

FLOOD RISK ASSESSMENT & DRAINAGE STRATEGY REPORT

*PROPOSED RESIDENTIAL DEVELOPMENT
ST MARGARET'S BUSINESS CENTRE
MOOR MEAD ROAD
TWICKENHAM
TW1 1JS*

PREPARED FOR: Sheen Lane Developments Ltd

JOB NO: P20-435A

DATE: 11 March 2022

ISSUE NO: 1



DOCUMENT HISTORY

| Issue No. | Description | Date |
|-----------|--------------------|----------|
| 1 | Issue for comment. | 11/03/22 |
| | | |
| | | |
| | | |

CONTENTS

1. INTRODUCTION..... 3

2. SITE LOCATION AND CHARACTERISTICS 3

3. PROPOSED SCHEME..... 5

4. FLOOD RISK POLICY & GUIDANCE 5

5. SOURCES OF FLOODING 6

6. THE SEQUENTIAL & EXCEPTION TEST..... 13

7. MANAGING THE RISK OF FLOODING..... 13

8. SURFACE WATER MANAGEMENT & DRAINAGE STRATEGY..... 14

9. CONCLUSIONS..... 21

APPENDICES

- APPENDIX A: TOPOGRAPHICAL SURVEY
- APPENDIX B: PLANNING DRAWINGS
- APPENDIX C: EA FLOOD RISK DATA
- APPENDIX D: THAMES WATER CORRESPONDENCE
- APPENDIX E: LONDON SUSTAINABLE DRAINAGE PROFORMA
- APPENDIX F: RUNOFF CALCULATIONS
- APPENDIX G: PROPOSED DRAINAGE STRATEGY PLAN
- APPENDIX H: DRAINAGE STRATEGY DESIGN RESULTS

1. INTRODUCTION

- 1.1 This report has been prepared on behalf of Sheen Lane Developments Ltd to accompany a planning application for a proposed residential development at St Margaret's Business Car Park in Moor Mead Road, Twickenham.
- 1.2 The report assesses flood risk associated with the development proposals, closely following guidance set out in the National Planning Policy Framework (NPPF), the associated Planning Practice Guidance, Policy LP 21 (Flood Risk & Sustainable Drainage) of the London Borough of Richmond Adopted Local Plan and the London Borough of Richmond upon Thames Strategic Flood Risk Assessment – Level 1 Update (March 2021).
- 1.3 The report also details a strategy for the disposal of foul and surface water runoff from the development, closely following guidance on sustainable drainage set out in the London Sustainable Drainage Proforma that was adopted by the London Borough of Richmond upon Thames in April 2019.

2. SITE LOCATION AND CHARACTERISTICS

Site Location

- 2.1 The site is located at St Margaret's Business Park in Moor Mead Road Twickenham, TW1 1JS as shown on *Figure 1* below. The site is centred on Ordnance Survey grid reference TQ 16645 74123 and co-ordinates X: 516645, Y: 174123.



Figure 1: Site Location

Site Description

- 2.2 The sites measured area is approximately 0.06 Ha and presently comprises of a parking area as shown on the topographical survey included in *Appendix A*.

Topography

- 2.3 The topographical survey included in *Appendix A*, shows site levels to be between 6.00mAOD to 6.40mAOD.

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|--------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 3 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

Existing Ground Conditions

2.4 *Figure 2 and Figure 3 below have been taken from the British Geological Survey website and show the superficial geology of the local area to comprise of the Kempton Park Gravel Member, while the bedrock geology is shown to comprise the London Clay Formation. The Kempton Park Gravel Member is indicated to comprise of Sands and Gravels while the London Clay Formation is indicated to comprise of Clays and Silts.*

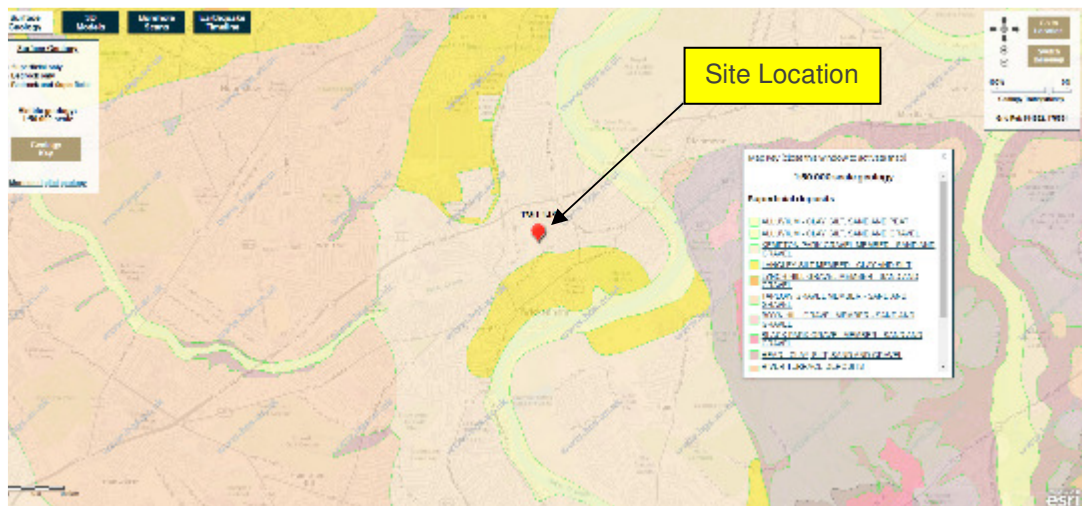


Figure 2: BGS Superficial Geology Map

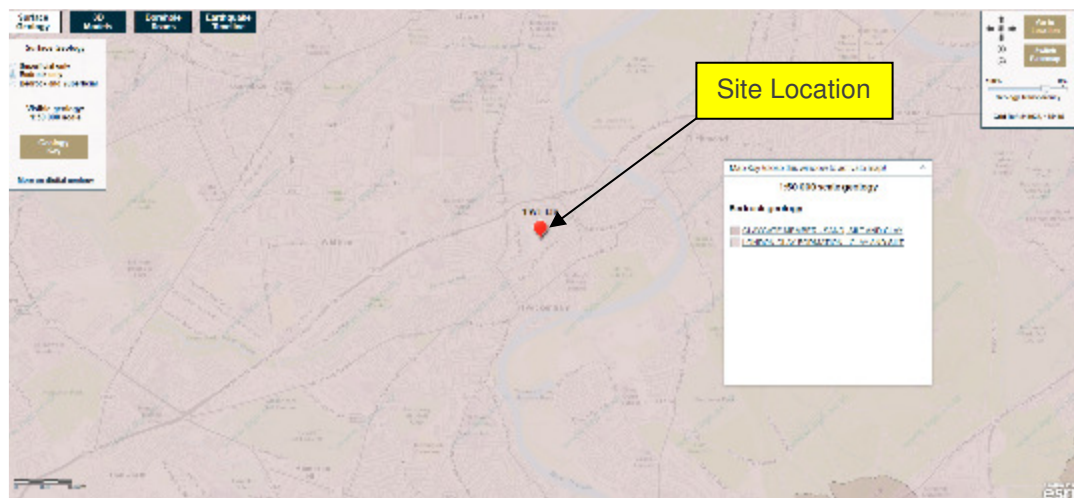


Figure 3: Bed Rock Geology Map

Existing Drainage Arrangements

2.5 *Figure 5 below shows an extract from sewer records provided by Thames Water. The extract shows the local area to be drained by a network of foul and surface water networks present in the surrounding road network.*

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|--------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 4 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

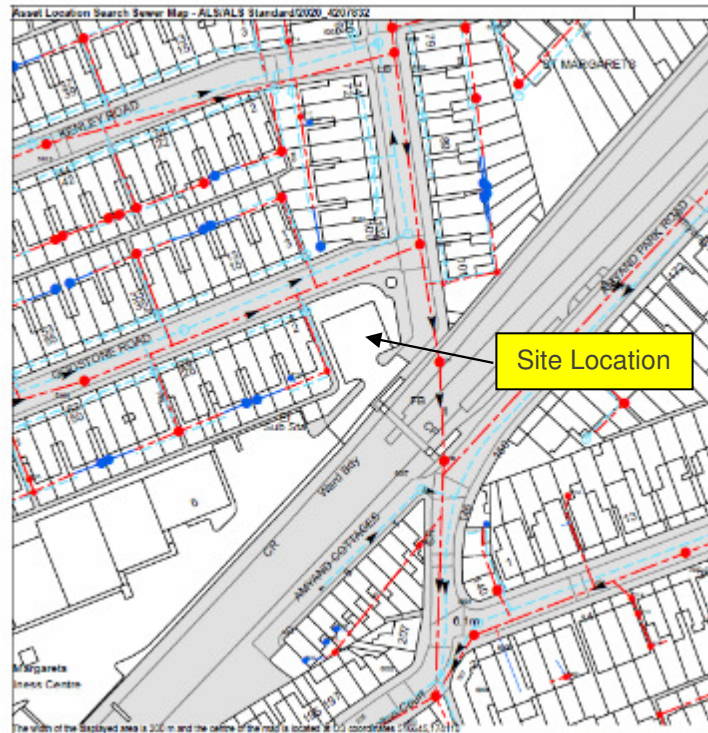


Figure 4: Thames Water Sewer Records

2.6 The topographical survey included in *Appendix A* shows the existing car park to be drained by a dished channel and road gullies.

3. PROPOSED SCHEME

3.1 The proposed development comprises 3 No. residential dwellings with associated gardens and parking spaces.

3.2 A set of drawings illustrating the development proposals is included in *Appendix B*.

4. FLOOD RISK POLICY & GUIDANCE

4.1 At a national level, the National Planning Policy Framework (NPPF) and the Planning Practice Guidance (PPG) to the NPPF ensure flood risk is taken into account at all stages of the planning process, to avoid inappropriate development in areas at risk of flooding and to direct development towards areas at lowest flood risk. The NPPF retains a risk-based approach to the planning process and defines four Flood Zones to be used as the basis for applying the sequential test, as well as flood risk vulnerability classifications, which define the type of development that is considered appropriate within each zone.

4.2 The NPPF establishes the Flood Zones as the starting point for assessment with the overarching aim to steer new development to areas with the lowest probability of flooding. Flood Zone maps are available on the GOV.UK website and the definitions of the Flood Zones extracted from the National Planning Policy Framework (NPPF) are described below:

- Flood Zone 1 – Low probability. This zone comprises land assessed as having a less than 1 in 1,000 annual probability of river or sea flooding (<0.1%).

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|--------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 5 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

- Flood Zone 2 – Medium probability. This zone comprises land assessed as having between a 1 in 100 and 1 in 1,000 annual probability of river flooding (1% - 0.1%), or between a 1 in 200 and 1 in 1,000 annual probability of sea flooding (0.5% - 0.1%) in any year.
- Flood Zone 3a – High probability. This zone comprises land assessed as having a 1 in 100 or greater annual probability of river flooding (>1%), or a 1 in 200 or greater annual probability of flooding from the sea (>0.5%) in any year.
- Flood Zone 3b – The functional floodplain. This zone comprises land where water has to flow or be stored in times of flood. Typically, land which would flood with an annual probability of 1 in 20 (0.5%) or greater in any year, or is designed to flood in an extreme (0.1%) flood.

4.3 Policy LP 21 (Flood Risk & Sustainable Drainage) of Richmond upon Thames Adopted Local Plan adopts similar principles to the NPPF and identifies that Level 1 Strategic Flood Risk Assessment should be used to inform site specific flood risk assessments in the district. The following section of this report reviews flood risk associated with sources of flooding identified within the Level 1 SFRA and the EA’s online flood risk maps.

5. SOURCES OF FLOODING

Fluvial Flooding

5.1 The flood zone map in *Figure 5* below has been taken from EA’s website and shows the site to be in Flood Zone 2 associated with the River Crane.

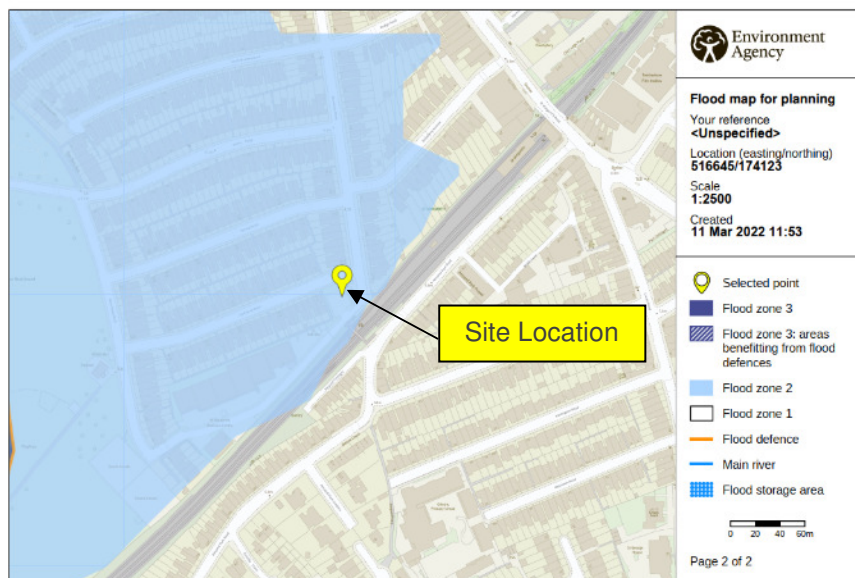


Figure 5: EA Flood Zone Map

5.2 The risk of river / tidal flood map taken from the EA’s website in *Figure 6* below shows the shows the risk of fluvial flooding to be low.

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|--------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 6 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |



Figure 6: EA Risk of Fluvial / Tidal Flooding Map

5.3 The flood zone map in Figure 7 below has been generated from interactive mapping developed to accompany the Level 1 SFRA. The map shows the flood zones to be consistent with the EA flood zone with the site shown to be in Flood Zone 2. The site is also shown to be in an EA flood alert area.

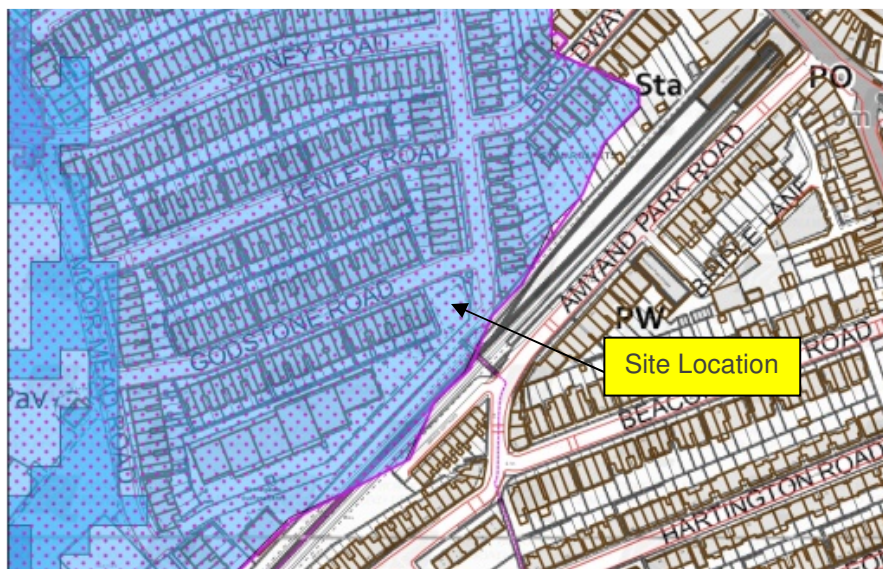


Figure 7: Level 1 SFRA Flood Zone Map

5.4 The flood zone maps available on the EA's website and within the SFRA are produced from a combination of a national generalised computer model, detailed modelling and some historic flood event outlines and are intended as a guide only. More detailed flood data received from the EA is included in Appendix C.

5.5 The data received from the EA includes a set of flood maps for various Annual Exceedance Probabilities (AEP) at a number of modelled floodplain nodes within and surrounding the site. The maps are shown in Figure 8, Figure 9 and Figure 10 below.

