efficiency (99) + (108) = 51.24 (109)

# DER WorkSheet: New dwelling design stage

## User Details:

|                                     |                  |                          |                   |
|-------------------------------------|------------------|--------------------------|-------------------|
| <b>Assessor Name:</b>               | Peter Mitchell   | <b>Stroma Number:</b>    | STRO007945        |
| <b>Software Name:</b>               | Stroma FSAP 2012 | <b>Software Version:</b> | Version: 1.0.4.25 |
| Property Address: Unit 1 Clean ASHP |                  |                          |                   |

## Address :

1. Overall dwelling dimensions:

|   | <b>Area(m<sup>2</sup>)</b> | <b>Av. Height(m)</b>                 | <b>Volume(m<sup>3</sup>)</b> |
|---|----------------------------|--------------------------------------|------------------------------|
| Ground floor  | 52.9<br>(1a)               | x<br>(2a)                            | = 125.37<br>(3a)             |
| First floor   | 35.26<br>(1b)              | x<br>(2b)                            | = 90.27<br>(3b)              |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n) | 88.16<br>(4)               |                                      |                              |
| Dwelling volume   |                            | (3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) = | 215.64<br>(5)                |

2. Ventilation rate:

|                              | <b>main heating</b> | <b>secondary heating</b> | <b>other</b> | <b>total</b> | <b>m<sup>3</sup> per hour</b> |
|------------------------------|---------------------|--------------------------|--------------|--------------|-------------------------------|
| Number of chimneys           | 0                   | +                        | 0            | +            | 0 = 0 x 40 = 0<br>(6a)        |
| Number of open flues         | 0                   | +                        | 0            | +            | 0 = 0 x 20 = 0<br>(6b)        |
| Number of intermittent fans  |                     |                          |              |              | x 10 = 20<br>(7a)             |
| Number of passive vents      |                     |                          |              |              | x 10 = 0<br>(7b)              |
| Number of flueless gas fires |                     |                          |              |              | x 40 = 0<br>(7c)              |

## Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = 20 ÷ (5) = 0.09 (8)

If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)

Number of storeys in the dwelling (ns)

Additional infiltration

[(9)-1]x0.1 = 0  
(9)

Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction

if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35

If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0

If no draught lobby, enter 0.05, else enter 0

Percentage of windows and doors draught stripped

Window infiltration 0.25 - [0.2 x (14) ÷ 100] =

Infiltration rate (8) + (10) + (11) + (12) + (13) + (15) =

Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area If based on air permeability value, then (18) = [(17) ÷ 20]+(8), otherwise (18) = (16)

Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used

Number of sides sheltered

Shelter factor (20) = 1 - [0.075 x (19)] =

Infiltration rate incorporating shelter factor (21) = (18) x (20) =

Infiltration rate modified for monthly wind speed

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Monthly average wind speed from Table 7

|        |     |   |     |     |     |     |     |     |   |     |     |     |
|--------|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|
| (22)m= | 5.1 | 5 | 4.9 | 4.4 | 4.3 | 3.8 | 3.8 | 3.7 | 4 | 4.3 | 4.5 | 4.7 |
|--------|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|

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Wind Factor (22a)m = (22)m ÷ 4

|         |      |      |      |     |      |      |      |      |   |      |      |      |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|
| (22a)m= | 1.27 | 1.25 | 1.23 | 1.1 | 1.08 | 0.95 | 0.95 | 0.92 | 1 | 1.08 | 1.12 | 1.18 |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|

Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 0.37 | 0.36 | 0.36 | 0.32 | 0.31 | 0.28 | 0.28 | 0.27 | 0.29 | 0.31 | 0.33 | 0.34 |
|------|------|------|------|------|------|------|------|------|------|------|------|

Calculate effective air change rate for the applicable case

If mechanical ventilation:

|   |       |
|---|-------|
| 0 | (23a) |
|---|-------|

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

|   |       |
|---|-------|
| 0 | (23b) |
|---|-------|

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

|   |       |
|---|-------|
| 0 | (23c) |
|---|-------|

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24a)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24a)

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24b)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24b)

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b)m + 0.5 × (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24c)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24c)

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² × 0.5]

|         |      |      |      |      |      |      |      |      |      |      |      |      |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|
| (24d)m= | 0.57 | 0.57 | 0.56 | 0.55 | 0.55 | 0.54 | 0.54 | 0.54 | 0.54 | 0.55 | 0.55 | 0.56 |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|

(24d)

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

|        |      |      |      |      |      |      |      |      |      |      |      |      |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|
| (25)m= | 0.57 | 0.57 | 0.56 | 0.55 | 0.55 | 0.54 | 0.54 | 0.54 | 0.54 | 0.55 | 0.55 | 0.56 |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|

(25)

### 3. Heat losses and heat loss parameter:

| ELEMENT                                | Gross area (m <sup>2</sup> ) | Openings m <sup>2</sup> | Net Area A ,m <sup>2</sup> | U-value W/m <sup>2</sup> K | A X U (W/K) | k-value kJ/m <sup>2</sup> ·K | A X k kJ/K |
|--|------------------------------|-------------------------|----------------------------|----------------------------|-------------|------------------------------|------------|
| Windows Type 1                         |                              |                         | 6.01                       | x1/[1/( 1.2 )+ 0.04] =     | 6.88        |                              | (27)       |
| Windows Type 2                         |                              |                         | 6.3                        | x1/[1/( 1.2 )+ 0.04] =     | 7.21        |                              | (27)       |
| Windows Type 3                         |                              |                         | 1.59                       | x1/[1/( 1.2 )+ 0.04] =     | 1.82        |                              | (27)       |
| Windows Type 4                         |                              |                         | 0.61                       | x1/[1/( 1.2 )+ 0.04] =     | 0.7         |                              | (27)       |
| Rooflights Type 1                      |                              |                         | 1.41                       | x1/[1/(1.2) + 0.04] =      | 1.692       |                              | (27b)      |
| Rooflights Type 2                      |                              |                         | 1.25                       | x1/[1/(1.2) + 0.04] =      | 1.5         |                              | (27b)      |
| Rooflights Type 3                      |                              |                         | 2.04                       | x1/[1/(1.2) + 0.04] =      | 2.448       |                              | (27b)      |
| Floor                                  |                              |                         | 52.9                       | x 0.13 =                   | 6.877       |                              | (28)       |
| Walls                                  | 109.46                       | 16.71                   | 92.75                      | x 0.18 =                   | 16.7        |                              | (29)       |
| Roof Type1                             | 35.52                        | 1.25                    | 34.27                      | x 0.13 =                   | 4.46        |                              | (30)       |
| Roof Type2                             | 17.86                        | 3.45                    | 14.41                      | x 0.13 =                   | 1.87        |                              | (30)       |
| Total area of elements, m <sup>2</sup> |                              |                         | 215.74                     |                            |             |                              | (31)       |
| Party wall                             |                              |                         | 32.84                      | x 0 =                      | 0           |                              | (32)       |

\* for windows and roof windows, use effective window U-value calculated using formula  $1/[(1/U\text{-value})+0.04]$  as given in paragraph 3.2