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|--------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 7 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | | GSC |

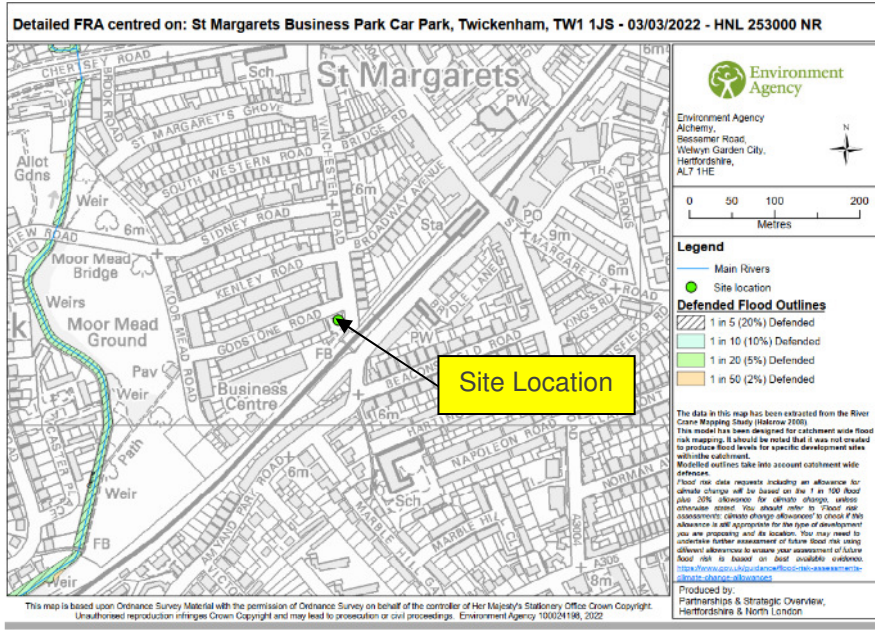


Figure 8: Defended Flood Outline Map 1

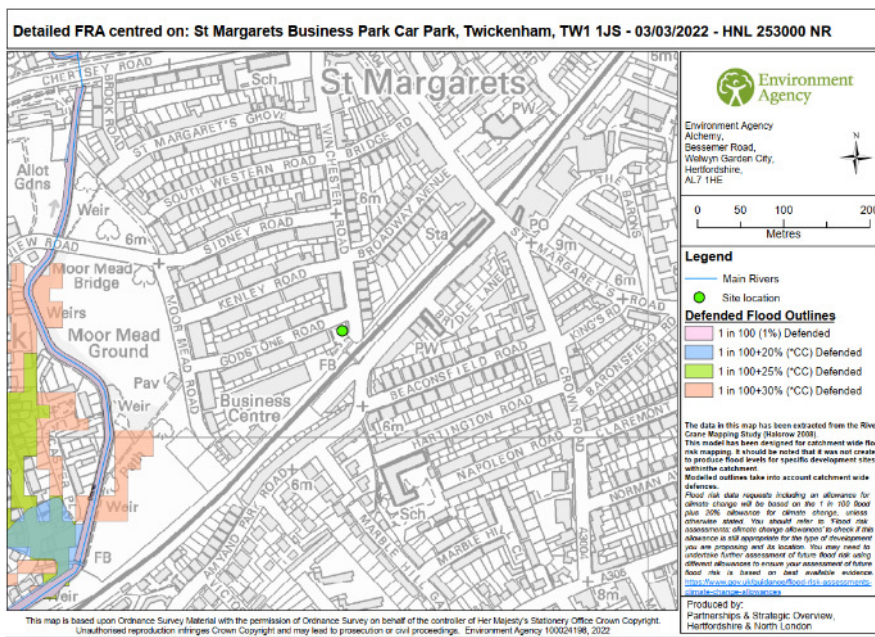


Figure 9: Defended Flood Outline Map 2

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|--------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 8 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

Detailed FRA centred on: St Margarets Business Park Car Park, Twickenham, TW1 1JS - 03/03/2022 - HNL 253000 NR

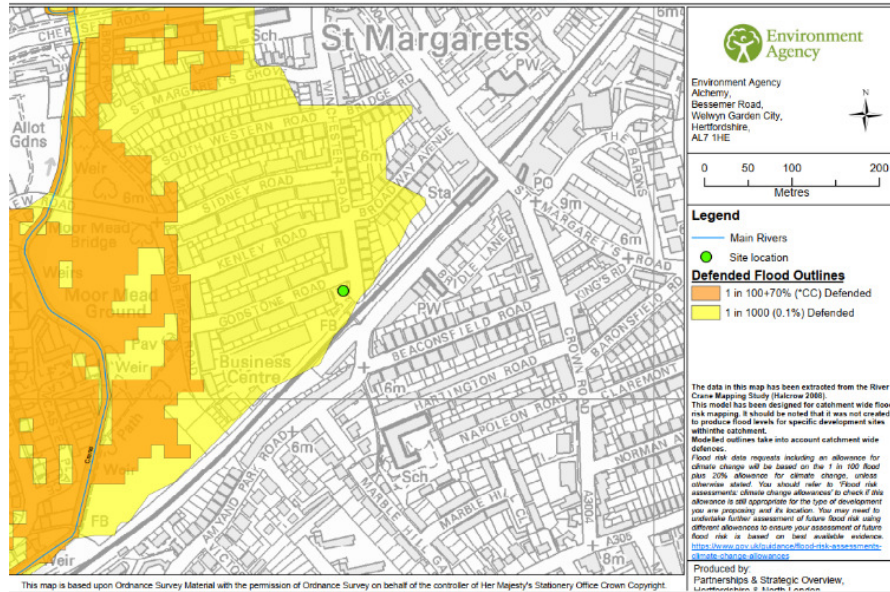


Figure 10: Defended Flood Outline Map 3

5.6 Figure 8, Figure 9 and Figure 10 show the site and immediate surrounding area to be unaffected by the 1% plus climate change AEP's but within the flood outline associated with the 0.1% AEP. Figure 11 below shows the predicted flood level associated with the 0.1% AEP to be 6.34mAOD at the site.

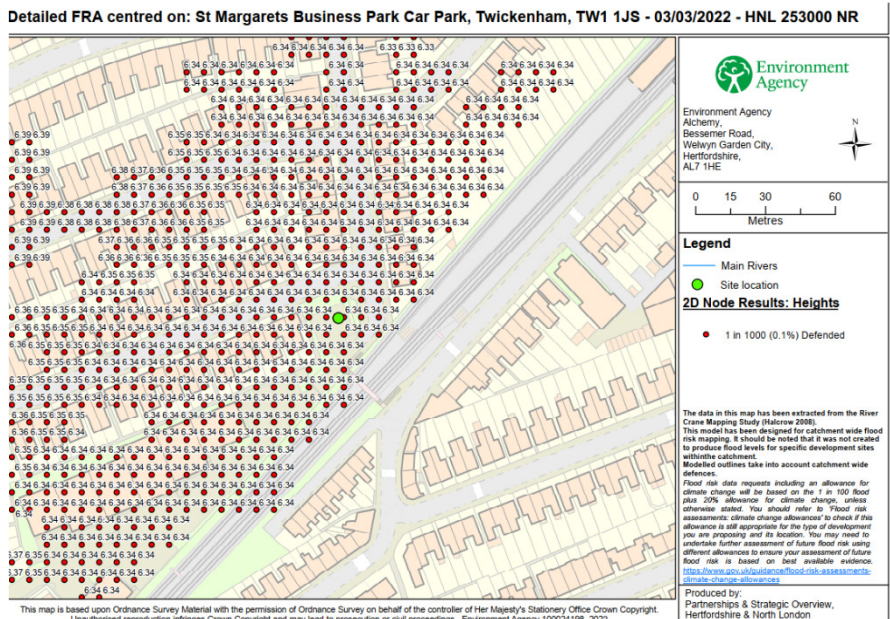


Figure 11: 0.1% AEP Defended Flood Levels

Surface Water Flooding

5.7 The EA have modelled locations along critical flow paths and areas situated in topographic depressions, which could flood following an extreme rainfall event. Figure 12 below, shows a surface water flood risk map taken from the EA's website with the location of the site identified.

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|--------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 9 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

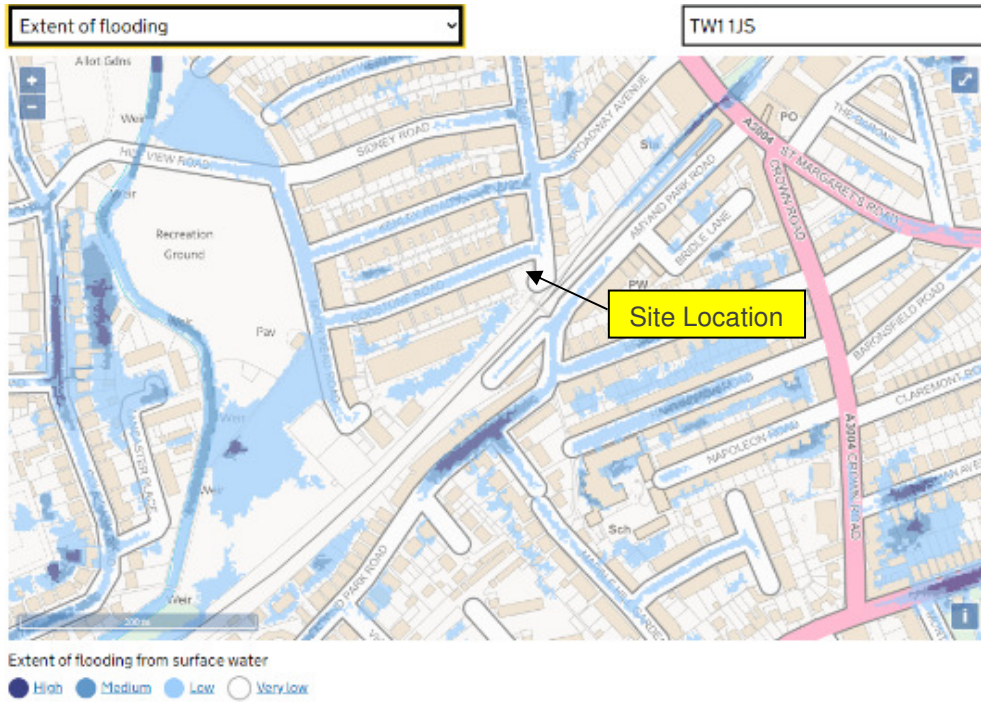


Figure 12: EA Surface Water Flood Risk Map

5.8 Figure 12 indicates the site to not be affected by surface water flooding. Figure 13 below, shows a surface water flood risk map generated from interactive mapping developed to accompany the Level 1 SFRA. The map shows the site to not be affected by surface water indicated for up to a 1 in 1000 year event.

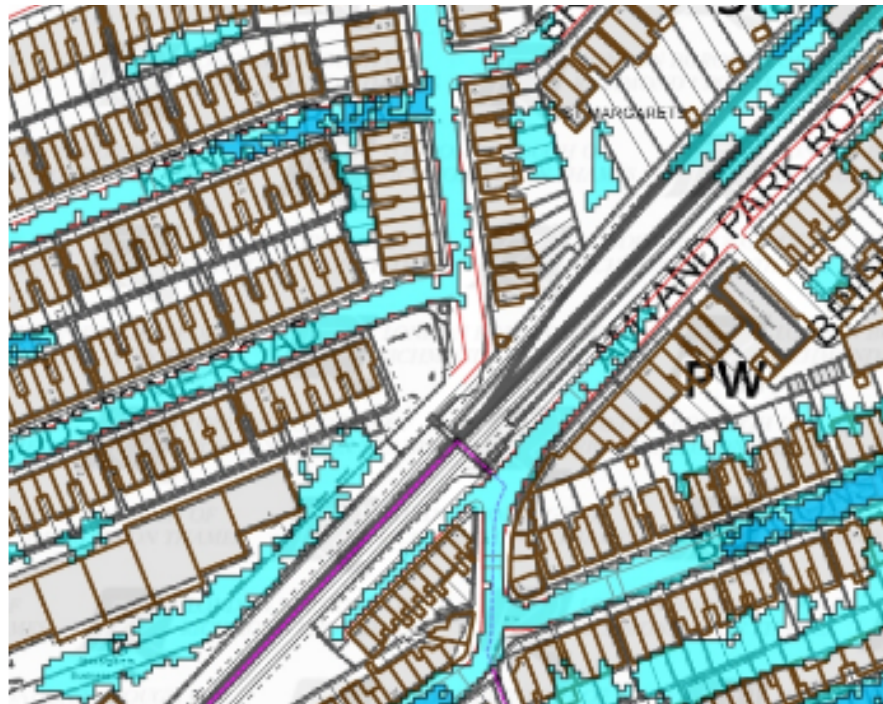


Figure 13: Level 1 Surface Water Flood Risk Map

Groundwater Flooding

5.9 The Susceptibility to Groundwater Flooding Map in *Figure 14* below has been generated from interactive mapping developed to accompany the Level 1 SFRA. The map shows the site to be located in an area where there is potential for groundwater flooding to occur at the surface.



Figure 14: SFRA Susceptibility to Groundwater Flooding Map

Sewer Flooding

5.10 The Sewer Flooding Incidents Map in *Figure 15* below has been generated from interactive mapping developed to accompany the Level 1 SFRA. The map shows the local post code to be an area where there have been between 0 to 10 incidents of sewer flooding have been reported.



Figure 15: SFRA Sewer Flooding Incidents Map

5.11 Correspondence received from Thames Water is included in *Appendix D*, which advises that there have been no incidents of flooding at the site as a result of surcharging public sewers.

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|---------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 11 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

5.12 The correspondence also confirms that the existing foul sewer network would have sufficient capacity for foul water flows from the development and that Thames Water would accept the discharge of surface water runoff from the development to the surface water sewer network at a rate of 2.0 l/s if it is not possible to discharge runoff by infiltration or to a watercourse.

Flooding from Artificial Sources

5.13 Flooding from artificial sources, is most likely to result from burst water mains or from infrastructure failure in an artificial watercourse or water body, i.e. canals or other water features such as reservoirs.

5.14 Flood maps associated with large reservoirs that hold over 25,000 cubic meters of water are available on the EA website. The maps help to identify areas that could potentially be affected by reservoir flooding and display a realistic worst case scenario of the largest area that may be flooded if a reservoir were to fail and release the water it holds.

5.15 *Figure 16* below shows a Reservoir Flood Map taken from the EA’s website. The map shows the site to be at risk of flooding from reservoirs.



Figure 16: EA Reservoir Flood Map

5.16 The risk of failure of reservoirs is low as they are maintained, improved and regularly inspected by Thames Water.

5.17 Flood patterns associated with burst water mains would be similar to surface water flood patterns, which have been assessed to be low.

6. THE SEQUENTIAL & EXCEPTION TEST

- 6.1 The National Planning Policy Framework (NPPF) encourages a sequential risk-based approach to determine the suitability of land for development in flood risk areas. It advises local planning authorities to demonstrate that there are no reasonably available sites in areas with a lower probability of flooding that would be appropriate to the type of development or land use proposed.
- 6.2 In areas at risk of river flooding, NPPF advises that preference be given to new development in Flood Zone 1. If there are no reasonably available sites in Flood Zone 1 the flood vulnerability of the development can be considered in locating development in Flood Zone 2 and then Flood Zone 3. Within each flood zone new development should be directed to sites at the lowest probability of flooding from all sources.
- 6.3 In Section 5 it was established that the site lies in Flood Zone 2. The NPPF and Local Policy of the London Borough of Richmond upon Thames advises that residential developments are a more vulnerable use and appropriate in Flood Zone 2 provided they pass the sequential test with it not being necessary to apply the exception test.

7. MANAGING THE RISK OF FLOODING

- 7.1 Section 5 established the site to be in Flood Zone 2, which is an area assessed to be at medium probability of flooding from the River Crane. The site-specific requirements for flood risk assessments within Flood Zone 2 from the Level 1 SFRA are outlined below.
- For all sites within Zone 2 Medium Probability, a high-level FRA should be prepared based upon readily available existing flooding information, sourced from the EA. It will be necessary to demonstrate that the residual risk of flooding to the property is effectively managed through, for example, the provision of raised floor levels and the provision of a planned evacuation route and / or safe haven.
 - The risk of other sources of flooding (e.g. urban drainage and/or groundwater) must be considered, and sustainable urban drainage techniques must be employed to ensure no worsening to existing flooding problems elsewhere within the area.
 - As part of the high-level FRA, the developer must provide a clear and concise statement summarising how the proposed (re)development has contributed to a positive reduction in flood risk within the Borough.
 - Details of proposed sustainable drainage systems (SuDS) that will be implemented to ensure that runoff from the site (post redevelopment) does not exceed greenfield runoff rates. Any SuDS design must take due account of groundwater and geological conditions.
- 7.2 The measures summarised under the headings below sets out recommendations on how the development could comply with these requirements.