\*\* include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = 54.42 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) = 0 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m<sup>2</sup>K Indicative Value: Medium 250 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f

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can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K

19.03 (36)

if details of thermal bridging are not known (36) =  $0.05 \times (31)$

Total fabric heat loss

$(33) + (36) =$

73.44 (37)

Ventilation heat loss calculated monthly

$(38)m = 0.33 \times (25)m \times (5)$

| Jan          | Feb  | Mar   | Apr   | May   | Jun   | Jul   | Aug   | Sep  | Oct   | Nov  | Dec   |
|--------------|------|-------|-------|-------|-------|-------|-------|------|-------|------|-------|
| (38)m= 40.49 | 40.3 | 40.11 | 39.23 | 39.07 | 38.31 | 38.31 | 38.16 | 38.6 | 39.07 | 39.4 | 39.75 |

(38)

Heat transfer coefficient, W/K

$(39)m = (37) + (38)m$

|  |        |        |        |        |        |        |        |        |        |        |             |
|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------------|
| (39)m= 113.93                            | 113.74 | 113.55 | 112.68 | 112.51 | 111.75 | 111.75 | 111.61 | 112.04 | 112.51 | 112.84 | 113.19      |
| Average = Sum(39) <sub>1...12</sub> /12= |        |        |        |        |        |        |        |        |        |        | 112.67 (39) |

Heat loss parameter (HLP), W/m<sup>2</sup>K

$(40)m = (39)m \div (4)$

|  |      |      |      |      |      |      |      |      |      |      |           |
|--|------|------|------|------|------|------|------|------|------|------|-----------|
| (40)m= 1.29                              | 1.29 | 1.29 | 1.28 | 1.28 | 1.27 | 1.27 | 1.27 | 1.27 | 1.28 | 1.28 | 1.28      |
| Average = Sum(40) <sub>1...12</sub> /12= |      |      |      |      |      |      |      |      |      |      | 1.28 (40) |

Number of days in month (Table 1a)

| Jan       | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| (41)m= 31 | 28  | 31  | 30  | 31  | 30  | 31  | 31  | 30  | 31  | 30  | 31  |

(41)

## 4. Water heating energy requirement:

kWh/year:

Assumed occupancy, N

2.6 (42)

if TFA > 13.9,  $N = 1 + 1.76 \times [1 - \exp(-0.000349 \times (\text{TFA} - 13.9)^2)] + 0.0013 \times (\text{TFA} - 13.9)$

if TFA £ 13.9,  $N = 1$

Annual average hot water usage in litres per day  $Vd,average = (25 \times N) + 36$

95.94 (43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Hot water usage in litres per day for each month  $Vd,m = \text{factor from Table 1c} \times (43)$

|                                     |       |       |       |       |       |       |       |       |       |       |              |
|-------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------------|
| (44)m= 105.54                       | 101.7 | 97.86 | 94.02 | 90.19 | 86.35 | 86.35 | 90.19 | 94.02 | 97.86 | 101.7 | 105.54       |
| Total = Sum(44) <sub>1...12</sub> = |       |       |       |       |       |       |       |       |       |       | 1151.31 (44) |

Energy content of hot water used - calculated monthly =  $4.190 \times Vd,m \times nm \times DTm / 3600 \text{ kWh/month}$  (see Tables 1b, 1c, 1d)

|                                     |        |        |        |        |        |       |        |        |        |        |              |
|-------------------------------------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------------|
| (45)m= 156.51                       | 136.88 | 141.25 | 123.15 | 118.16 | 101.96 | 94.49 | 108.42 | 109.72 | 127.87 | 139.58 | 151.57       |
| Total = Sum(45) <sub>1...12</sub> = |        |        |        |        |        |       |        |        |        |        | 1509.55 (45) |

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

|              |       |       |       |       |       |       |       |       |       |       |       |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| (46)m= 23.48 | 20.53 | 21.19 | 18.47 | 17.72 | 15.29 | 14.17 | 16.26 | 16.46 | 19.18 | 20.94 | 22.74 |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|

(46)

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel

120 (47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

a) If manufacturer's declared loss factor is known (kWh/day):

0 (48)

Temperature factor from Table 2b

0 (49)

Energy lost from water storage, kWh/year  $(48) \times (49) =$

120 (50)

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day)

0.01 (51)

If community heating see section 4.3

Volume factor from Table 2a

1 (52)

Temperature factor from Table 2b

0.54 (53)

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Energy lost from water storage, kWh/year  $(47) \times (51) \times (52) \times (53) =$  0.75 (54)  
 Enter (50) or (54) in (55) 0.75 (55)

Water storage loss calculated for each month  $((56)m = (55) \times (41)m$  23.2 20.95 23.2 22.45 23.2 22.45 23.2 23.2 22.45 23.2 22.45 23.2 (56)

If cylinder contains dedicated solar storage, (57)m = (56)m x [(50) – (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

(57)m = 23.2 20.95 23.2 22.45 23.2 22.45 23.2 23.2 22.45 23.2 22.45 23.2 (57)

Primary circuit loss (annual) from Table 3 0 (58)

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 × (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)  
(59)m = 23.26 21.01 23.26 22.51 23.26 22.51 23.26 23.26 22.51 23.26 22.51 23.26 (59)

Combi loss calculated for each month (61)m = (60) ÷ 365 × (41)m

(61)m = 0 0 0 0 0 0 0 0 0 0 0 0 (61)

Total heat required for water heating calculated for each month (62)m = 0.85 × (45)m + (46)m + (57)m + (59)m + (61)m

(62)m = 202.97 178.85 187.71 168.11 164.62 146.92 140.94 154.88 154.68 174.32 184.54 198.03 (62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)

(63)m = 0 0 0 0 0 0 0 0 0 0 0 0 (63)

Output from water heater

(64)m = 202.97 178.85 187.71 168.11 164.62 146.92 140.94 154.88 154.68 174.32 184.54 198.03 Output from water heater (annual) 1...12 2056.57 (64)

Heat gains from water heating, kWh/month 0.25 [0.85 × (45)m + (61)m] + 0.8 × [(46)m + (57)m + (59)m]

(65)m = 89.21 79.08 84.13 76.91 76.46 69.87 68.58 73.22 72.45 79.68 82.38 87.56 (65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

## 5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

| Jan    | Feb    | Mar    | Apr    | May    | Jun    | Jul    | Aug    | Sep    | Oct    | Nov    | Dec    |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 | 129.98 |

(66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

(67)m = 21.01 18.66 15.17 11.49 8.59 7.25 7.83 10.18 13.67 17.35 20.25 21.59 (67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

(68)m = 235.65 238.1 231.93 218.82 202.26 186.69 176.3 173.85 180.01 193.13 209.69 225.25 (68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

(69)m = 36 36 36 36 36 36 36 36 36 36 36 36 (69)

Pumps and fans gains (Table 5a)

(70)m = 0 0 0 0 0 0 0 0 0 0 0 0 (70)

Losses e.g. evaporation (negative values) (Table 5)

(71)m = -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 (71)

Water heating gains (Table 5)

(72)m = 119.9 117.68 113.08 106.83 102.76 97.04 92.18 98.41 100.62 107.1 114.41 117.69 (72)

**Total internal gains =**  $(66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m$

(73)m = 438.56 436.44 422.19 399.13 375.6 352.98 338.31 344.44 356.3 379.58 406.35 426.54 (73)

## 6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

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| Orientation: | Access Factor<br>Table 6d | Area<br>m <sup>2</sup> | Flux<br>Table 6a | g<br>Table 6b | FF<br>Table 6c | Gains<br>(W)  |
|--------------|---------------------------|------------------------|------------------|---------------|----------------|---------------|
| North        | 0.9x 0.77                 | x 6.01                 | x 10.63          | x 0.76        | x 0.7          | = 23.56 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 10.63          | x 0.76        | x 0.7          | = 24.7 (74)   |
| North        | 0.9x 0.77                 | x 1.59                 | x 10.63          | x 0.76        | x 0.7          | = 12.47 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 20.32          | x 0.76        | x 0.7          | = 45.03 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 20.32          | x 0.76        | x 0.7          | = 47.2 (74)   |
| North        | 0.9x 0.77                 | x 1.59                 | x 20.32          | x 0.76        | x 0.7          | = 23.82 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 34.53          | x 0.76        | x 0.7          | = 76.51 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 34.53          | x 0.76        | x 0.7          | = 80.2 (74)   |
| North        | 0.9x 0.77                 | x 1.59                 | x 34.53          | x 0.76        | x 0.7          | = 40.48 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 55.46          | x 0.76        | x 0.7          | = 122.89 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 55.46          | x 0.76        | x 0.7          | = 128.82 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 55.46          | x 0.76        | x 0.7          | = 65.03 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.72          | x 0.76        | x 0.7          | = 165.55 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.72          | x 0.76        | x 0.7          | = 173.54 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.72          | x 0.76        | x 0.7          | = 87.6 (74)   |
| North        | 0.9x 0.77                 | x 6.01                 | x 79.99          | x 0.76        | x 0.7          | = 177.23 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 79.99          | x 0.76        | x 0.7          | = 185.78 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 79.99          | x 0.76        | x 0.7          | = 93.77 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.68          | x 0.76        | x 0.7          | = 165.46 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.68          | x 0.76        | x 0.7          | = 173.45 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.68          | x 0.76        | x 0.7          | = 87.55 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 59.25          | x 0.76        | x 0.7          | = 131.27 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 59.25          | x 0.76        | x 0.7          | = 137.61 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 59.25          | x 0.76        | x 0.7          | = 69.46 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 41.52          | x 0.76        | x 0.7          | = 91.99 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 41.52          | x 0.76        | x 0.7          | = 96.43 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 41.52          | x 0.76        | x 0.7          | = 48.67 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 24.19          | x 0.76        | x 0.7          | = 53.6 (74)   |
| North        | 0.9x 0.77                 | x 6.3                  | x 24.19          | x 0.76        | x 0.7          | = 56.18 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 24.19          | x 0.76        | x 0.7          | = 28.36 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 13.12          | x 0.76        | x 0.7          | = 29.07 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 13.12          | x 0.76        | x 0.7          | = 30.47 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 13.12          | x 0.76        | x 0.7          | = 15.38 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 8.86           | x 0.76        | x 0.7          | = 19.64 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 8.86           | x 0.76        | x 0.7          | = 20.59 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 8.86           | x 0.76        | x 0.7          | = 10.39 (74)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 46.75          | x 0.76        | x 0.7          | = 21.03 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 76.57          | x 0.76        | x 0.7          | = 34.44 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 97.53          | x 0.76        | x 0.7          | = 43.87 (78)  |

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|            |      |      |   |      |   |        |   |      |   |     |   |        |      |
|------------|------|------|---|------|---|--------|---|------|---|-----|---|--------|------|
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.23 | x | 0.76 | x | 0.7 | = | 49.58  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 114.87 | x | 0.76 | x | 0.7 | = | 51.67  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.55 | x | 0.76 | x | 0.7 | = | 49.72  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 108.01 | x | 0.76 | x | 0.7 | = | 48.58  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 104.89 | x | 0.76 | x | 0.7 | = | 47.18  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 101.89 | x | 0.76 | x | 0.7 | = | 45.83  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 82.59  | x | 0.76 | x | 0.7 | = | 37.15  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 55.42  | x | 0.76 | x | 0.7 | = | 24.93  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 40.4   | x | 0.76 | x | 0.7 | = | 18.17  | (78) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 30.32  | x | 0.76 | x | 0.7 | = | 20.47  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 31.5   | x | 0.76 | x | 0.7 | = | 18.85  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 30.32  | x | 0.76 | x | 0.7 | = | 29.61  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 60.64  | x | 0.76 | x | 0.7 | = | 40.94  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 62.43  | x | 0.76 | x | 0.7 | = | 37.36  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 60.64  | x | 0.76 | x | 0.7 | = | 59.23  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 103.31 | x | 0.76 | x | 0.7 | = | 69.75  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 105.22 | x | 0.76 | x | 0.7 | = | 62.98  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 103.31 | x | 0.76 | x | 0.7 | = | 100.91 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 156.31 | x | 0.76 | x | 0.7 | = | 105.53 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 157.83 | x | 0.76 | x | 0.7 | = | 94.46  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 156.31 | x | 0.76 | x | 0.7 | = | 152.68 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 196.72 | x | 0.76 | x | 0.7 | = | 132.8  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 197.69 | x | 0.76 | x | 0.7 | = | 118.32 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 196.72 | x | 0.76 | x | 0.7 | = | 192.14 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 203.69 | x | 0.76 | x | 0.7 | = | 137.51 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 204.35 | x | 0.76 | x | 0.7 | = | 122.31 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 203.69 | x | 0.76 | x | 0.7 | = | 198.95 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 192.96 | x | 0.76 | x | 0.7 | = | 130.27 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 193.73 | x | 0.76 | x | 0.7 | = | 115.95 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 192.96 | x | 0.76 | x | 0.7 | = | 188.48 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 162.28 | x | 0.76 | x | 0.7 | = | 109.56 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 163.49 | x | 0.76 | x | 0.7 | = | 97.85  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 162.28 | x | 0.76 | x | 0.7 | = | 158.51 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 121.97 | x | 0.76 | x | 0.7 | = | 82.35  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 123.75 | x | 0.76 | x | 0.7 | = | 74.06  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 121.97 | x | 0.76 | x | 0.7 | = | 119.14 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 72.85  | x | 0.76 | x | 0.7 | = | 49.18  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 74.68  | x | 0.76 | x | 0.7 | = | 44.69  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 72.85  | x | 0.76 | x | 0.7 | = | 71.15  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 38.04  | x | 0.76 | x | 0.7 | = | 25.68  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 39.41  | x | 0.76 | x | 0.7 | = | 23.59  | (82) |



# DER WorkSheet: New dwelling design stage

## 9a. Energy requirements – Individual heating systems including micro-CHP)

### Space heating:

Fraction of space heat from secondary/supplementary system

0 (201)

Fraction of space heat from main system(s)

$(202) = 1 - (201) =$

1 (202)

Fraction of total heating from main system 1

$(204) = (202) \times [1 - (203)] =$

1 (204)