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|---------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 13 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

Floor Levels

- 7.3 It is recommended that that the residual risk of flooding to the property is effectively managed by setting proposed buildings ground floor levels above the predicted flood level of 6.34mAOD for the 0.1% AEP.

Access / Egress

- 7.4 The flood outline maps provided by the Environment Agency for the 1% plus climate change AEP's showed the site and immediate surrounding area to not be affected by flooding associated with such events. Therefore access / egress routes are not expected to be compromised in such conditions. There would be a residual risk of access / egress routes been compromised by flood events exceeding the 1% plus climate change event, however, the raised floor levels would ensure that the dwellings provide a safe haven for residents in such conditions.

Other sources

- 7.5 Raising the proposed buildings floor level would largely address the risk of flooding from other sources. However, National and Local Policy requires development to seek opportunities to reduce the overall level of flood risk in the area and beyond through the use of Sustainable Drainage Systems (SuDS). The following section of this report sets out a strategy for the management of surface water runoff from the development using SuDS.

8. SURFACE WATER MANAGEMENT & DRAINAGE STRATEGY

- 8.1 This section of the report outlines an approach for the disposal and management of surface water runoff from the development, with it expected that any further details of the strategy could be provided via a condition of the planning permission once detailed design information and construction drawings are available for the relevant phase of the development.

Surface Water Drainage Policy & Guidance

- 8.2 The London Borough of Richmond upon Thames are one of London's 33 Lead Local Flood Authorities (LLFA's) that have adopted the London Sustainable Drainage (SuDS) Proforma.
- 8.3 SuDS encompass a wide range of drainage techniques intended to minimise the rate of discharge, volume and environmental impact of runoff and include; blue / green roofs; rainwater harvesting; soakaways / infiltration systems / infiltration trenches / permeable paving; swales / basins / ponds / wetlands / below ground attenuation tanks.
- 8.4 The proforma advises that drainage strategies for developments in the London Borough of Richmond upon Thames need to comply with the following policies on SuDS:
- London Borough of Richmond upon Thames Local Plan policy LP21
 - London Plan policy 5.13 and draft New London Plan policy SI13
 - The National Planning Policy Framework (NPPF)

- 8.5 Section C of policy LP21 advises the following:

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|---------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 14 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

- The Council will require the use of Sustainable Drainage Systems (SuDS) in all development proposals. Applicants will have to demonstrate that their proposal complies with the following:
 - a) A reduction in surface water discharge to greenfield run-off rates wherever feasible.
 - b) Where greenfield run-off rates are not feasible, this will need to be demonstrated by the applicant, and in such instances, the minimum requirement is to achieve at least a 50% attenuation of the site's surface water runoff at peak times based on the levels existing prior to the development.

8.6 Section 6.2.22 of policy LP 21 advises that to reduce the risk of surface water and sewer flooding, all development proposals in the borough that could lead to changes to, and have impacts on, surface water run-off are required to follow the London Plan drainage hierarchy. The London Plan policy 5.13 advises the following:

- Development should utilise SUDS unless there are practical reasons for not doing so, and should aim to achieve greenfield run-off rates and ensure that surface water run-off is managed as close to its source as possible in line with the following drainage hierarchy:
 - i. Store rainwater for later use.
 - ii. Use infiltration techniques, such as porous surfaces in non-clay areas.
 - iii. Attenuate rainwater in ponds or open water features for gradual release.
 - iv. Attenuate rainwater by storing in tanks or sealed water features for gradual release.
 - v. Discharge rainwater direct to a watercourse.
 - vi. Discharge rainwater to a surface water sewer/drain.
 - vii. Discharge rainwater to the combined sewer.
- Drainage should be designed and implemented in ways that deliver other policy objectives of the Plan, including water use efficiency and quality, biodiversity, amenity and recreation

8.7 The Sustainable Design & Construction Supplementary Planning Guidance (SPG) document provides further guidance on the implementation of London Plan policy. Chapter 3 of the SPG advises that London Plan policy recommends that developers should aim for a greenfield runoff rate from their developments with greenfield runoff rates defined as the runoff rates from a site, in its natural state, prior to any development. However, the SPG notes that runoff rates should not be more than three times the calculated greenfield rate on previously developed sites. The only exceptions to this, where greater discharge rates may be acceptable, are where a pumped discharge would be required to meet the standards or where surface water drainage is to tidal waters and therefore would be able to discharge at unrestricted rates provided unacceptable scour would not result.

8.8 The NPPF advise that Major developments should incorporate sustainable drainage systems unless there is clear evidence that this would be inappropriate. The systems used should:

- a) take account of advice from the lead local flood authority;
- b) have appropriate proposed minimum operational standards;

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|---------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 15 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

- c) have maintenance arrangements in place to ensure an acceptable standard of operation for the lifetime of the development;
- d) where possible, provide multifunctional benefits.

8.9 The proforma is required to accompany a drainage strategy prepared for a planning application where required by national or local planning policy. It is to be used to summarise the key outputs from the strategy to allow assessing officers at the LLFA to quickly assess compliance with the above SuDS planning policies. A completed proforma is included in *Appendix E*, while further supporting information in connection with the surface water drainage strategy is provided under the following headings.

Proposed discharge arrangement

8.10 The proforma sets out a hierarchy for the discharge of surface water runoff. The methods of discharge are summarised in *Table 1* below with an assessment of each methods suitability.

Table 1: Surface Water Runoff Discharge Method

| System | Assessment |
|--|--|
| Store rainwater for later use | Rainwater harvesting is the collection of rainwater runoff for use. Runoff can be collected from roofs and then used in place of mains water for certain applications. It is likely that rainwater butts could be used to collect roof water for the purposes of irrigating domestic gardens. More complex systems are also available to reduce mains water consumption in the form of harvesting systems that can store rainwater for re-use for toilet flushing. However, the proposed building footprints will occupy most of the site leaving limited space for above and below ground rainwater harvesting. Therefore, rainwater harvesting has not been considered as part of the surface water drainage strategy for the development. |
| Use infiltration techniques, such as porous surfaces in non-clay areas | In Section 2 it was identified that the bedrock geology of the local area is shown to be the London Clay Formation, which comprises of Clays and Silts that would be expected to be relatively impermeable in nature. In addition, in Section 4 it was identified that the site is shown to be located in an area where there is potential for groundwater flooding to occur at the surface. Therefore, infiltration techniques, such as porous surfaces in non-clay areas are not assessed to be appropriate. |
| Attenuation of rainwater in ponds and open water features | The development falls in a town centre environment and areas of soft landscaping are limited to private gardens with no space available for ponds and open water features. |
| Attenuation of rainwater through tanks or sealed water features | An area of shared parking is proposed as part of the development and a below ground storage tank could be considered beneath this area. |
| Discharge rainwater direct to a watercourse | The nearest watercourse is located over 250m to the west of the site. Given the substantial distance, it would not be a viable destination for surface water runoff. |
| Discharge rainwater to a surface water sewer/drain | A surface water sewer network is present in the roads adjacent the site. Thames Water have advised that it would be acceptable to discharge surface water runoff from the development to the network if flows are restricted to a maximum discharge rate of 2.0 l/s and if other methods of disposal in the surface water drainage hierarchy have been investigated and proven to not be viable. Correspondence received from Thames Water is included in <i>Appendix D</i> . |

| | |
|--|---|
| Discharge rainwater to the combined sewer. | As it has been established that discharge from the development could be made to a surface water sewer, it is not appropriate to consider discharge to a combined sewer. |
|--|---|

8.11 Based on the assessment in *Table 1*, it is assessed to be appropriate to discharge surface water runoff from the development to the surface water sewer network, if flows are restricted to a maximum discharge rate of 2.0 l/s.

Runoff Management

8.12 The proforma requires an assessment of greenfield and existing discharge rates. Greenfield runoff rates for the required storm events have been estimated based on the IH 124 Facility of the MicroDrainage Software Package. The calculation results are included in *Appendix F* and are based on the sites area of 0.06 Ha. The calculated rates for a variety of storm events up to the 1 in 100-year return period are summarised in *Table 2* below.

Table 2: Runoff Rates

| Return Period (Year) | Greenfield Runoff Rate (l/s) | Existing Discharge Rate (l/s) |
|----------------------|------------------------------|-------------------------------|
| QBAR | 0.9 | N/A |
| 1 | 0.7 | 2.3 |
| 30 | 1.5 | 5.1 |
| 100 | 1.7 | 6.6 |

8.13 Discharge rates for the existing brownfield site are also shown in *Table 2*, which have been established using the Modified Rational Method Formula based on 360-minute rainfall profiles. The Modified Rational Method calculations and rainfall profiles are included in *Appendix F*. The calculation results are also based on the sites area of 0.06 Ha.

8.14 Policy LP 21 requires a reduction in surface water discharge to greenfield run-off rates wherever feasible. Therefore, it is proposed to limit the rate of discharge from the development to a maximum allowable discharge rate of 1.7 l/s. This would be less than the discharge limit of 2.0 l/s recommended by Thames Water so would also comply with their requirements.

8.15 Surface water runoff exceeding the proposed discharge limit of 1.7 l/s would need to be stored and attenuated on site for all rainfall events up to and including a 1 in 100 year event with a 40% allowance for potential future increases in rainfall intensities associated with climate change. The MicroDrainage quick storage estimate tool has been used to estimate the required storage volume with the results shown in *Figure 17* below. The results are based on a drained area of 273m², which includes for the developments roof area, parking area and a 10% allowance for creep.

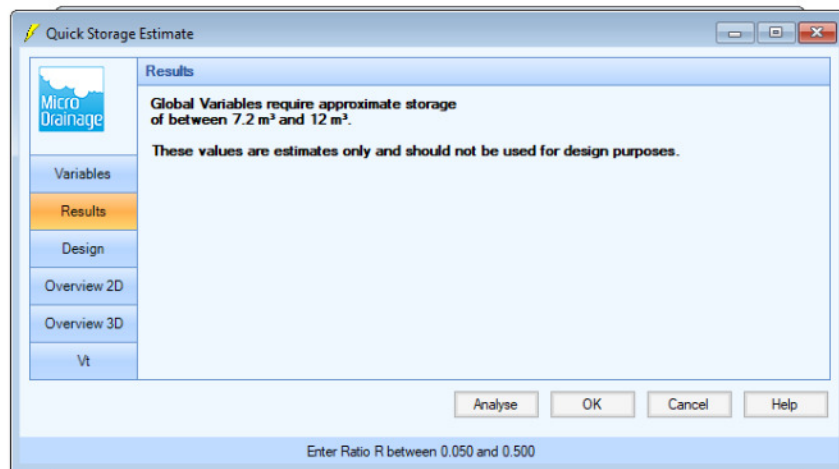
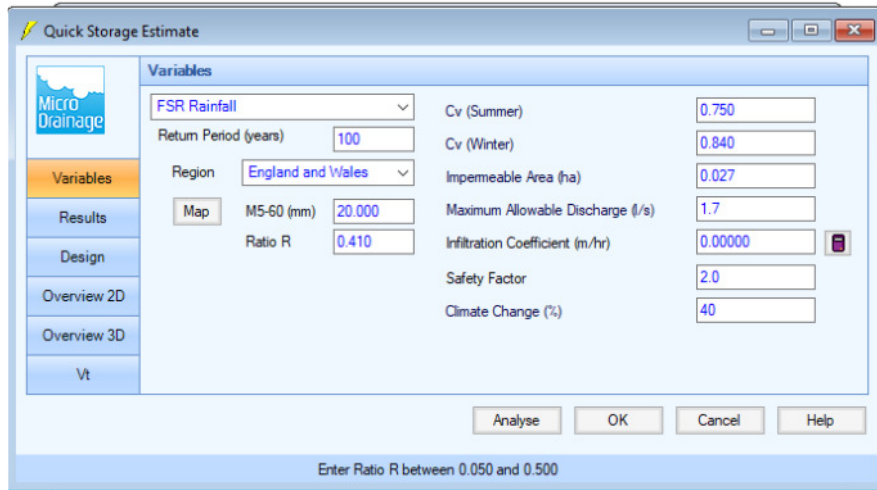


Figure 17: MicroDrainage Quick Storage Estimate

- 8.16 Figure 17 shows that an estimated storage volume of between 7.2m³ to 12.0m³ would be required to store surface water runoff on site for a 1 in 100 year event with a 40% allowance for climate change.

Sustainable Drainage Systems (SuDS)

- 8.17 The London Borough of Richmond upon Thames surface water drainage policy recommends that the development should aim to restrict surface water flows from the site to greenfield runoff rates using SuDS to control surface water as close to the source as possible. Table 3 below lists a range of SuDS techniques that can be used to minimise the rate of discharge, volume and environmental impact of runoff and provides an assessment of each methods suitability.

Table 3: SUDS Assessment

| System | Assessment |
|--|--|
| Rainwater Harvesting / Attenuation Tanks | Rainwater harvesting is the collection of rainwater runoff for use. Runoff can be collected from roofs and then used in place of mains water for certain applications. It is likely that rainwater butts could be used to collect roof water for the purposes of irrigating domestic gardens. More complex systems are also available to reduce mains water consumption in the form of harvesting systems that can store rainwater for re-use for toilet flushing. |

| | |
|--|--|
| | However, the proposed building footprints will occupy most of the site leaving limited space for above and below ground rainwater harvesting. Therefore, rainwater harvesting has not been considered as part of the surface water drainage strategy for the developments. |
| Infiltration Systems | In Section 2 it was identified that the bedrock geology of the local area is shown to be the London Clay Formation, which comprises of Clays and Silts that would be expected to be relatively impermeable in nature. In addition, in Section 4 it was identified that the site is shown to be located in an area where there is potential for groundwater flooding to occur at the surface. Therefore, infiltration systems are not assessed to be appropriate. |
| Blue / Green Roofs | The proposed buildings roof structure will comprise of pitched roof profiles, which would not be suitable for blue / green roof systems. |
| Swales / Basins / Ponds / Wetlands | The development falls in a town centre environment and areas of soft landscaping are limited to private gardens with no space available for swales, basins, ponds, or wetlands. |
| Bioretention / tree pits | The development falls in a town centre environment and areas of soft landscaping are limited to private gardens with no space available for bioretention or tree pits. |
| Filter Strips / Filter Drains / Pervious Pavements | Although infiltration systems are not considered to be appropriate for the site, pervious pavements and filter drains could be used to intercept / retain / treat precipitation as well as reduce runoff rates from paved surfaces provided that they are connected to a surface water drainage network. |
| Attenuation Tanks | An area of shared parking is proposed as part of the development and a below ground storage tank could be considered beneath this area for the attenuation of surface water and for gradual release. |

Drainage Strategy

8.18 Based on the assessment in *Table 3*, a surface water drainage scheme has been developed for the site and is shown on the proposed drainage strategy plan included in *Appendix G*. A description of the proposals is provided below.

- Roof water runoff from dwellings would be captured by a combination of rainwater gutters, downpipes that would discharge to rainwater butts where feasible for the purposes of irrigating domestic gardens.
- The parking spaces are shown to be constructed using a pervious pavement system, which would allow surface water runoff to filter into a 525mm thick layer of porous sub-base, providing 9.2m³ of storage volume for the attenuation of surface water runoff.
- The pervious pavement system would be lined with an impermeable geomembrane to prevent groundwater from entering the system.
- The roof drainage systems would connect to a traditional network of below ground pipework, which would discharge to the zone of porous sub-base located beneath the shared parking spaces.
- The outfall from the system would be restricted to a maximum allowable discharge rate of 1.7 l/s using a flow control chamber before discharging the surface water sewer network and the below ground geocellular storage tank and pervious pavement system would store excess runoff for all storm return periods up to and including a 1 in 100 year event with 40% allowance for climate change.

- 8.19 Design results for the system are included in *Appendix H*. A summary of the design results is provided in *Table 4* below.