Efficiency of main space heating system 1

237.4 (206)

Efficiency of secondary/supplementary heating system, %

0 (208)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | kWh/year |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------|

Space heating requirement (calculated above)

|        |       |        |        |       |   |   |   |   |        |        |        |
|--------|-------|--------|--------|-------|---|---|---|---|--------|--------|--------|
| 936.46 | 710.4 | 537.52 | 233.13 | 64.11 | 0 | 0 | 0 | 0 | 321.07 | 665.89 | 963.63 |
|--------|-------|--------|--------|-------|---|---|---|---|--------|--------|--------|

$(211)m = \{[(98)m \times (204)]\} \times 100 \div (206)$  (211)

|        |        |        |      |       |   |   |   |   |        |        |       |
|--------|--------|--------|------|-------|---|---|---|---|--------|--------|-------|
| 394.46 | 299.24 | 226.42 | 98.2 | 27.01 | 0 | 0 | 0 | 0 | 135.24 | 280.49 | 405.9 |
|--------|--------|--------|------|-------|---|---|---|---|--------|--------|-------|

Total (kWh/year) = Sum(211)<sub>1...5,10...12</sub> = 1866.96 (211)

Space heating fuel (secondary), kWh/month

=  $\{[(98)m \times (201)]\} \times 100 \div (208)$

|   |   |   |   |   |   |   |   |   |   |   |   |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---|---|---|---|---|---|---|---|---|---|---|---|

Total (kWh/year) = Sum(215)<sub>1...5,10...12</sub> = 0 (215)

### Water heating

Output from water heater (calculated above)

|        |        |        |        |        |        |        |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 202.97 | 178.85 | 187.71 | 168.11 | 164.62 | 146.92 | 140.94 | 154.88 | 154.68 | 174.32 | 184.54 | 198.03 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|

Efficiency of water heater

119.34 (216)

|        |        |        |        |        |        |        |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 | 119.34 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|

119.34 (216)

Fuel for water heating, kWh/month

$(219)m = (64)m \times 100 \div (217)m$

|        |        |        |        |        |        |       |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|
| 170.07 | 149.86 | 157.29 | 140.86 | 137.94 | 123.11 | 118.1 | 129.78 | 129.61 | 146.07 | 154.63 | 165.94 |
|--------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|

Total = Sum(219a)<sub>1...12</sub> = 1723.29 (219)

kWh/year

Annual totals

Space heating fuel used, main system 1

1866.96

Water heating fuel used

1723.29

Electricity for pumps, fans and electric keep-hot

Total electricity for the above, kWh/year

sum of (230a)...(230g) = 0 (231)

Electricity for lighting

371.02 (232)

## 12a. CO2 emissions – Individual heating systems including micro-CHP

|   | Energy<br>kWh/year              | Emission factor<br>kg CO2/kWh | Emissions<br>kg CO2/year |
|---|---------------------------------|-------------------------------|--------------------------|
| Space heating (main system 1)                     | (211) x                         | 0.519                         | = 968.95 (261)           |
| Space heating (secondary)                         | (215) x                         | 0.519                         | = 0 (263)                |
| Water heating                                     | (219) x                         | 0.519                         | = 894.39 (264)           |
| Space and water heating                           | (261) + (262) + (263) + (264) = |                               | 1863.34 (265)            |
| Electricity for pumps, fans and electric keep-hot | (231) x                         | 0.519                         | = 0 (267)                |
| Electricity for lighting                          | (232) x                         | 0.519                         | = 192.56 (268)           |

## DER WorkSheet: New dwelling design stage

|                            |                        |        |       |
|----------------------------|------------------------|--------|-------|
| Total CO2, kg/year         | sum of (265)...(271) = | 2055.9 | (272) |
| Dwelling CO2 Emission Rate | $(272) \div (4) =$     | 23.32  | (273) |
| EI rating (section 14)     |                        | 79     | (274) |

# TER WorkSheet: New dwelling design stage

## User Details:

|                       |                  |                          |                   |
|-----------------------|------------------|--------------------------|-------------------|
| <b>Assessor Name:</b> | Peter Mitchell   | <b>Stroma Number:</b>    | STRO007945        |
| <b>Software Name:</b> | Stroma FSAP 2012 | <b>Software Version:</b> | Version: 1.0.4.25 |

Property Address: Unit 1 Clean ASHP

## Address :

1. Overall dwelling dimensions:

|   | <b>Area(m<sup>2</sup>)</b>   | <b>Av. Height(m)</b>                 | <b>Volume(m<sup>3</sup>)</b> |
|---|------------------------------|--------------------------------------|------------------------------|
| Ground floor  | 52.9<br><small>(1a)</small>  | x<br><small>(2a)</small>             | 2.37<br><small>(3a)</small>  |
| First floor   | 35.26<br><small>(1b)</small> | x<br><small>(2b)</small>             | 2.56<br><small>(3b)</small>  |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n) | 88.16<br><small>(4)</small>  |                                      |                              |
| Dwelling volume   |                              | (3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) = | 215.64<br><small>(5)</small> |

2. Ventilation rate:

|                              | <b>main heating</b> | <b>secondary heating</b> | <b>other</b> | <b>total</b> | <b>m<sup>3</sup> per hour</b>    |
|------------------------------|---------------------|--------------------------|--------------|--------------|----------------------------------|
| Number of chimneys           | 0                   | +                        | 0            | = 0          | x 40 = 0<br><small>(6a)</small>  |
| Number of open flues         | 0                   | +                        | 0            | = 0          | x 20 = 0<br><small>(6b)</small>  |
| Number of intermittent fans  |                     |                          |              | 3            | x 10 = 30<br><small>(7a)</small> |
| Number of passive vents      |                     |                          |              | 0            | x 10 = 0<br><small>(7b)</small>  |
| Number of flueless gas fires |                     |                          |              | 0            | x 40 = 0<br><small>(7c)</small>  |

## Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = 30 ÷ (5) = 0.14 (8)

If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)

Number of storeys in the dwelling (ns)

Additional infiltration

[(9)-1]x0.1 =

0 (9)

0 (10)

0 (11)

Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction

if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35

If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0

0 (12)

If no draught lobby, enter 0.05, else enter 0

0 (13)

Percentage of windows and doors draught stripped

0 (14)

Window infiltration

$0.25 - [0.2 \times (14) \div 100] =$

0 (15)

Infiltration rate

$(8) + (10) + (11) + (12) + (13) + (15) =$

0 (16)

Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area

0 (17)

If based on air permeability value, then (18) = [(17) ÷ 20]+(8), otherwise (18) = (16)

0.39 (18)

Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used

Number of sides sheltered

2 (19)

Shelter factor

$(20) = 1 - [0.075 \times (19)] =$

0.85 (20)

Infiltration rate incorporating shelter factor

$(21) = (18) \times (20) =$

0.33 (21)

Infiltration rate modified for monthly wind speed

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Monthly average wind speed from Table 7

|        |     |   |     |     |     |     |     |     |   |     |     |     |
|--------|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|
| (22)m= | 5.1 | 5 | 4.9 | 4.4 | 4.3 | 3.8 | 3.8 | 3.7 | 4 | 4.3 | 4.5 | 4.7 |
|--------|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|

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Wind Factor (22a)m = (22)m ÷ 4

|         |      |      |      |     |      |      |      |      |   |      |      |      |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|
| (22a)m= | 1.27 | 1.25 | 1.23 | 1.1 | 1.08 | 0.95 | 0.95 | 0.92 | 1 | 1.08 | 1.12 | 1.18 |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|

Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 0.42 | 0.41 | 0.41 | 0.36 | 0.36 | 0.31 | 0.31 | 0.31 | 0.33 | 0.36 | 0.37 | 0.39 |
|------|------|------|------|------|------|------|------|------|------|------|------|

Calculate effective air change rate for the applicable case

If mechanical ventilation:

|   |       |
|---|-------|
| 0 | (23a) |
|---|-------|

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

|   |       |
|---|-------|
| 0 | (23b) |
|---|-------|

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

|   |       |
|---|-------|
| 0 | (23c) |
|---|-------|

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24a)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24a)

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24b)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24b)

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b)m + 0.5 × (23b)

|         |   |   |   |   |   |   |   |   |   |   |   |   |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|
| (24c)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|

(24c)

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² × 0.5]

|         |      |      |      |      |      |      |      |      |      |      |      |      |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|
| (24d)m= | 0.59 | 0.59 | 0.58 | 0.57 | 0.56 | 0.55 | 0.55 | 0.55 | 0.56 | 0.57 | 0.58 | 0.58 |
|---------|------|------|------|------|------|------|------|------|------|------|------|------|

(24d)

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

|        |      |      |      |      |      |      |      |      |      |      |      |      |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|
| (25)m= | 0.59 | 0.59 | 0.58 | 0.57 | 0.56 | 0.55 | 0.55 | 0.55 | 0.56 | 0.57 | 0.58 | 0.58 |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|

(25)

### 3. Heat losses and heat loss parameter:

| ELEMENT                                | Gross area (m <sup>2</sup> ) | Openings m <sup>2</sup> | Net Area A ,m <sup>2</sup> | U-value W/m <sup>2</sup> K | A X U (W/K) | k-value kJ/m <sup>2</sup> ·K | A X k kJ/K |
|--|------------------------------|-------------------------|----------------------------|----------------------------|-------------|------------------------------|------------|
| Windows Type 1                         |                              |                         | 6.01                       | x1/[1/( 1.4 )+ 0.04] =     | 7.97        |                              | (27)       |
| Windows Type 2                         |                              |                         | 6.3                        | x1/[1/( 1.4 )+ 0.04] =     | 8.35        |                              | (27)       |
| Windows Type 3                         |                              |                         | 1.59                       | x1/[1/( 1.4 )+ 0.04] =     | 2.11        |                              | (27)       |
| Windows Type 4                         |                              |                         | 0.61                       | x1/[1/( 1.4 )+ 0.04] =     | 0.81        |                              | (27)       |
| Rooflights Type 1                      |                              |                         | 1.41                       | x1/[1/(1.7) + 0.04] =      | 2.397       |                              | (27b)      |
| Rooflights Type 2                      |                              |                         | 1.25                       | x1/[1/(1.7) + 0.04] =      | 2.125       |                              | (27b)      |
| Rooflights Type 3                      |                              |                         | 2.04                       | x1/[1/(1.7) + 0.04] =      | 3.468       |                              | (27b)      |
| Floor                                  |                              |                         | 52.9                       | x 0.13 =                   | 6.877       |                              | (28)       |
| Walls                                  | 109.46                       | 16.71                   | 92.75                      | x 0.18 =                   | 16.7        |                              | (29)       |
| Roof Type1                             | 35.52                        | 1.25                    | 34.27                      | x 0.13 =                   | 4.46        |                              | (30)       |
| Roof Type2                             | 17.86                        | 3.45                    | 14.41                      | x 0.13 =                   | 1.87        |                              | (30)       |
| Total area of elements, m <sup>2</sup> |                              |                         | 215.74                     |                            |             |                              | (31)       |
| Party wall                             |                              |                         | 32.84                      | x 0 =                      | 0           |                              | (32)       |

\* for windows and roof windows, use effective window U-value calculated using formula  $1/[(1/U\text{-value})+0.04]$  as given in paragraph 3.2

\*\* include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = 59.54 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) = 0 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m<sup>2</sup>K Indicative Value: Medium 250 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f

# TER WorkSheet: New dwelling design stage

can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K

13.12 (36)

if details of thermal bridging are not known (36) =  $0.05 \times (31)$

Total fabric heat loss

(33) + (36) =

72.66 (37)

Ventilation heat loss calculated monthly

(38)m =  $0.33 \times (25)m \times (5)$

| Jan          | Feb   | Mar   | Apr   | May   | Jun   | Jul   | Aug   | Sep   | Oct   | Nov   | Dec   |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| (38)m= 41.91 | 41.66 | 41.42 | 40.29 | 40.08 | 39.09 | 39.09 | 38.91 | 39.47 | 40.08 | 40.51 | 40.95 |

(38)

Heat transfer coefficient, W/K

(39)m = (37) + (38)m

|  |        |        |        |        |        |        |        |        |        |        |        |
|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| (39)m= 114.57                            | 114.32 | 114.08 | 112.95 | 112.74 | 111.75 | 111.75 | 111.57 | 112.13 | 112.74 | 113.17 | 113.61 |
| Average = Sum(39) <sub>1...12</sub> /12= |        |        |        |        |        |        |        |        |        |        | 112.95 |

(39)

Heat loss parameter (HLP), W/m<sup>2</sup>K

(40)m = (39)m ÷ (4)

|  |     |      |      |      |      |      |      |      |      |      |      |
|--|-----|------|------|------|------|------|------|------|------|------|------|
| (40)m= 1.3                               | 1.3 | 1.29 | 1.28 | 1.28 | 1.27 | 1.27 | 1.27 | 1.27 | 1.28 | 1.28 | 1.29 |
| Average = Sum(40) <sub>1...12</sub> /12= |     |      |      |      |      |      |      |      |      |      | 1.28 |

(40)

Number of days in month (Table 1a)

| Jan       | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| (41)m= 31 | 28  | 31  | 30  | 31  | 30  | 31  | 31  | 30  | 31  | 30  | 31  |

(41)

4. Water heating energy requirement:

kWh/year:

Assumed occupancy, N

2.6

(42)

if TFA > 13.9,  $N = 1 + 1.76 \times [1 - \exp(-0.000349 \times (\text{TFA} - 13.9)2)] + 0.0013 \times (\text{TFA} - 13.9)$

if TFA £ 13.9,  $N = 1$

Annual average hot water usage in litres per day  $Vd,\text{average} = (25 \times N) + 36$

95.94

(43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Hot water usage in litres per day for each month  $Vd,m = \text{factor from Table 1c} \times (43)$

|                                     |       |       |       |       |       |       |       |       |       |       |         |
|-------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|
| (44)m= 105.54                       | 101.7 | 97.86 | 94.02 | 90.19 | 86.35 | 86.35 | 90.19 | 94.02 | 97.86 | 101.7 | 105.54  |
| Total = Sum(44) <sub>1...12</sub> = |       |       |       |       |       |       |       |       |       |       | 1151.31 |