Table 4: System Design Results

| Catchment Area (m ²) | Max. Storage Volume (m ³) | Discharge Rate (l/s) | | | |
|----------------------------------|---------------------------------------|----------------------|---------|----------|----------------|
| | | 1 in 1 | 1 in 30 | 1 in 100 | 1 in 100 + 40% |
| 272 | 9.2 | 0.7 | 1.2 | 1.4 | 1.7 |

- 8.20 The design results show that the system would store surface water up to and including a 1 in 100-year rainfall event with 40% allowance for climate change.
- 8.21 *Table 5* below compares the combined maximum rate of discharge analysed for each storm event to the greenfield / brownfield runoff rates identified in *Table 4*.

Table 5: Comparison of Discharge Rates

| Return Period | Greenfield | Brownfield | |
|---------------|------------------------|-----------------------|------------------------|
| | | Pre-Development | Post-Development |
| | Peak Runoff Rate (l/s) | 6hr Runoff Rate (l/s) | Peak Runoff Rate (l/s) |
| 1 | 0.7 | 2.3 | 0.7 |
| 30 | 1.5 | 5.1 | 1.2 |
| 100 | 1.7 | 6.6 | 1.4 |
| 100+40 | 1.7 | 6.6 | 1.7 |

- 8.22 The above table shows that surface water flows from the development would be less than or equal to the greenfield runoff rate for all analysed rainfall events up to and including the 1 in 100 year return period with 40% allowance for climate change. This would be in accordance with the London Borough of Richmond upon Thames surface water drainage policy and advice received from Thames Water, with flows not exceeding their recommended restricted rate of discharge of 2.0 l/s.

Exceedance

- 8.23 Overland surface water flows resulting from exceedance of the drainage systems capacity or resulting from a blockage should be managed in a manner that minimises the risks to people and property.
- 8.24 If the capacity of these systems was exceeded, the buildings would still be protected from surface water flooding as the ground levels of buildings would be raised above surrounding road and landscaping levels.

Water Quality

- 8.25 The proposed SuDS systems would fulfil the water quality aims of the London Borough of Richmond upon Thames surface water drainage policy. The CIRIA C753 SuDS Manual 2015 sets out requirements for delivering appropriate levels of treatment to surface water runoff using SuDS. *Table 6* below identifies that the proposed SuDS components would have a total pollution mitigation index equal to or

exceeding the recommended pollution hazard index thus confirming the SuDS components would provide suitable treatment to surface water runoff.

Table 6: Comparison of Discharge Rates & Volumes

| Use | Pollution Hazard Index | | | SUDS Component | Mitigation Index | | |
|-----------------|------------------------|--------|------|-------------------|------------------|--------|-----|
| | TSS | Metals | TPH | | TSS | Metals | TPH |
| Roof | 0.3 | 0.2 | 0.05 | Porous Sub-base | 0.4 | 0.4 | 0.4 |
| Roads / Parking | 0.5 | 0.4 | 0.4 | Pervious Pavement | 0.7 | 0.6 | 0.7 |

Amenity / Biodiversity

- 8.26 The new gardens proposed for the development would maximise amenity and biodiversity benefits, over the existing situation.

Maintenance

- 8.27 Property owners would be responsible for the maintenance of the drainage systems within their individual properties, while shared drainage systems forming part of the estate would be maintained as part of wider communal infrastructure by a management company. On occupation of the development, a maintenance and management plan would be incorporated into each developments Operation and Maintenance Manual with the as-built drainage system operated and maintained in accordance with the regime set out in the plan.

9. CONCLUSIONS

- 9.1 It has been established that the site is located in Flood Zone 2, which is an area assessed to be at medium probability of flooding from the River Crane. The residual risk of flooding to the site can be effectively managed by setting the proposed buildings ground floor levels above the predicted flood level of 6.34mAOD for the 0.1% AEP.
- 9.2 National and Local Policy aims to avoid inappropriate development in areas at risk of flooding and recommends that development is directed towards areas at lowest flood risk. The NPPF and Local Policy of the London Borough of Richmond upon Thames advises that residential developments are a more vulnerable use and appropriate in Flood Zone 2 provided they pass the sequential test with it not being necessary to apply the exception test.
- 9.3 Raising the proposed buildings floor level would largely address the risk of flooding from other sources. However, National and Local Policy requires development to seek opportunities to reduce the overall level of flood risk in the area and beyond through the use of Sustainable Drainage Systems (SuDS). A hierarchical assessment has established that an existing surface water sewer in the roads adjacent the site would be the most appropriate destination for the disposal of surface water runoff from the development provided that surface water flows are limited to a maximum allowable discharge rate of 1.7 l/s using SuDS.
- 9.4 A further hierarchical assessment has established that water butts and pervious pavement system would be the most appropriate SuDS components for minimising the rate of discharge, volume and environmental impact of surface water runoff from

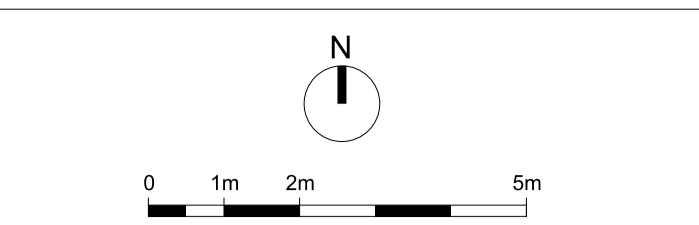
the development. A surface water drainage strategy has been developed for the site comprising of these components, which would ensure that surface water flows are controlled as close to the source as possible, prior to discharging to the surface water sewer, with flows restricted to a maximum allowable discharge rate of 1.7 l/s for all analysed rainfall events up to and including the 1 in 100 year return period with 40% allowance for climate change. The systems would also provide sufficient capacity for excess runoff to be stored and attenuated on site for all rainfall events up to and including the 1 in 100-year storm return period with 40% allowance for climate change.

- 9.5 In terms of flood risk, it is concluded that the development can be occupied and operated safely and that there will be no increase in the level of flood risk to the site or neighbouring sites because of the development.

| | | | | | | |
|---------|----------|-----------|--------|-------------|----------|---------|
| JOB NO: | P20-435A | ISSUE NO: | 1 | ISSUE DATE: | 11/03/22 | Page 22 |
| AUTHOR: | GSC | OFFICE: | HENLEY | CHECKED BY: | GSC | |

**APPENDIX A
TOPOGRAPHICAL SURVEY**

**APPENDIX B
PLANNING DRAWINGS**



| Revision | Date | Description |
|----------|------|-------------|
| | | |

© copyright Wimshurst Pelleriti, all rights reserved 2022

Do not scale-off this drawing, Wimshurst Pelleriti take no responsibility for any dimensions obtained by measuring or scaling from this drawing and no reliance may be placed on such dimensions. If no dimension is given, it is the responsibility of the recipient to ascertain the dimension specifically from the Architect or by site measurement.

The sizing of all structural and service elements must always be checked against the relevant engineers drawings. No reliance should be placed upon sizing information shown on this drawing.

Project
St Margarets Business Centre
 Richmond, London

Drawing Title
 GA Plan
 Proposed Level GF
 External Layout Option 1

| Drawing Number | Revision |
|---------------------|----------|
| WP-0780-A-0100-P-00 | |

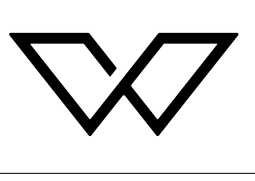
| Scale @ A1 | Revision Date |
|------------|---------------|
| 1:100 | |

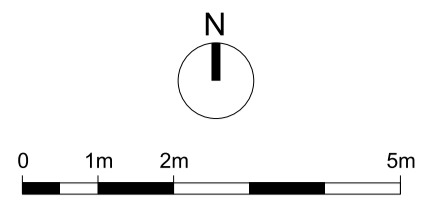
Drawing Purpose
 DRAFT FOR DISCUSSION

WIMSHURST PELLERITI

The Mews,
 6 Putney Common, SW15 1HL

0208 780 2206
 info@wp.uk.com
 wimshurst-pelleriti.com





| Revision | Date | Description |
|----------|------|-------------|
| | | |

© copyright Wimshurst Pelleriti, all rights reserved 2022

Do not scale-off this drawing, Wimshurst Pelleriti take no responsibility for any dimensions obtained by measuring or scaling from this drawing and no reliance may be placed on such dimensions. If no dimension is given, it is the responsibility of the recipient to ascertain the dimension specifically from the Architect or by site measurement.

The sizing of all structural and service elements must always be checked against the relevant engineers drawings. No reliance should be placed upon sizing information shown on this drawing.

Project
St Margarets Business Centre
 Richmond, London

Drawing Title
 GA Plan
 Proposed Level First Floor

| Drawing Number | Revision |
|---------------------|----------|
| WP-0780-A-0101-P-01 | |


| Scale @ A1 | Revision Date |
|------------|---------------|
| 1:100 | |

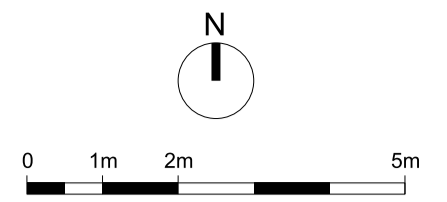
Drawing Purpose
 DRAFT FOR DISCUSSION

WIMSHURST PELLERITI

The Mews,
 6 Putney Common, SW15 1HL

0208 780 2206
 info@wp.uk.com
 wimshurst-pelleriti.com





| Revision | Date | Description |
|----------|------|-------------|
| | | |

© copyright Wimshurst Pelleriti, all rights reserved 2022

Do not scale-off this drawing. Wimshurst Pelleriti take no responsibility for any dimensions obtained by measuring or scaling from this drawing and no reliance may be placed on such dimensions. If no dimension is given, it is the responsibility of the recipient to ascertain the dimension specifically from the Architect or by site measurement.

The sizing of all structural and service elements must always be checked against the relevant engineers drawings. No reliance should be placed upon sizing information shown on this drawing.

Project
St Margarets Business Centre
 Richmond, London

Drawing Title
 GA Plan
 Proposed Level Second Floor

| Drawing Number | Revision |
|---------------------|----------|
| WP-0780-A-0102-P-02 | |


| Scale @ A1 | Revision Date |
|------------|---------------|
| 1:100 | |

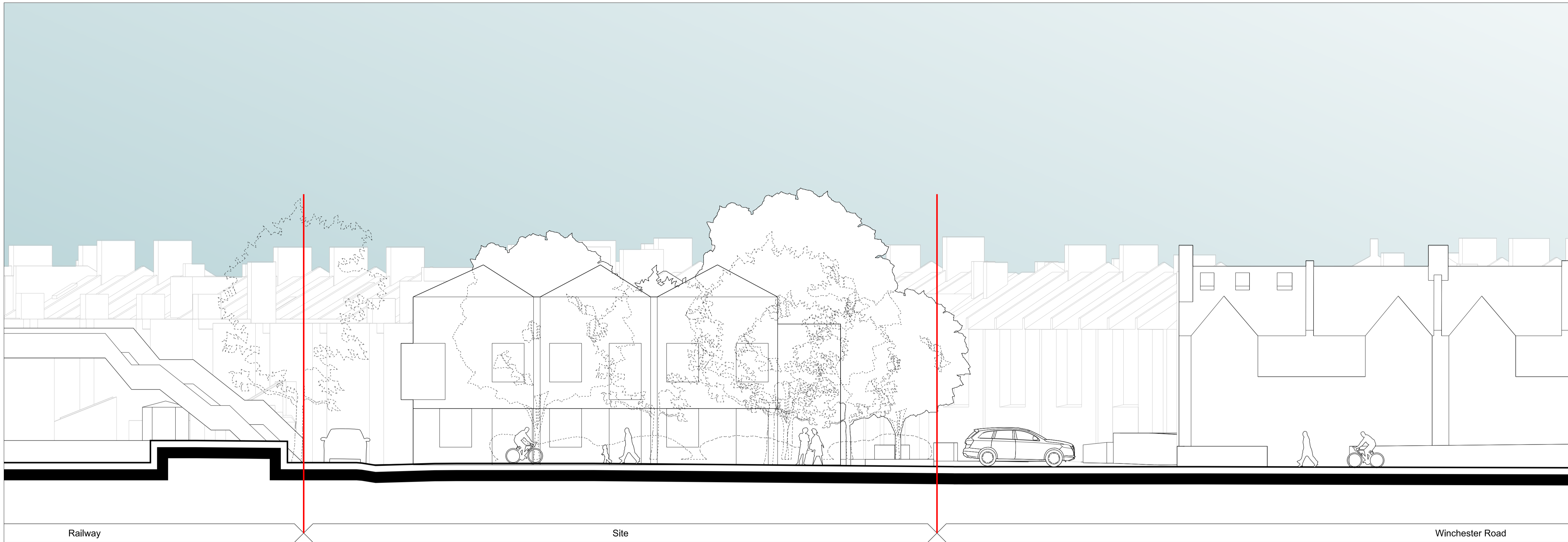
Drawing Purpose
 DRAFT FOR DISCUSSION

WIMSHURST PELLERITI

The Mews,
 6 Putney Common, SW15 1HL

0208 780 2206
 info@wp.uk.com
 wimshurst-pelleriti.com





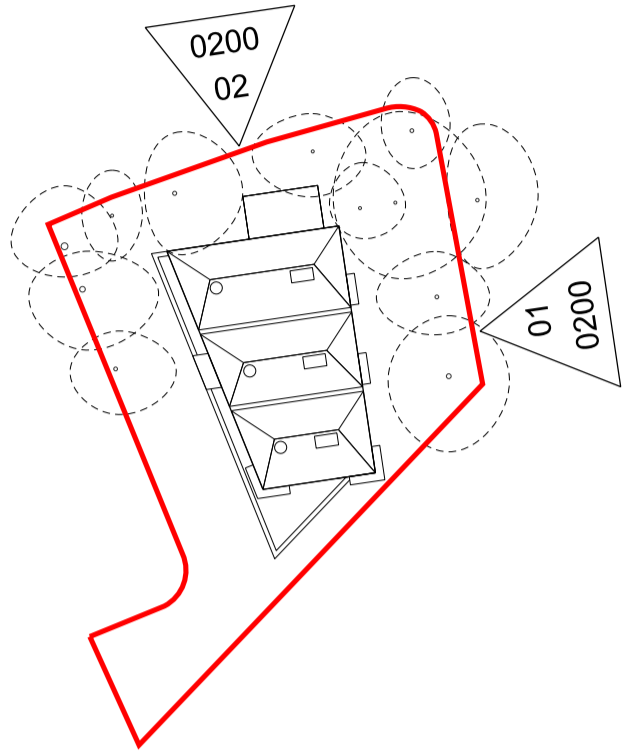
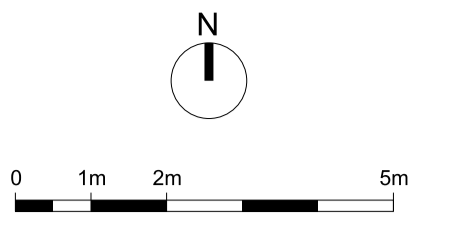
01
0200

East Elevation



02
0200

North Elevation



| Revision | Date | Description |
|----------|------|-------------|
| | | |

© copyright Wimshurst Pelleriti, all rights reserved 2022

Do not scale-off this drawing, Wimshurst Pelleriti take no responsibility for any dimensions obtained by measuring or scaling from this drawing and no reliance may be placed on such dimensions. If no dimension is given, it is the responsibility of the recipient to ascertain the dimension specifically from the Architect or by site measurement.

The sizing of all structural and service elements must always be checked against the relevant engineers drawings. No reliance should be placed upon sizing information shown on this drawing.

Project
St Margarets Business Centre
 Richmond, London

Drawing Title
Proposed Elevations East & North

Drawing Number **Revision**
 WP-0780-A-0200-E-XX

Scale @ A1 **Revision Date**
 1:100

Drawing Purpose
DRAFT FOR DISCUSSION

WIMSHURST PELLERITI

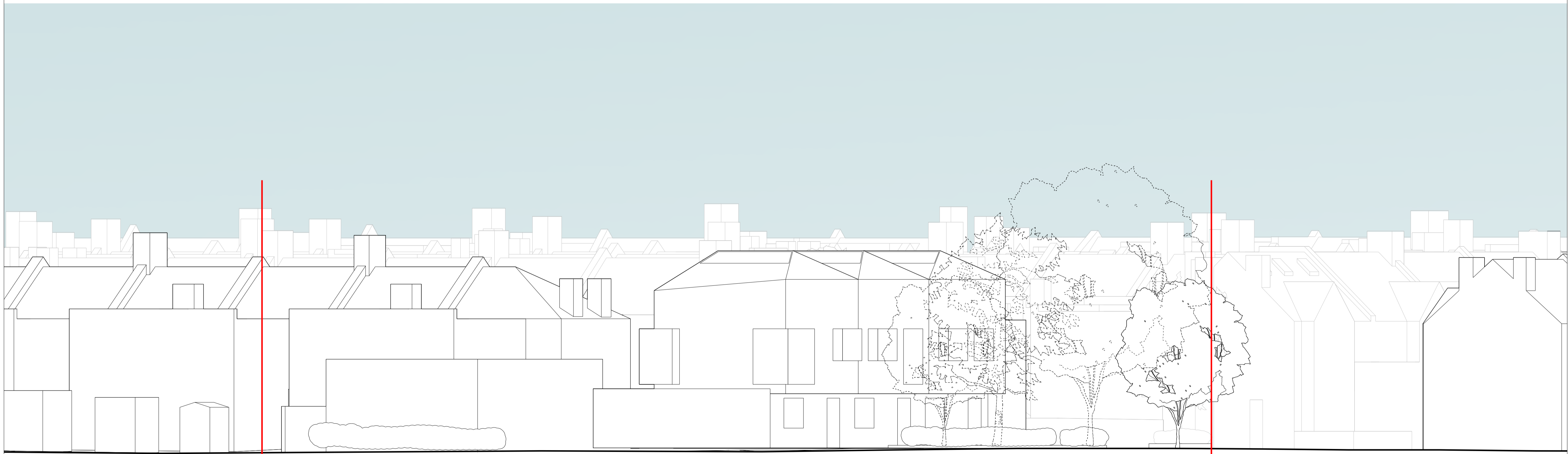
The Mews,
 6 Putney Common, SW15 1HL
 0208 780 2206
 info@wp.uk.com
 wimshurst-pelleriti.com





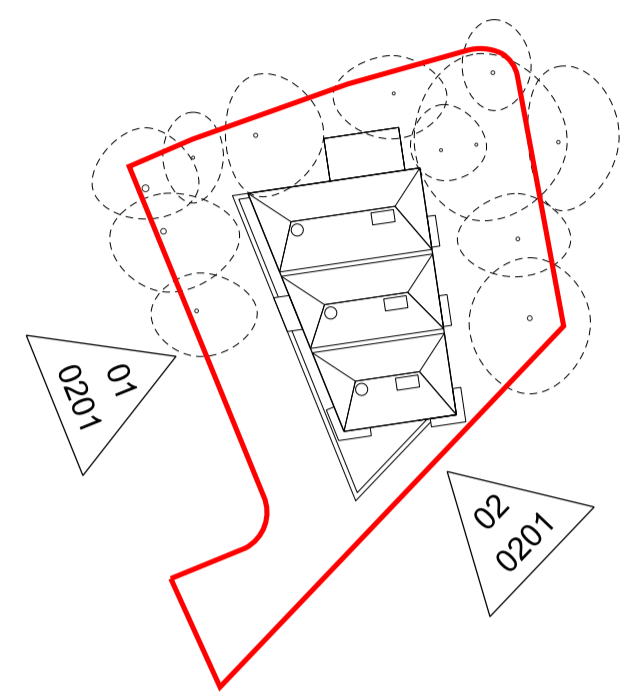
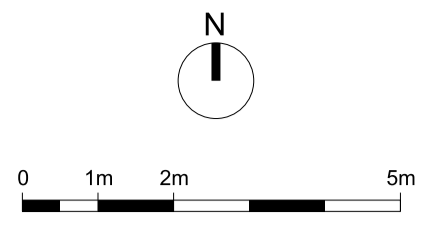
West Elevation

01
0201



South Elevation

02
0201



| Revision | Date | Description |
|----------|------|-------------|
| | | |

© copyright Wimshurst Pelleriti, all rights reserved 2022

Do not scale-off this drawing, Wimshurst Pelleriti take no responsibility for any dimensions obtained by measuring or scaling from this drawing and no reliance may be placed on such dimensions. If no dimension is given, it is the responsibility of the recipient to ascertain the dimension specifically from the Architect or by site measurement.

The sizing of all structural and service elements must always be checked against the relevant engineers drawings. No reliance should be placed upon sizing information shown on this drawing.

Project
St Margaret's Business Centre
Richmond, London

Drawing Title
Proposed Elevations
West & South

Drawing Number WP-0780-A-0201-E-XX **Revision**

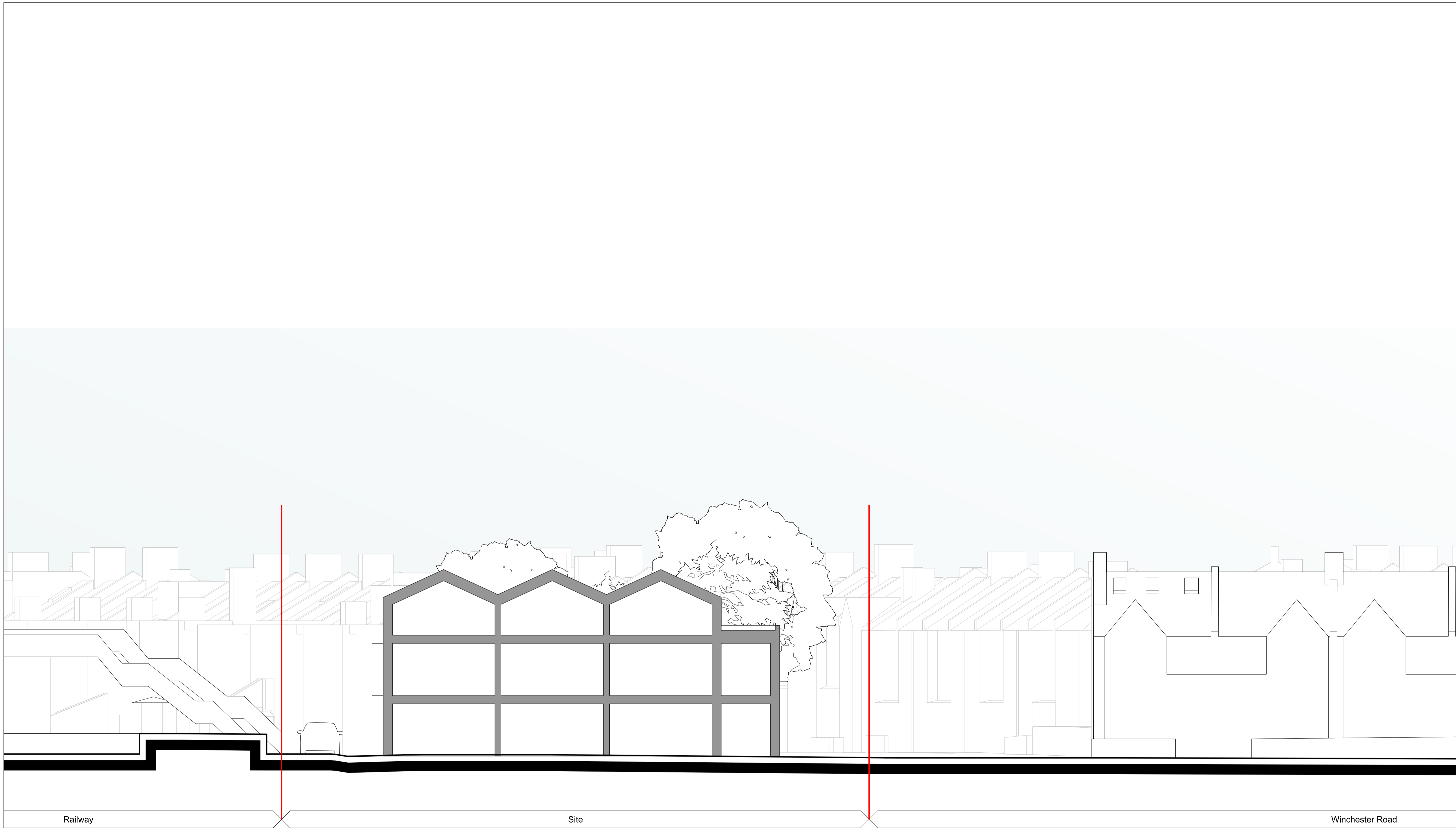
Scale @ A1 1:100 **Revision Date**

Drawing Purpose
DRAFT FOR DISCUSSION

WIMSHURST PELLERITI

The Mews,
6 Putney Common, SW15 1HL
0208 780 2206
info@wp.uk.com
wimshurst-pelleriti.com

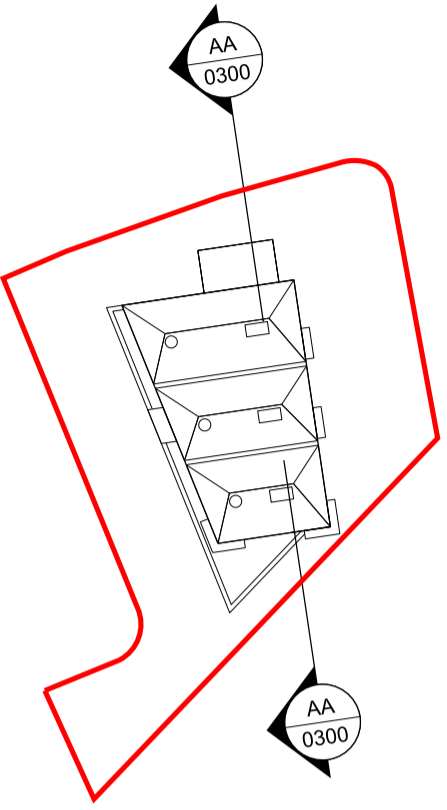
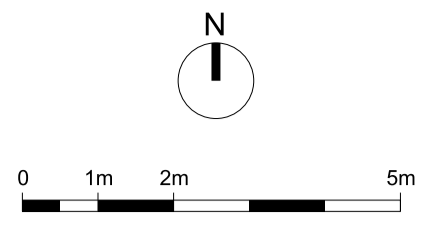




AA
0300

Section AA

Railway Site Winchester Road



| Revision | Date | Description |
|----------|------|-------------|
| | | |

© copyright Wimshurst Pelleriti, all rights reserved 2022

Do not scale-off this drawing, Wimshurst Pelleriti take no responsibility for any dimensions obtained by measuring or scaling from this drawing and no reliance may be placed on such dimensions. If no dimension is given, it is the responsibility of the recipient to ascertain the dimension specifically from the Architect or by site measurement.

The sizing of all structural and service elements must always be checked against the relevant engineers drawings. No reliance should be placed upon sizing information shown on this drawing.

Project
St Margarets Business Centre
Richmond, London

Drawing Title
Proposed Sections
AA

| | |
|-----------------------|-----------------|
| Drawing Number | Revision |
| WP-0780-A-0300-S-XX | |


| | |
|-------------------|----------------------|
| Scale @ A1 | Revision Date |
| 1:100 | |