(44)

Energy content of hot water used - calculated monthly =  $4.190 \times Vd,m \times nm \times DTm / 3600 \text{ kWh/month}$  (see Tables 1b, 1c, 1d)

|                                     |        |        |        |        |        |       |        |        |        |        |         |
|-------------------------------------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|---------|
| (45)m= 156.51                       | 136.88 | 141.25 | 123.15 | 118.16 | 101.96 | 94.49 | 108.42 | 109.72 | 127.87 | 139.58 | 151.57  |
| Total = Sum(45) <sub>1...12</sub> = |        |        |        |        |        |       |        |        |        |        | 1509.55 |

(45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

|              |       |       |       |       |       |       |       |       |       |       |       |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| (46)m= 23.48 | 20.53 | 21.19 | 18.47 | 17.72 | 15.29 | 14.17 | 16.26 | 16.46 | 19.18 | 20.94 | 22.74 |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|

(46)

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel

150

(47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

a) If manufacturer's declared loss factor is known (kWh/day):

1.22

(48)

Temperature factor from Table 2b

0.54

(49)

Energy lost from water storage, kWh/year

(48) x (49) =

0.66

(50)

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day)

0

(51)

If community heating see section 4.3

Volume factor from Table 2a

0

(52)

Temperature factor from Table 2b

0

(53)

# TER WorkSheet: New dwelling design stage

Energy lost from water storage, kWh/year  $(47) \times (51) \times (52) \times (53) =$  0 (54)  
 Enter (50) or (54) in (55) 0.66 (55)

Water storage loss calculated for each month  $((56)m = (55) \times (41)m$  0 (56)

(56)m= 20.5 18.52 20.5 19.84 20.5 19.84 20.5 20.5 19.84 20.5 19.84 20.5 (56)

If cylinder contains dedicated solar storage, (57)m = (56)m x [(50) – (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

(57)m= 20.5 18.52 20.5 19.84 20.5 19.84 20.5 20.5 19.84 20.5 19.84 20.5 (57)

Primary circuit loss (annual) from Table 3 0 (58)

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 × (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)  
(59)m= 23.26 21.01 23.26 22.51 23.26 22.51 23.26 23.26 22.51 23.26 22.51 23.26 (59)

Combi loss calculated for each month (61)m = (60) ÷ 365 × (41)m (61)

(61)m= 0 0 0 0 0 0 0 0 0 0 0 0 (61)

Total heat required for water heating calculated for each month (62)m = 0.85 × (45)m + (46)m + (57)m + (59)m + (61)m

(62)m= 200.27 176.41 185.01 165.5 161.92 144.32 138.25 152.19 152.07 171.63 181.93 195.33 (62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)  
(63)m= 0 0 0 0 0 0 0 0 0 0 0 0 (63)

Output from water heater  
(64)m= 200.27 176.41 185.01 165.5 161.92 144.32 138.25 152.19 152.07 171.63 181.93 195.33 Output from water heater (annual) 1...12 2024.83 (64)

Heat gains from water heating, kWh/month 0.25 [0.85 × (45)m + (61)m] + 0.8 × [(46)m + (57)m + (59)m]  
(65)m= 87.05 77.14 81.98 74.83 74.3 67.78 66.43 71.06 70.36 77.53 80.29 85.41 (65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

## 5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts  
(66)m= Jan Feb Mar Apr May Jun Jul Aug Sep Oct Nov Dec 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 129.98 (66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5  
(67)m= 21.01 18.66 15.17 11.49 8.59 7.25 7.83 10.18 13.67 17.35 20.25 21.59 (67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5  
(68)m= 235.65 238.1 231.93 218.82 202.26 186.69 176.3 173.85 180.01 193.13 209.69 225.25 (68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5  
(69)m= 36 36 36 36 36 36 36 36 36 36 36 36 (69)

Pumps and fans gains (Table 5a)  
(70)m= 3 3 3 3 3 3 3 3 3 3 3 3 (70)

Losses e.g. evaporation (negative values) (Table 5)  
(71)m= -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 -103.99 (71)

Water heating gains (Table 5)  
(72)m= 117 114.79 110.18 103.93 99.86 94.14 89.28 95.51 97.73 104.2 111.51 114.79 (72)

**Total internal gains =**  $(66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m$   
(73)m= 438.66 436.54 422.29 399.23 375.7 353.08 338.41 344.54 356.4 379.68 406.45 426.64 (73)

## 6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

# TER WorkSheet: New dwelling design stage

| Orientation: | Access Factor<br>Table 6d | Area<br>m <sup>2</sup> | Flux<br>Table 6a | g<br>Table 6b | FF<br>Table 6c | Gains<br>(W)  |
|--------------|---------------------------|------------------------|------------------|---------------|----------------|---------------|
| North        | 0.9x 0.77                 | x 6.01                 | x 10.63          | x 0.63        | x 0.7          | = 19.53 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 10.63          | x 0.63        | x 0.7          | = 20.47 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 10.63          | x 0.63        | x 0.7          | = 10.33 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 20.32          | x 0.63        | x 0.7          | = 37.32 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 20.32          | x 0.63        | x 0.7          | = 39.13 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 20.32          | x 0.63        | x 0.7          | = 19.75 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 34.53          | x 0.63        | x 0.7          | = 63.42 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 34.53          | x 0.63        | x 0.7          | = 66.48 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 34.53          | x 0.63        | x 0.7          | = 33.56 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 55.46          | x 0.63        | x 0.7          | = 101.87 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 55.46          | x 0.63        | x 0.7          | = 106.79 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 55.46          | x 0.63        | x 0.7          | = 53.9 (74)   |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.72          | x 0.63        | x 0.7          | = 137.23 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.72          | x 0.63        | x 0.7          | = 143.85 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.72          | x 0.63        | x 0.7          | = 72.61 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 79.99          | x 0.63        | x 0.7          | = 146.91 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 79.99          | x 0.63        | x 0.7          | = 154 (74)    |
| North        | 0.9x 0.77                 | x 1.59                 | x 79.99          | x 0.63        | x 0.7          | = 77.73 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 74.68          | x 0.63        | x 0.7          | = 137.16 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 74.68          | x 0.63        | x 0.7          | = 143.78 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 74.68          | x 0.63        | x 0.7          | = 72.57 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 59.25          | x 0.63        | x 0.7          | = 108.82 (74) |
| North        | 0.9x 0.77                 | x 6.3                  | x 59.25          | x 0.63        | x 0.7          | = 114.07 (74) |
| North        | 0.9x 0.77                 | x 1.59                 | x 59.25          | x 0.63        | x 0.7          | = 57.58 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 41.52          | x 0.63        | x 0.7          | = 76.25 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 41.52          | x 0.63        | x 0.7          | = 79.93 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 41.52          | x 0.63        | x 0.7          | = 40.35 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 24.19          | x 0.63        | x 0.7          | = 44.43 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 24.19          | x 0.63        | x 0.7          | = 46.57 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 24.19          | x 0.63        | x 0.7          | = 23.51 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 13.12          | x 0.63        | x 0.7          | = 24.09 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 13.12          | x 0.63        | x 0.7          | = 25.26 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 13.12          | x 0.63        | x 0.7          | = 12.75 (74)  |
| North        | 0.9x 0.77                 | x 6.01                 | x 8.86           | x 0.63        | x 0.7          | = 16.28 (74)  |
| North        | 0.9x 0.77                 | x 6.3                  | x 8.86           | x 0.63        | x 0.7          | = 17.07 (74)  |
| North        | 0.9x 0.77                 | x 1.59                 | x 8.86           | x 0.63        | x 0.7          | = 8.61 (74)   |
| South        | 0.9x 0.77                 | x 0.61                 | x 46.75          | x 0.63        | x 0.7          | = 17.43 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 76.57          | x 0.63        | x 0.7          | = 28.55 (78)  |
| South        | 0.9x 0.77                 | x 0.61                 | x 97.53          | x 0.63        | x 0.7          | = 36.37 (78)  |

# TER WorkSheet: New dwelling design stage

|            |      |      |   |      |   |        |   |      |   |     |   |        |      |
|------------|------|------|---|------|---|--------|---|------|---|-----|---|--------|------|
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.23 | x | 0.63 | x | 0.7 | = | 41.1   | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 114.87 | x | 0.63 | x | 0.7 | = | 42.83  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 110.55 | x | 0.63 | x | 0.7 | = | 41.22  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 108.01 | x | 0.63 | x | 0.7 | = | 40.27  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 104.89 | x | 0.63 | x | 0.7 | = | 39.11  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 101.89 | x | 0.63 | x | 0.7 | = | 37.99  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 82.59  | x | 0.63 | x | 0.7 | = | 30.79  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 55.42  | x | 0.63 | x | 0.7 | = | 20.66  | (78) |
| South      | 0.9x | 0.77 | x | 0.61 | x | 40.4   | x | 0.63 | x | 0.7 | = | 15.06  | (78) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 30.32  | x | 0.63 | x | 0.7 | = | 16.97  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 31.5   | x | 0.63 | x | 0.7 | = | 15.63  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 30.32  | x | 0.63 | x | 0.7 | = | 24.55  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 60.64  | x | 0.63 | x | 0.7 | = | 33.93  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 62.43  | x | 0.63 | x | 0.7 | = | 30.97  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 60.64  | x | 0.63 | x | 0.7 | = | 49.1   | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 103.31 | x | 0.63 | x | 0.7 | = | 57.82  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 105.22 | x | 0.63 | x | 0.7 | = | 52.2   | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 103.31 | x | 0.63 | x | 0.7 | = | 83.65  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 156.31 | x | 0.63 | x | 0.7 | = | 87.48  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 157.83 | x | 0.63 | x | 0.7 | = | 78.3   | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 156.31 | x | 0.63 | x | 0.7 | = | 126.56 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 196.72 | x | 0.63 | x | 0.7 | = | 110.09 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 197.69 | x | 0.63 | x | 0.7 | = | 98.08  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 196.72 | x | 0.63 | x | 0.7 | = | 159.28 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 203.69 | x | 0.63 | x | 0.7 | = | 113.99 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 204.35 | x | 0.63 | x | 0.7 | = | 101.38 | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 203.69 | x | 0.63 | x | 0.7 | = | 164.92 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 192.96 | x | 0.63 | x | 0.7 | = | 107.99 | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 193.73 | x | 0.63 | x | 0.7 | = | 96.12  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 192.96 | x | 0.63 | x | 0.7 | = | 156.24 | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 162.28 | x | 0.63 | x | 0.7 | = | 90.82  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 163.49 | x | 0.63 | x | 0.7 | = | 81.11  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 162.28 | x | 0.63 | x | 0.7 | = | 131.4  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 121.97 | x | 0.63 | x | 0.7 | = | 68.26  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 123.75 | x | 0.63 | x | 0.7 | = | 61.39  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 121.97 | x | 0.63 | x | 0.7 | = | 98.76  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 72.85  | x | 0.63 | x | 0.7 | = | 40.77  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 74.68  | x | 0.63 | x | 0.7 | = | 37.05  | (82) |
| Rooflights | 0.9x | 1    | x | 2.04 | x | 72.85  | x | 0.63 | x | 0.7 | = | 58.98  | (82) |
| Rooflights | 0.9x | 1    | x | 1.41 | x | 38.04  | x | 0.63 | x | 0.7 | = | 21.29  | (82) |
| Rooflights | 0.9x | 1    | x | 1.25 | x | 39.41  | x | 0.63 | x | 0.7 | = | 19.55  | (82) |



# TER WorkSheet: New dwelling design stage

## 9a. Energy requirements – Individual heating systems including micro-CHP)

### Space heating:

Fraction of space heat from secondary/supplementary system

0 (201)

Fraction of space heat from main system(s)

$(202) = 1 - (201) =$

1 (202)

Fraction of total heating from main system 1

$(204) = (202) \times [1 - (203)] =$

1 (204)

Efficiency of main space heating system 1

93.5 (206)

Efficiency of secondary/supplementary heating system, %

0 (208)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | kWh/year |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------|
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------|

Space heating requirement (calculated above)

|        |        |        |        |       |   |   |   |   |        |        |        |
|--------|--------|--------|--------|-------|---|---|---|---|--------|--------|--------|
| 827.31 | 644.04 | 516.16 | 257.13 | 87.45 | 0 | 0 | 0 | 0 | 312.49 | 595.66 | 846.51 |
|--------|--------|--------|--------|-------|---|---|---|---|--------|--------|--------|

$$(211)m = \{[(98)m \times (204)]\} \times 100 \div (206) \quad (211)$$

|        |        |        |        |       |   |   |   |   |        |        |        |
|--------|--------|--------|--------|-------|---|---|---|---|--------|--------|--------|
| 884.83 | 688.81 | 552.04 | 275.01 | 93.53 | 0 | 0 | 0 | 0 | 334.22 | 637.07 | 905.36 |
|--------|--------|--------|--------|-------|---|---|---|---|--------|--------|--------|

$$\text{Total (kWh/year)} = \text{Sum}(211)_{1...5,10...12} = \quad 4370.86 \quad (211)$$

Space heating fuel (secondary), kWh/month

$$= \{[(98)m \times (201)]\} \times 100 \div (208)$$

|   |   |   |   |   |   |   |   |   |   |   |   |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|---|---|---|---|---|---|---|---|---|---|---|---|

$$\text{Total (kWh/year)} = \text{Sum}(215)_{1...5,10...12} = \quad 0 \quad (215)$$

### Water heating

Output from water heater (calculated above)

|        |        |        |       |        |        |        |        |        |        |        |        |
|--------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|--------|
| 200.27 | 176.41 | 185.01 | 165.5 | 161.92 | 144.32 | 138.25 | 152.19 | 152.07 | 171.63 | 181.93 | 195.33 |
|--------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|--------|