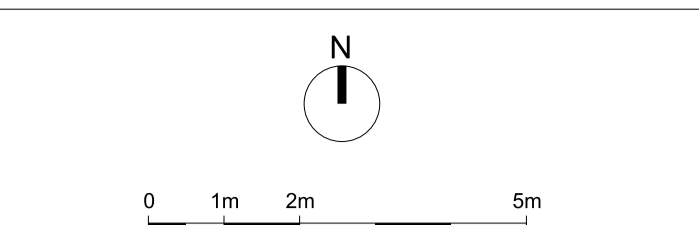
Drawing Purpose
DRAFT FOR DISCUSSION

WIMSHURST PELLERITI

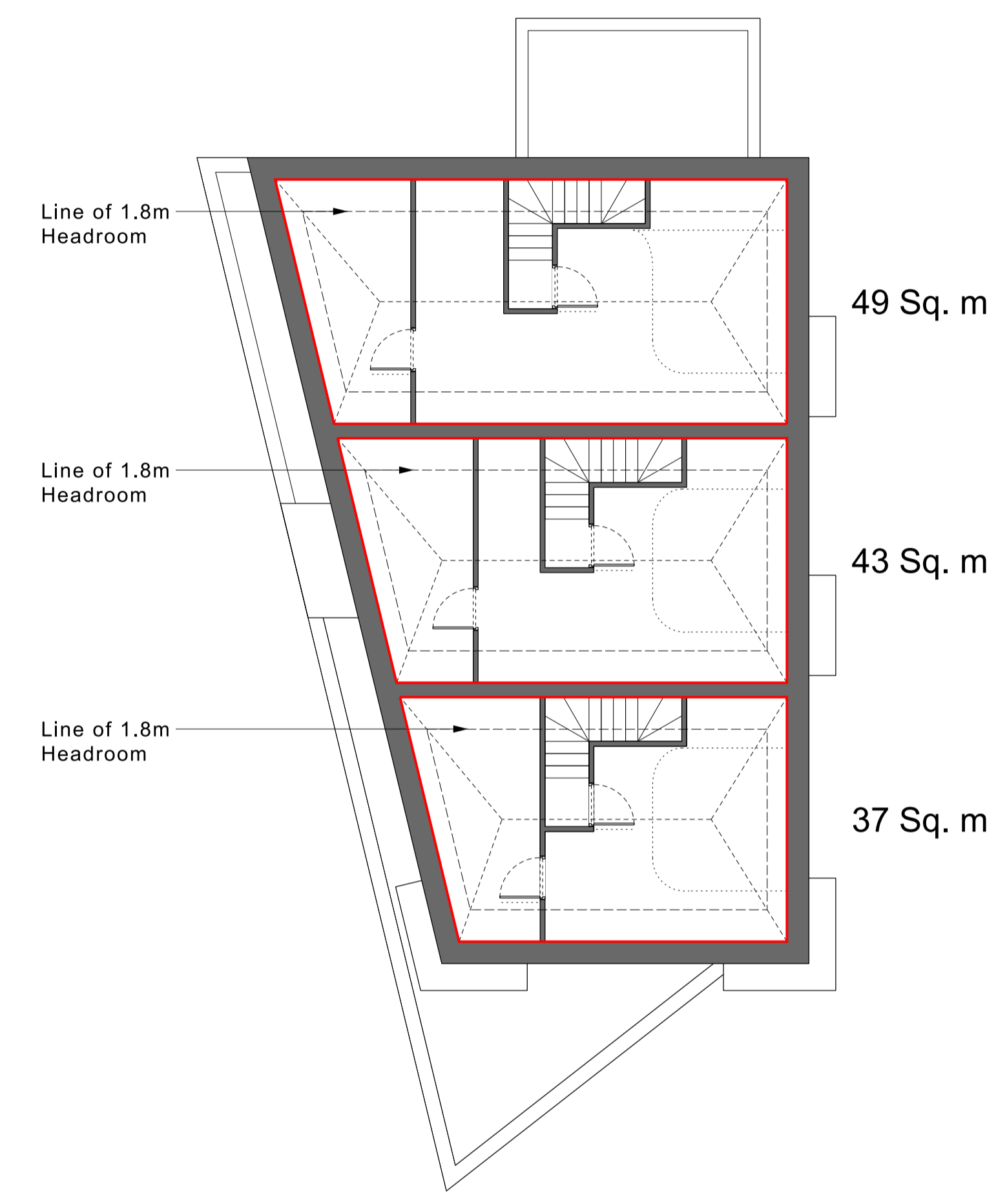
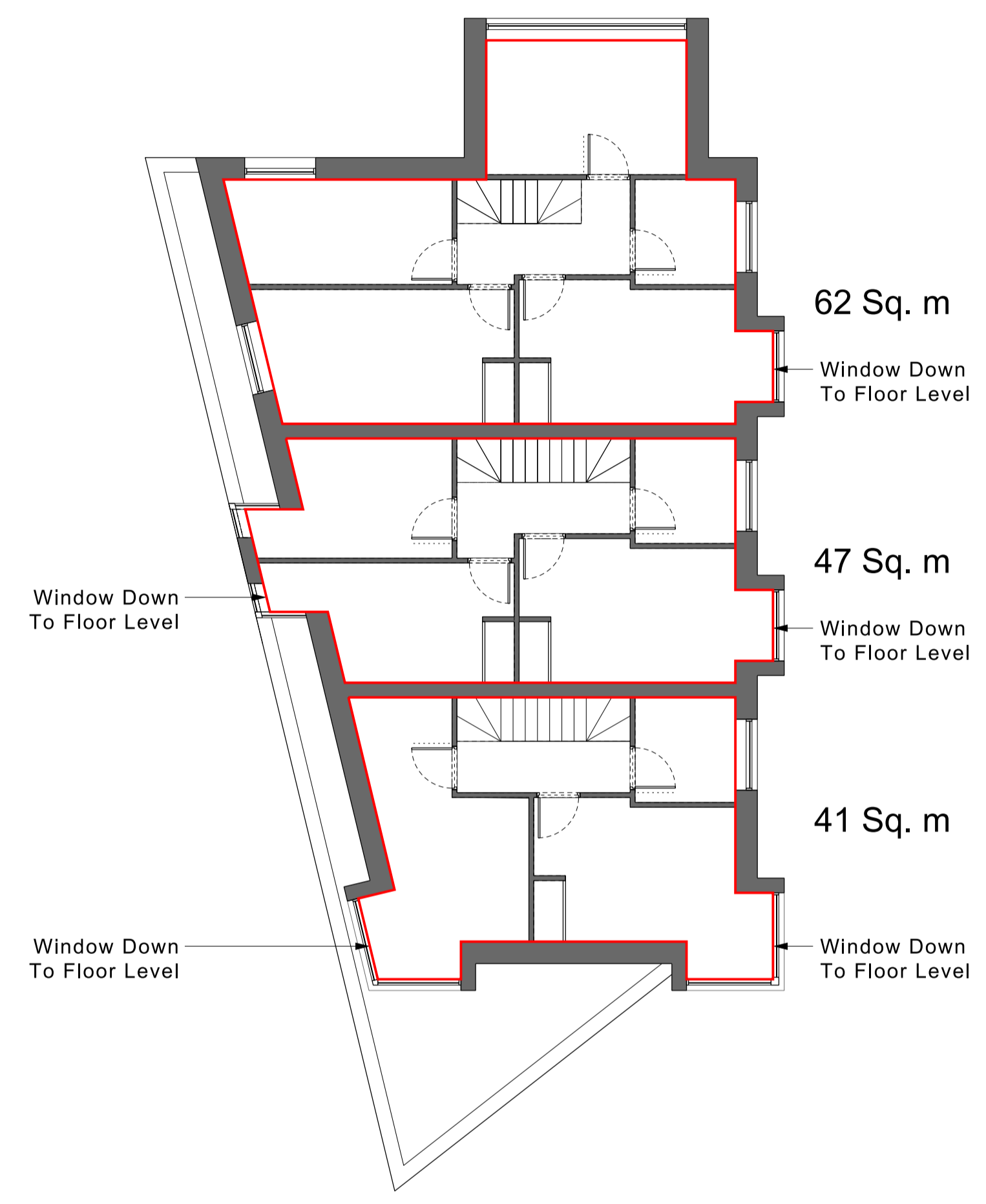
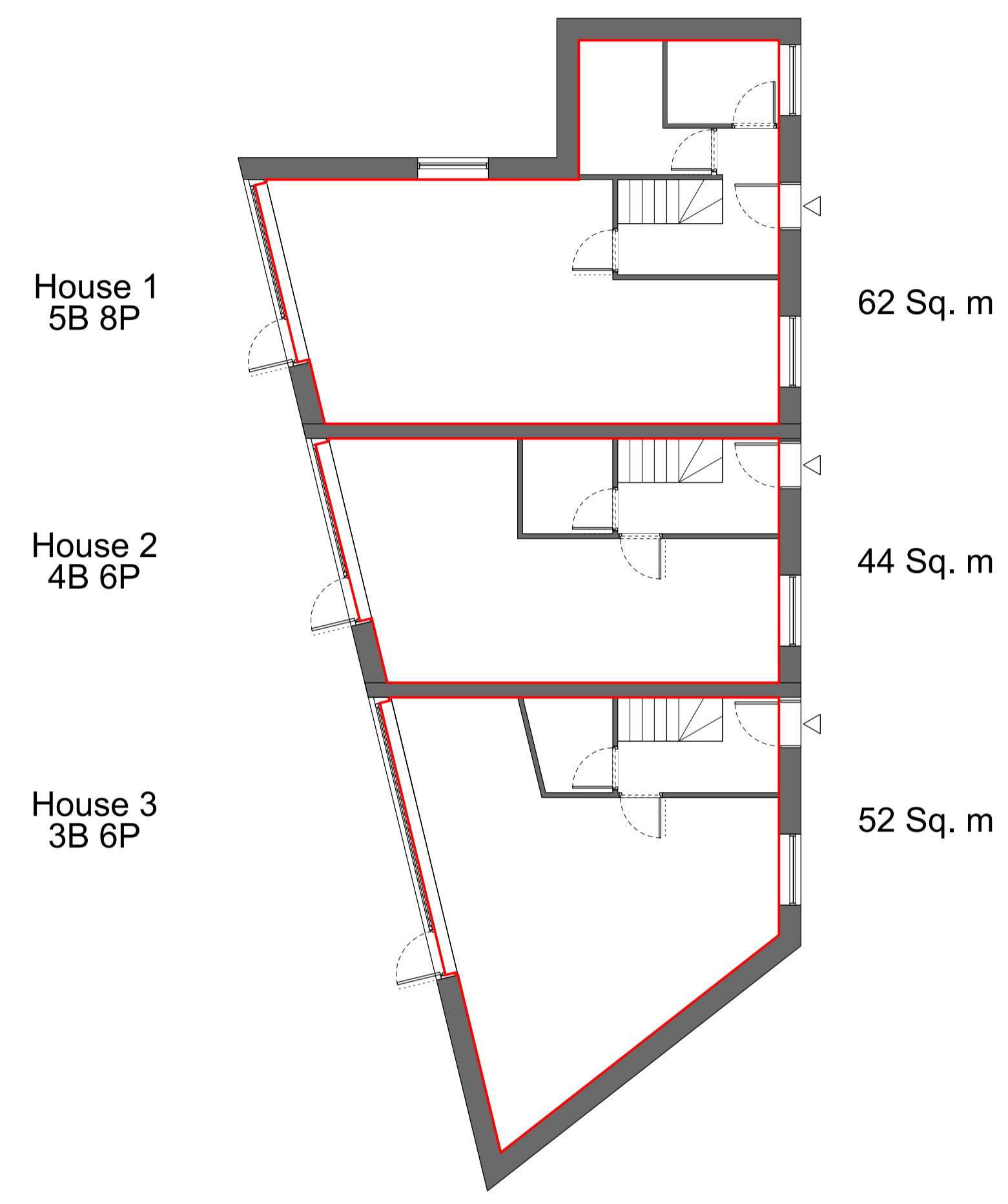
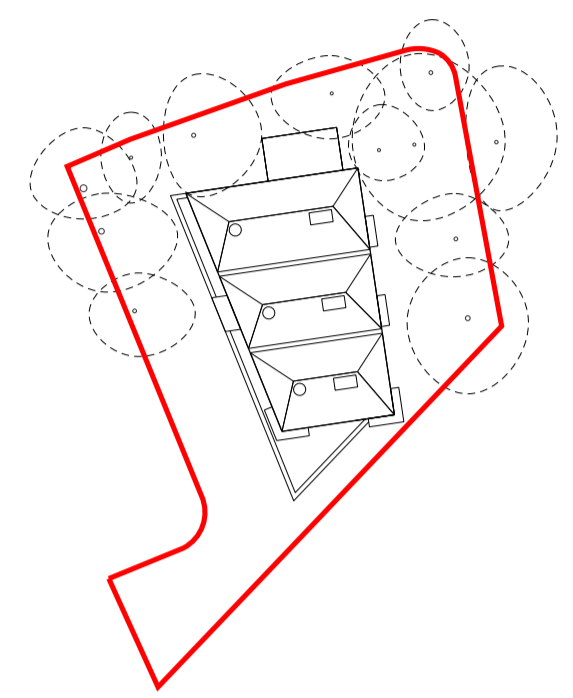
The Mews,
6 Putney Common, SW15 1HL

0208 780 2206
info@wp.uk.com
wimshurst-pelleriti.com





AREA CALCULATIONS
 These areas have been measured from plans produced at stage 2 pre-planning and are approximate and illustrative only. Further development of the design, measurement and construction tolerances and/or further client/tenant requests will inevitably result in changes to these areas (which could involve significant reductions) and WP accept no legal responsibility for any decision, commercial or otherwise, made on the basis of these areas.



01
0400 Ground Floor Areas

02
0400 First Floor Areas

03
0400 Second Floor Areas

| Areas in Sqm | House 1 5B 8P | House 2 4B 6P | House 3 3B 6P |
|-------------------------------|---------------|---------------|---------------|
| Ground | 62 | 44 | 52 |
| 1st | 62 | 47 | 41 |
| 2nd | 49 | 43 | 37 |
| Total | 173 | 134 | 130 |
| Minimum Required To Meet NDSS | 134 | 112 | 108 |

| Revision | Date | Description |
|----------|------|-------------|
| | | |

© copyright Wimshurst Pelleriti, all rights reserved 2022
 Do not scale-off this drawing. Wimshurst Pelleriti take no responsibility for any dimensions obtained by measuring or scaling from this drawing and no reliance may be placed on such dimensions. If no dimension is given, it is the responsibility of the recipient to ascertain the dimension specifically from the Architect or by site measurement.
 The sizing of all structural and service elements must always be checked against the relevant engineers drawings. No reliance should be placed upon sizing information shown on this drawing.

Project
St Margarets Business Centre
 Richmond, London

Drawing Title
 Area Schedule

| Drawing Number | Revision |
|---------------------|----------|
| WP-0780-A-0400-P-XX | |

| Scale @ A1 | Revision Date |
|------------|---------------|
| 1:100 | |

Drawing Purpose
 DRAFT FOR DISCUSSION

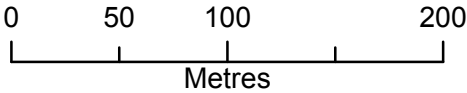
WIMSHURST PELLERITI
 The Mews,
 6 Putney Common, SW15 1HL
 0208 780 2206
 info@wp.uk.com
 wimshurst-pelleriti.com

**APPENDIX C
EA FLOOD RISK DATA**

Detailed FRA centred on: St Margarets Business Park Car Park, Twickenham, TW1 1JS - 03/03/2022 - HNL 253000 NR



Environment Agency
 Alchemy,
 Bessemer Road,
 Welwyn Garden City,
 Hertfordshire,
 AL7 1HE



Legend

- Main Rivers
- Site location

Defended Flood Outlines

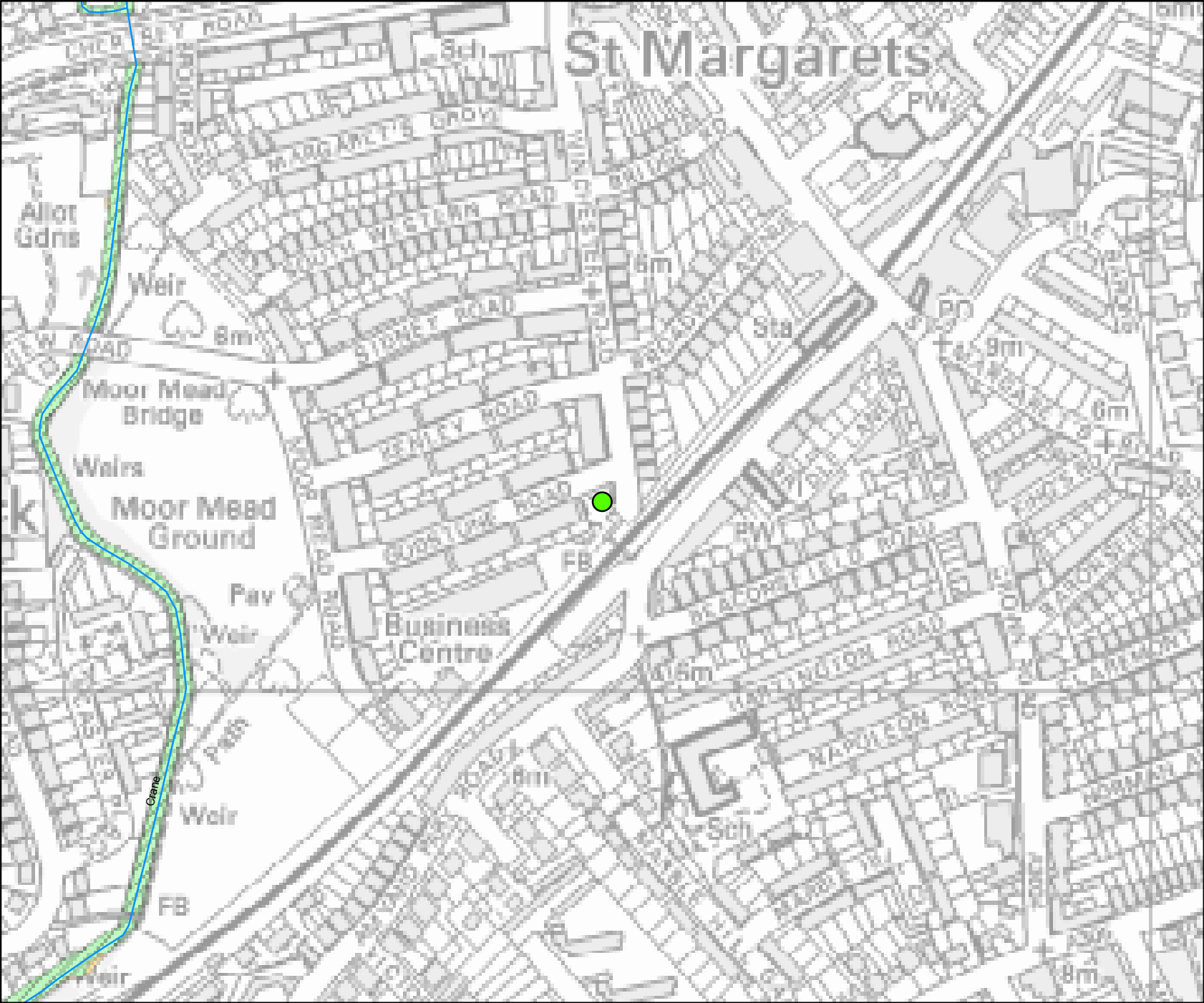
- 1 in 5 (20%) Defended
- 1 in 10 (10%) Defended
- 1 in 20 (5%) Defended
- 1 in 50 (2%) Defended

The data in this map has been extracted from the River Crane Mapping Study (Halcrow 2008). This model has been designed for catchment wide flood risk mapping. It should be noted that it was not created to produce flood levels for specific development sites within the catchment.

Modelled outlines take into account catchment wide defences.

Flood risk data requests including an allowance for climate change will be based on the 1 in 100 flood plus 20% allowance for climate change, unless otherwise stated. You should refer to 'Flood risk assessments: climate change allowances' to check if this allowance is still appropriate for the type of development you are proposing and its location. You may need to undertake further assessment of future flood risk using different allowances to ensure your assessment of future flood risk is based on best available evidence. <https://www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances>

Produced by:
 Partnerships & Strategic Overview,
 Hertfordshire & North London

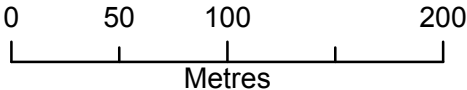


This map is based upon Ordnance Survey Material with the permission of Ordnance Survey on behalf of the controller of Her Majesty's Stationery Office Crown Copyright. Unauthorised reproduction infringes Crown Copyright and may lead to prosecution or civil proceedings. Environment Agency 100024198, 2022

Detailed FRA centred on: St Margarets Business Park Car Park, Twickenham, TW1 1JS - 03/03/2022 - HNL 253000 NR



Environment Agency
 Alchemy,
 Bessemer Road,
 Welwyn Garden City,
 Hertfordshire,
 AL7 1HE



Legend

- Main Rivers
- Site location

Defended Flood Outlines

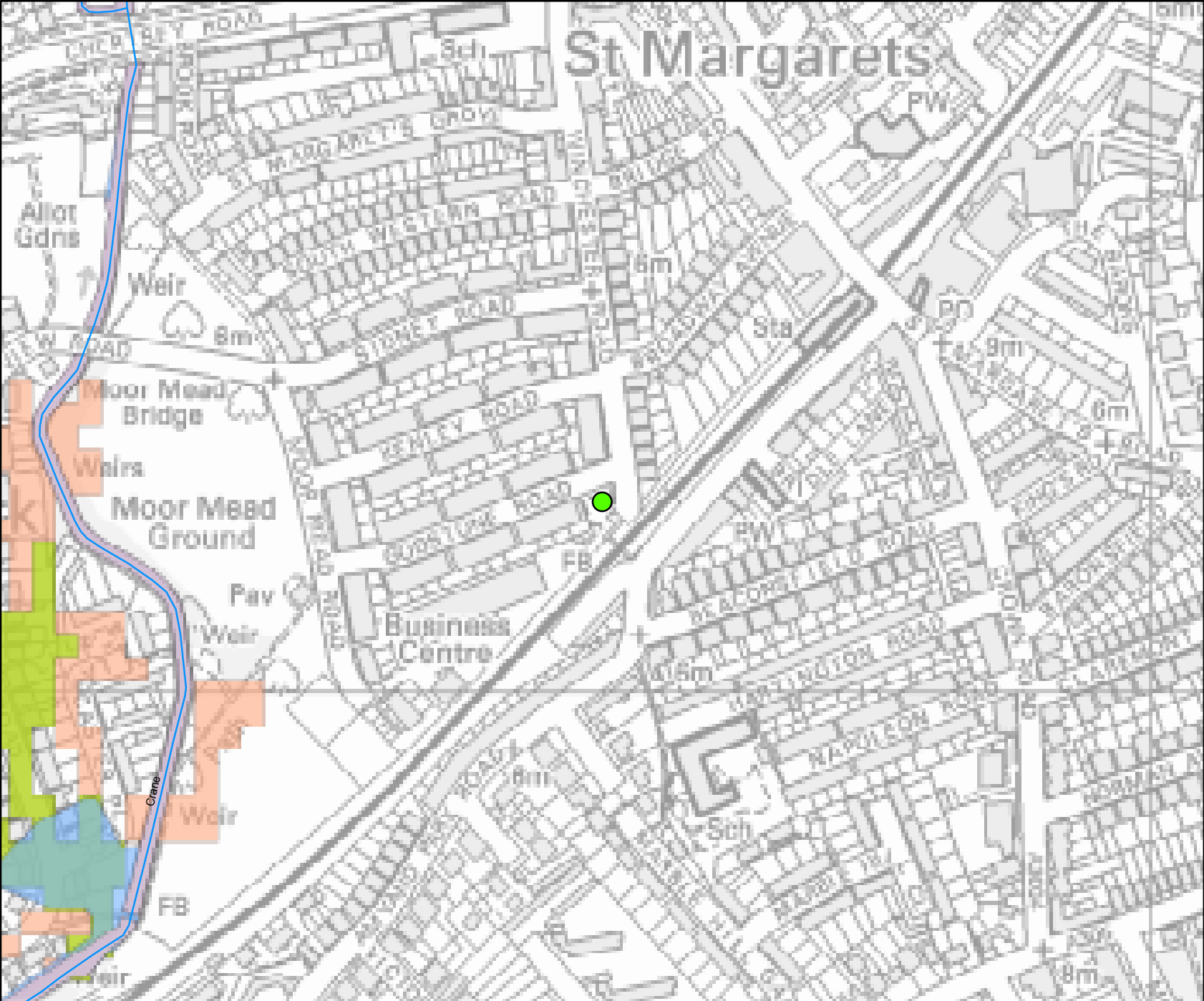
- 1 in 100 (1%) Defended
- 1 in 100+20% (*CC) Defended
- 1 in 100+25% (*CC) Defended
- 1 in 100+30% (*CC) Defended

The data in this map has been extracted from the River Crane Mapping Study (Halcrow 2008). This model has been designed for catchment wide flood risk mapping. It should be noted that it was not created to produce flood levels for specific development sites within the catchment.

Modelled outlines take into account catchment wide defences.

Flood risk data requests including an allowance for climate change will be based on the 1 in 100 flood plus 20% allowance for climate change, unless otherwise stated. You should refer to 'Flood risk assessments: climate change allowances' to check if this allowance is still appropriate for the type of development you are proposing and its location. You may need to undertake further assessment of future flood risk using different allowances to ensure your assessment of future flood risk is based on best available evidence. <https://www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances>

Produced by:
 Partnerships & Strategic Overview,
 Hertfordshire & North London

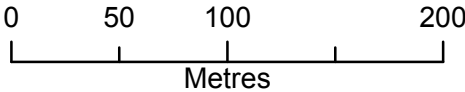


This map is based upon Ordnance Survey Material with the permission of Ordnance Survey on behalf of the controller of Her Majesty's Stationery Office Crown Copyright. Unauthorised reproduction infringes Crown Copyright and may lead to prosecution or civil proceedings. Environment Agency 100024198, 2022

Detailed FRA centred on: St Margarets Business Park Car Park, Twickenham, TW1 1JS - 03/03/2022 - HNL 253000 NR



Environment Agency
 Alchemy,
 Bessemer Road,
 Welwyn Garden City,
 Hertfordshire,
 AL7 1HE



Legend

- Main Rivers
- Site location

Defended Flood Outlines

- 1 in 100+70% (*CC) Defended
- 1 in 1000 (0.1%) Defended

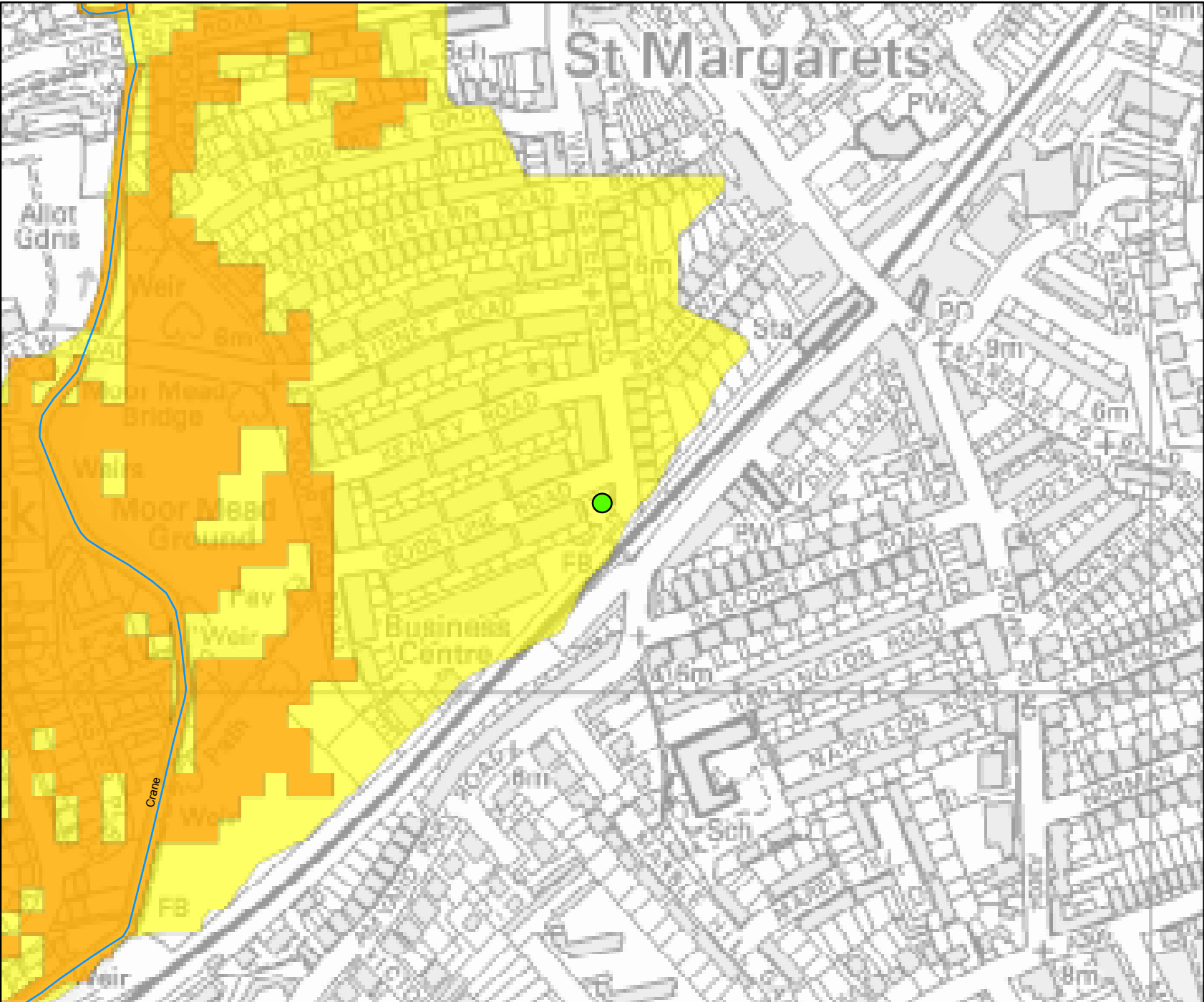
The data in this map has been extracted from the River Crane Mapping Study (Halcrow 2008). This model has been designed for catchment wide flood risk mapping. It should be noted that it was not created to produce flood levels for specific development sites within the catchment.

Modelled outlines take into account catchment wide defences.

Flood risk data requests including an allowance for climate change will be based on the 1 in 100 flood plus 20% allowance for climate change, unless otherwise stated. You should refer to 'Flood risk assessments: climate change allowances' to check if this allowance is still appropriate for the type of development you are proposing and its location. You may need to undertake further assessment of future flood risk using different allowances to ensure your assessment of future flood risk is based on best available evidence.

<https://www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances>

Produced by:
 Partnerships & Strategic Overview,
 Hertfordshire & North London

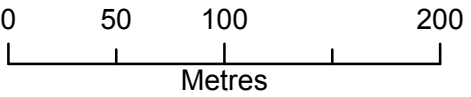


This map is based upon Ordnance Survey Material with the permission of Ordnance Survey on behalf of the controller of Her Majesty's Stationery Office Crown Copyright. Unauthorised reproduction infringes Crown Copyright and may lead to prosecution or civil proceedings. Environment Agency 100024198, 2022

Detailed FRA centred on: St Margarets Business Park Car Park, Twickenham, TW1 1JS - 03/03/2022 - HNL 253000 NR



Environment Agency
 Alchemy,
 Bessemer Road,
 Welwyn Garden City,
 Hertfordshire,
 AL7 1HE



Legend

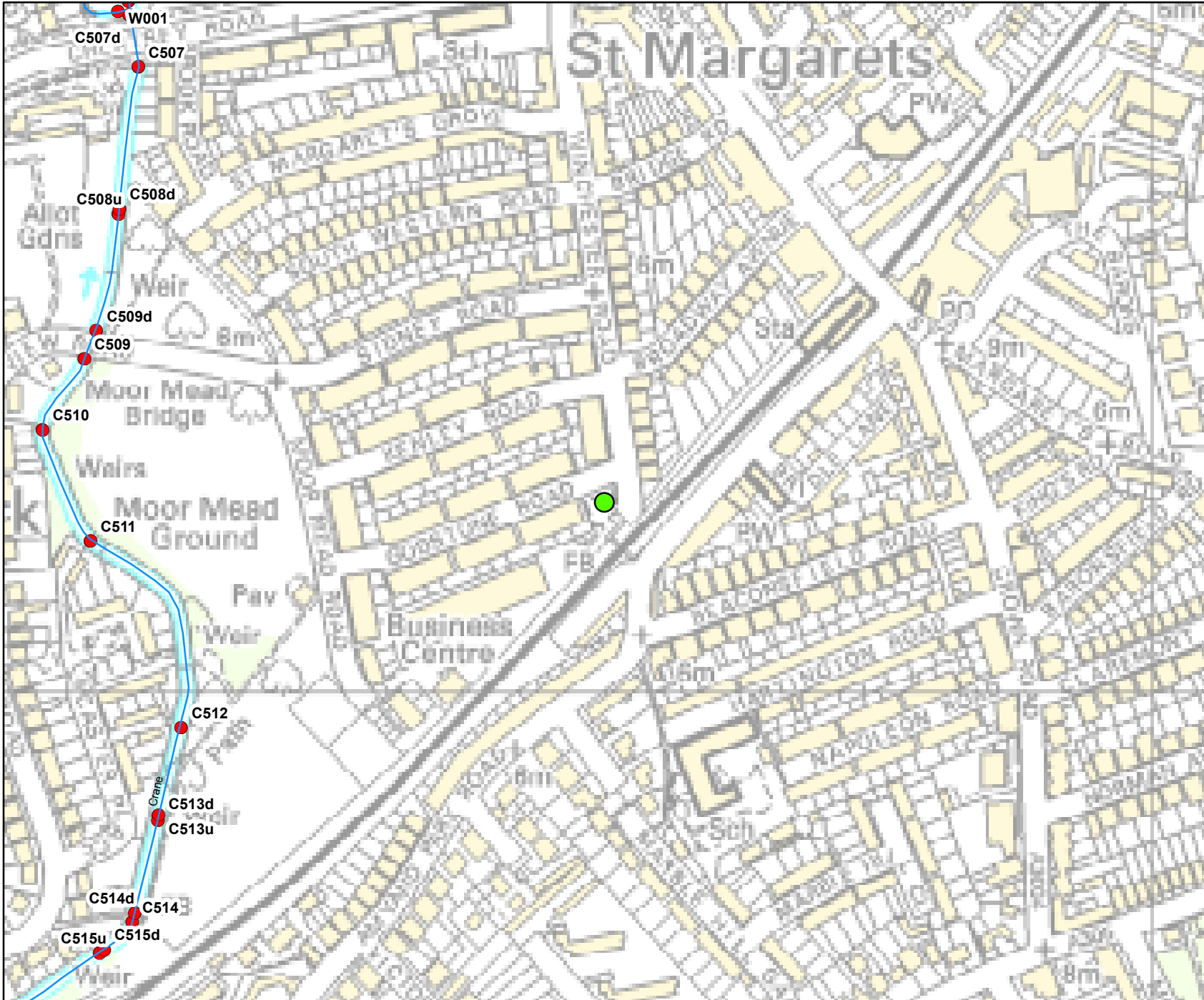
- Main Rivers
- Site location
- 1D Node Results**
- Node Results

The data in this map has been extracted from the River Crane Mapping Study (Halcrow 2008). This model has been designed for catchment wide flood risk mapping. It should be noted that it was not created to produce flood levels for specific development sites within the catchment. Modelled outlines take into account catchment wide defences.

Flood risk data requests including an allowance for climate change will be based on the 1 in 100 flood plus 20% allowance for climate change, unless otherwise stated. You should refer to 'Flood risk assessments: climate change allowances' to check if this allowance is still appropriate for the type of development you are proposing and its location. You may need to undertake further assessment of future flood risk using different allowances to ensure your assessment of future flood risk is based on best available evidence.

<https://www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances>

Produced by:
 Partnerships & Strategic Overview,
 Hertfordshire & North London



This map is based upon Ordnance Survey Material with the permission of Ordnance Survey on behalf of the controller of Her Majesty's Stationery Office Crown Copyright. Unauthorised reproduction infringes Crown Copyright and may lead to prosecution or civil proceedings. Environment Agency 100024198, 2022

Environment Agency ref: HNL 253000 NR

The following information has been extracted from the River Crane Mapping Study (Halcrow 2008)

Flood risk data requests including an allowance for climate change will be based on the 1 in 100 flood plus 20% allowance for climate change, unless otherwise stated. You should refer to 'Flood risk assessments: climate change allowances' to check if this allowance is still appropriate for the type of development you are proposing and its location. You may need to undertake further assessment of future flood risk using different allowances to ensure your assessment of future flood risk is based on best available evidence.

<https://www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances>

Caution:

The modelled flood levels and extents are appropriate for catchment wide strategic flood risk mapping. However, for more detailed flood risk assessment it is recommended that each of the underlying flood mapping, hydraulic modelling and hydrological assumptions are re-evaluated to determine the appropriateness in a more detailed analysis.