Efficiency of water heater

79.8 (216)

|      |       |       |       |       |      |      |      |      |       |       |       |
|------|-------|-------|-------|-------|------|------|------|------|-------|-------|-------|
| 88.2 | 87.96 | 87.41 | 85.99 | 83.25 | 79.8 | 79.8 | 79.8 | 79.8 | 86.39 | 87.75 | 88.28 |
|------|-------|-------|-------|-------|------|------|------|------|-------|-------|-------|

Fuel for water heating, kWh/month

$$(219)m = (64)m \times 100 \div (217)m$$

|        |        |        |        |       |        |        |        |        |        |        |        |
|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|
| 227.08 | 200.55 | 211.67 | 192.47 | 194.5 | 180.85 | 173.24 | 190.71 | 190.56 | 198.66 | 207.33 | 221.26 |
|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|

$$\text{Total} = \text{Sum}(219a)_{1...12} = \quad 2388.88 \quad (219)$$

### Annual totals

Space heating fuel used, main system 1

**kWh/year**

4370.86

Water heating fuel used

2388.88

Electricity for pumps, fans and electric keep-hot

central heating pump:

30 (230c)

boiler with a fan-assisted flue

45 (230e)

Total electricity for the above, kWh/year

sum of (230a)...(230g) =

75 (231)

Electricity for lighting

371.02 (232)

## 12a. CO2 emissions – Individual heating systems including micro-CHP

|                               | Energy<br>kWh/year              | Emission factor<br>kg CO2/kWh | Emissions<br>kg CO2/year |
|-------------------------------|---------------------------------|-------------------------------|--------------------------|
| Space heating (main system 1) | (211) x                         | 0.216                         | = 944.11 (261)           |
| Space heating (secondary)     | (215) x                         | 0.519                         | = 0 (263)                |
| Water heating                 | (219) x                         | 0.216                         | = 516 (264)              |
| Space and water heating       | (261) + (262) + (263) + (264) = |                               | 1460.1 (265)             |

## TER WorkSheet: New dwelling design stage

|   |         |                        |   |         |       |
|---|---------|------------------------|---|---------|-------|
| Electricity for pumps, fans and electric keep-hot | (231) x | 0.519                  | = | 38.93   | (267) |
| Electricity for lighting                          | (232) x | 0.519                  | = | 192.56  | (268) |
| Total CO2, kg/year                                |         | sum of (265)...(271) = |   | 1691.59 | (272) |
| <b>TER</b> =                                      |         |                        |   | 28.3    | (273) |

# SAP 2012 Overheating Assessment

Calculated by Stroma FSAP 2012 program, produced and printed on 16 April 2020

## Property Details: Unit 1 Clean ASHP

|   |                         |
|---|-------------------------|
| <b>Dwelling type:</b>                             | Semi-detached House     |
| <b>Located in:</b>                                | England                 |
| <b>Region:</b>                                    | Thames valley           |
| <b>Cross ventilation possible:</b>                | Yes                     |
| <b>Number of storeys:</b>                         | 2                       |
| <b>Front of dwelling faces:</b>                   | North                   |
| <b>Overshading:</b>                               | Average or unknown      |
| <b>Overhangs:</b>                                 | None                    |
| <b>Thermal mass parameter:</b>                    | Indicative Value Medium |
| <b>Night ventilation:</b>                         | True                    |
| <b>Blinds, curtains, shutters:</b>                |                         |
| <b>Ventilation rate during hot weather (ach):</b> | 6 ( Windows fully open) |

## Overheating Details:

|  |        |      |
|--|--------|------|
| <b>Summer ventilation heat loss coefficient:</b> | 426.96 | (P1) |
| <b>Transmission heat loss coefficient:</b>       | 73.4   |      |
| <b>Summer heat loss coefficient:</b>             | 500.41 | (P2) |

## Overhangs:

| <b>Orientation:</b> | <b>Ratio:</b> | <b>Z_overhangs:</b> |
|---------------------|---------------|---------------------|
| North (North)       | 0             | 1                   |
| North (North)       | 0             | 1                   |
| North (Northx2)     | 0             | 1                   |
| South (South x2)    | 0             | 1                   |
| South (S FF)        | 0             | 1                   |
| South (S GF)        | 0             | 1                   |
| South (S FF)        | 0             | 1                   |

## Solar shading:

| <b>Orientation:</b> | <b>Z blinds:</b> | <b>Solar access:</b> | <b>Overhangs:</b> | <b>Z summer:</b> |      |
|---------------------|------------------|----------------------|-------------------|------------------|------|
| North (North)       | 1                | 0.9                  | 1                 | 0.9              | (P8) |
| North (North)       | 1                | 0.9                  | 1                 | 0.9              | (P8) |
| North (Northx2)     | 1                | 0.9                  | 1                 | 0.9              | (P8) |
| South (South x2)    | 1                | 0.9                  | 1                 | 0.9              | (P8) |
| South (S FF)        | 1                | 1                    | 1                 | 1                | (P8) |
| South (S GF)        | 1                | 1                    | 1                 | 1                | (P8) |
| South (S FF)        | 1                | 1                    | 1                 | 1                | (P8) |

## Solar gains:

| <b>Orientation</b> | <b>Area</b> | <b>Flux</b> | <b>g_</b> | <b>FF</b> | <b>Shading</b> | <b>Gains</b>           |
|--------------------|-------------|-------------|-----------|-----------|----------------|------------------------|
| North (North)      | 0.9 x 6.01  | 81.19       | 0.76      | 0.7       | 0.9            | 210.26                 |
| North (North)      | 0.9 x 6.3   | 81.19       | 0.76      | 0.7       | 0.9            | 220.4                  |
| North (Northx2)    | 0.9 x 3.18  | 81.19       | 0.76      | 0.7       | 0.9            | 111.25                 |
| South (South x2)   | 0.9 x 1.22  | 112.21      | 0.76      | 0.7       | 0.9            | 58.99                  |
|                    | 1 x 1.41    | 206.74      | 0.76      | 0.7       | 1              | 139.57                 |
|                    | 1 x 1.25    | 207.42      | 0.76      | 0.7       | 1              | 124.14                 |
|                    | 1 x 2.04    | 206.74      | 0.76      | 0.7       | 1              | 201.93                 |
| <b>Total</b>       |             |             |           |           |                | <b>1066.54 (P3/P4)</b> |

## Internal gains:

|                    | <b>June</b> | <b>July</b> | <b>August</b> |
|--------------------|-------------|-------------|---------------|
| Internal gains     | 499.01      | 480.09      | 488.54        |
| Total summer gains | 1642.97     | 1546.63     | 1389.04 (P5)  |

## SAP 2012 Overheating Assessment

|  |                        |               |               |      |
|--|------------------------|---------------|---------------|------|
| Summer gain/loss ratio                           | 3.28                   | 3.09          | 2.78          | (P6) |
| Mean summer external temperature (Thames valley) | 16                     | 17.9          | 17.8          |      |
| Thermal mass temperature increment               | 0.25                   | 0.25          | 0.25          |      |
| Threshold temperature                            | 19.53                  | 21.24         | 20.83         | (P7) |
| <b>Likelihood of high internal temperature</b>   | <b>Not significant</b> | <b>Slight</b> | <b>Slight</b> |      |

**Assessment of likelihood of high internal temperature:** Slight