All flood levels are given in metres Above Ordnance Datum (mAOD)
All flows are given in cubic metres per second (cumecs)

MODELLED FLOOD LEVEL

| Node Label | Easting | Northing | Return Period | | | | | | | | | |
|------------|---------|----------|---------------|-------|-------|-------|--------|-------------|-------------|-------------|-------------|--------|
| | | | 5 yr | 10 yr | 20 yr | 50 yr | 100 yr | 100yr + 20% | 100yr + 25% | 100yr + 35% | 100yr + 70% | 1000yr |
| C515u | 516321 | 173829 | 6.78 | 6.84 | 6.87 | 6.90 | 6.92 | 6.96 | 6.98 | 7.09 | 7.11 | 7.15 |
| C515d | 516321 | 173829 | 6.70 | 6.76 | 6.78 | 6.81 | 6.84 | 6.88 | 6.89 | 7.01 | 7.03 | 7.06 |
| C514 | 516339 | 173852 | 6.65 | 6.70 | 6.73 | 6.76 | 6.78 | 6.82 | 6.84 | 6.95 | 6.97 | 7.00 |
| C514d | 516339 | 173852 | 6.65 | 6.71 | 6.74 | 6.77 | 6.80 | 6.85 | 6.86 | 6.98 | 7.00 | 7.04 |
| C513u | 516352 | 173919 | 6.57 | 6.63 | 6.65 | 6.68 | 6.70 | 6.74 | 6.76 | 6.86 | 6.87 | 6.90 |
| C513d | 516352 | 173919 | 6.47 | 6.52 | 6.54 | 6.57 | 6.59 | 6.63 | 6.65 | 6.74 | 6.76 | 6.77 |
| C512 | 516370 | 173977 | 6.41 | 6.46 | 6.48 | 6.51 | 6.53 | 6.57 | 6.58 | 6.68 | 6.70 | 6.71 |
| C511 | 516311 | 174096 | 6.28 | 6.32 | 6.35 | 6.38 | 6.40 | 6.44 | 6.45 | 6.54 | 6.57 | 6.59 |
| C510 | 516281 | 174173 | 6.23 | 6.28 | 6.31 | 6.34 | 6.36 | 6.40 | 6.41 | 6.51 | 6.54 | 6.60 |
| C509 | 516314 | 174220 | 6.21 | 6.26 | 6.29 | 6.31 | 6.34 | 6.37 | 6.39 | 6.48 | 6.50 | 6.54 |
| C509d | 516314 | 174220 | 6.21 | 6.25 | 6.27 | 6.30 | 6.31 | 6.35 | 6.36 | 6.43 | 6.44 | 6.47 |
| C508u | 516332 | 174310 | 6.11 | 6.15 | 6.17 | 6.19 | 6.21 | 6.24 | 6.25 | 6.32 | 6.33 | 6.36 |
| C508d | 516332 | 174310 | 5.41 | 5.45 | 5.46 | 5.48 | 5.50 | 5.52 | 5.53 | 5.59 | 5.61 | 5.70 |
| C507 | 516338 | 174406 | 5.30 | 5.33 | 5.35 | 5.37 | 5.38 | 5.41 | 5.42 | 5.48 | 5.50 | 5.63 |
| C507d | 516338 | 174406 | 5.22 | 5.25 | 5.27 | 5.29 | 5.30 | 5.32 | 5.33 | 5.40 | 5.42 | 5.58 |
| W001 | 516330 | 174440 | 5.20 | 5.24 | 5.25 | 5.27 | 5.28 | 5.31 | 5.32 | 5.38 | 5.40 | 5.57 |

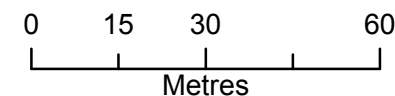
MODELLED FLOWS

| Node Label | Easting | Northing | Return Period | | | | | | | | | |
|------------|---------|----------|---------------|-------|-------|-------|--------|-------------|-------------|-------------|-------------|--------|
| | | | 5 yr | 10 yr | 20 yr | 50 yr | 100 yr | 100yr + 20% | 100yr + 25% | 100yr + 35% | 100yr + 70% | 1000yr |
| C515u | 516321 | 173829 | 24.16 | 25.42 | 26.05 | 26.69 | 27.29 | 28.17 | 28.51 | 30.97 | 31.56 | 32.85 |
| C515d | 516321 | 173829 | 24.16 | 25.42 | 26.05 | 26.69 | 27.29 | 28.17 | 28.51 | 30.97 | 31.56 | 32.85 |
| C514 | 516339 | 173852 | 24.16 | 25.42 | 26.05 | 26.69 | 27.29 | 28.17 | 28.51 | 30.97 | 31.56 | 32.93 |
| C514d | 516339 | 173852 | 24.16 | 25.42 | 26.05 | 26.69 | 27.29 | 28.17 | 28.51 | 30.97 | 31.56 | 32.93 |
| C513u | 516352 | 173919 | 24.16 | 25.42 | 26.05 | 26.69 | 27.29 | 28.17 | 28.51 | 30.96 | 31.54 | 32.89 |
| C513d | 516352 | 173919 | 24.16 | 25.42 | 26.05 | 26.69 | 27.29 | 28.17 | 28.51 | 30.96 | 31.54 | 32.89 |
| C512 | 516370 | 173977 | 24.16 | 25.42 | 26.05 | 26.69 | 27.29 | 28.17 | 28.51 | 30.96 | 31.54 | 32.80 |
| C511 | 516311 | 174096 | 24.16 | 25.42 | 26.05 | 26.69 | 27.29 | 28.18 | 28.51 | 30.96 | 31.50 | 32.14 |
| C510 | 516281 | 174173 | 24.16 | 25.42 | 26.05 | 26.69 | 27.29 | 28.18 | 28.51 | 30.85 | 31.35 | 31.18 |
| C509 | 516314 | 174220 | 24.20 | 25.43 | 26.07 | 26.74 | 27.30 | 28.22 | 28.55 | 30.86 | 31.36 | 32.18 |
| C509d | 516314 | 174220 | 24.20 | 25.43 | 26.07 | 26.74 | 27.30 | 28.22 | 28.55 | 30.86 | 31.36 | 32.18 |
| C508u | 516332 | 174310 | 24.20 | 25.43 | 26.07 | 26.74 | 27.30 | 28.22 | 28.55 | 30.86 | 31.36 | 32.17 |
| C508d | 516332 | 174310 | 24.20 | 25.43 | 26.07 | 26.74 | 27.30 | 28.22 | 28.55 | 30.86 | 31.36 | 32.17 |
| C507 | 516338 | 174406 | 24.20 | 25.43 | 26.07 | 26.74 | 27.30 | 28.22 | 28.55 | 30.86 | 31.36 | 32.16 |
| C507d | 516338 | 174406 | 24.20 | 25.43 | 26.07 | 26.74 | 27.30 | 28.22 | 28.55 | 30.86 | 31.36 | 32.16 |
| W001 | 516330 | 174440 | 0.21 | 0.21 | 0.21 | 0.26 | 0.28 | 0.32 | 0.34 | 0.69 | 1.39 | 5.89 |

Detailed FRA centred on: St Margarets Business Park Car Park, Twickenham, TW1 1JS - 03/03/2022 - HNL 253000 NR



Environment Agency
 Alchemy,
 Bessemer Road,
 Welwyn Garden City,
 Hertfordshire,
 AL7 1HE



Legend

- Main Rivers
- Site location

2D Node Results: Heights

- 1 in 1000 (0.1%) Defended

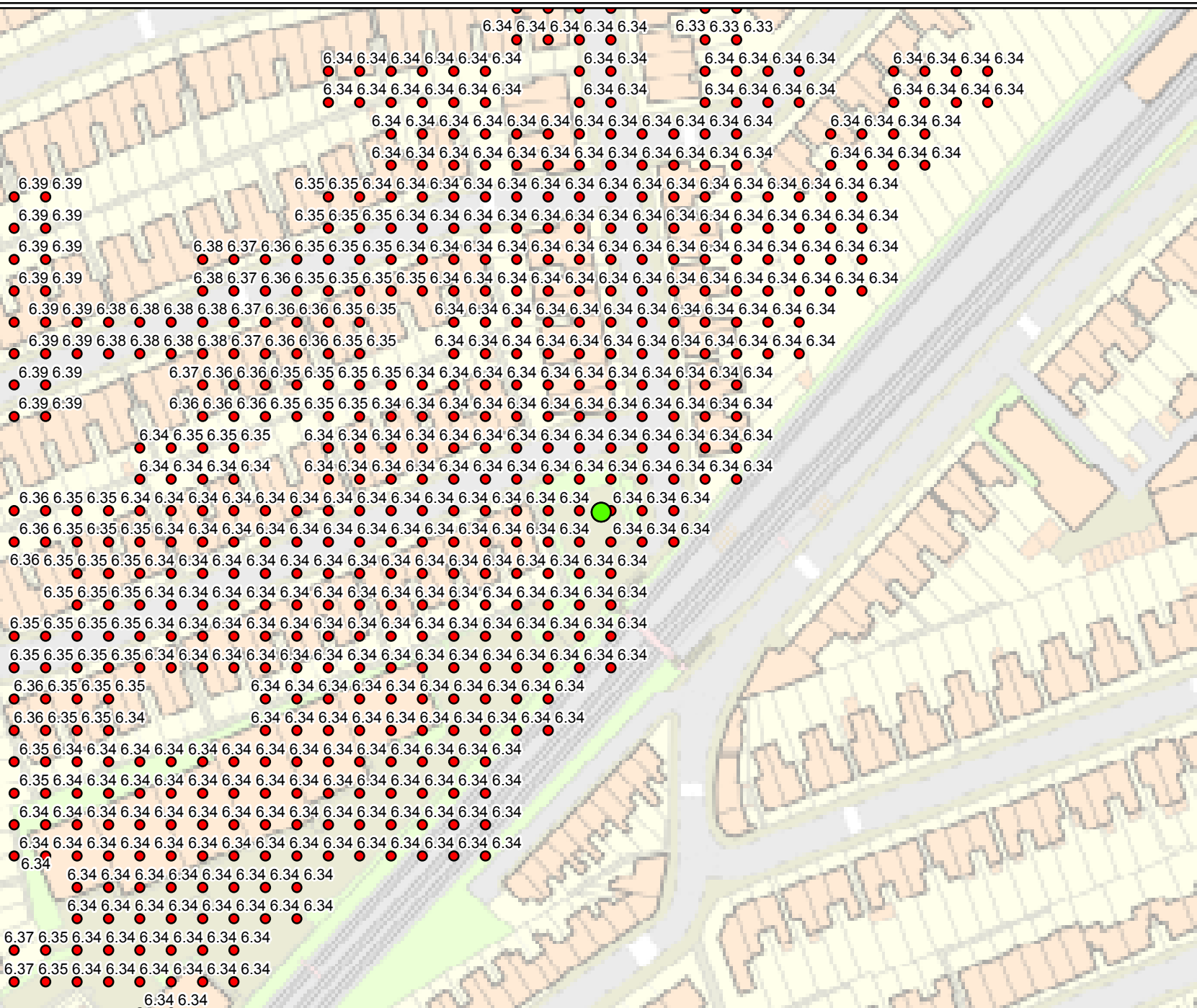
The data in this map has been extracted from the River Crane Mapping Study (Halcrow 2008). This model has been designed for catchment wide flood risk mapping. It should be noted that it was not created to produce flood levels for specific development sites within the catchment.

Modelled outlines take into account catchment wide defences.

Flood risk data requests including an allowance for climate change will be based on the 1 in 100 flood plus 20% allowance for climate change, unless otherwise stated. You should refer to 'Flood risk assessments: climate change allowances' to check if this allowance is still appropriate for the type of development you are proposing and its location. You may need to undertake further assessment of future flood risk using different allowances to ensure your assessment of future flood risk is based on best available evidence.

<https://www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances>

Produced by:
 Partnerships & Strategic Overview,
 Hertfordshire & North London



APPENDIX D
THAMES WATER CORRESPONDENCE

Sewer Flooding

History Enquiry



Property Searches

Simpson Associates

Friday Street

Search address supplied St Margarets Business Car Park
Winchester Road
Twickenham
TW1 1JS

Your reference St Margarets Business Car Park

Our reference SFH/SFH Standard/2020_4207835

Received date 2 July 2020

Search date 2 July 2020



Thames Water Utilities Ltd
Property Searches, PO Box 3189, Slough SL1 4WW
DX 151280 Slough 13



searches@thameswater.co.uk
www.thameswater-propertysearches.co.uk



0845 070 9148

Sewer Flooding

History Enquiry



Property Searches

Search address supplied: St Margarets Business Car Park, Winchester Road, Twickenham, TW1 1JS

This search is recommended to check for any sewer flooding in a specific address or area

TWUL, trading as Property Searches, are responsible in respect of the following:-

- (i) any negligent or incorrect entry in the records searched;
- (ii) any negligent or incorrect interpretation of the records searched;
- (iii) and any negligent or incorrect recording of that interpretation in the search report
- (iv) compensation payments



Thames Water Utilities Ltd
Property Searches, PO Box 3189, Slough SL1 4WW
DX 151280 Slough 13



searches@thameswater.co.uk
www.thameswater-propertysearches.co.uk



0845 070 9148

History of Sewer Flooding

Is the requested address or area at risk of flooding due to overloaded public sewers?

The flooding records held by Thames Water indicate that there have been no incidents of flooding in the requested area as a result of surcharging public sewers.

For your guidance:

- A sewer is “overloaded” when the flow from a storm is unable to pass through it due to a permanent problem (e.g. flat gradient, small diameter). Flooding as a result of temporary problems such as blockages, siltation, collapses and equipment or operational failures are excluded.
- “Internal flooding” from public sewers is defined as flooding, which enters a building or passes below a suspended floor. For reporting purposes, buildings are restricted to those normally occupied and used for residential, public, commercial, business or industrial purposes.
- “At Risk” properties are those that the water company is required to include in the Regulatory Register that is presented annually to the Director General of Water Services. These are defined as properties that have suffered, or are likely to suffer, internal flooding from public foul, combined or surface water sewers due to overloading of the sewerage system more frequently than the relevant reference period (either once or twice in ten years) as determined by the Company’s reporting procedure.
- Flooding as a result of storm events proven to be exceptional and beyond the reference period of one in ten years are not included on the At Risk Register.
- Properties may be at risk of flooding but not included on the Register where flooding incidents have not been reported to the Company.
- Public Sewers are defined as those for which the Company holds statutory responsibility under the Water Industry Act 1991.
- It should be noted that flooding can occur from private sewers and drains which are not the responsibility of the Company. This report excludes flooding from private sewers and drains and the Company makes no comment upon this matter.
- For further information please contact Thames Water on Tel: 0800 316 9800 or website www.thameswater.co.uk



Thames Water Utilities Ltd
Property Searches, PO Box 3189, Slough SL1 4WW
DX 151280 Slough 13



searches@thameswater.co.uk
www.thameswater-propertysearches.co.uk



0845 070 9148



Mr B Tawton
Simpson Associates
8 Friday st
Henley on Thames
Oxfordshire
RG9 1AH



Our ref: DS6075425



0800 009 3921

Monday to Friday, 8am to 5pm

8th July 2020

Pre-planning enquiry: Wastewater Capacity check

Dear Mr Tawton

Thank you for providing details of your development with the Pre-Planning application dated 2nd July 20 for development @ St. Magarets Buisness Centre Drummond Place Twickenham TW1 1JS

Existing brownfld site ,developed to { 4 dwellings } as per your above application.

We have completed the assessment of the foul water flows and surface water run-off based on the information submitted in your application with the purpose of assessing sewerage capacity within the existing Thames Water sewer network.

Foul

If your proposals progress in line with the details you've provided as above, we're pleased to confirm that there will be sufficient sewerage capacity in the nearest TW foul sewer network to serve your foul discharges from your development, provided it is by gravity.

This confirmation is valid for 12 months or for the life of any planning approval that this information is used to support, to a maximum of three years.

You'll need to keep us informed of any changes to your design – for example, an increase in the number or density of homes. Such changes could mean there is no longer sufficient capacity and has to be investigated again.

Surface Water

When developing a site, policy 5.13 of the London Plan and Policy 3.4 of the Supplementary Planning Guidance (Sustainable Design And Construction) states that every attempt should be made to use flow attenuation and SuDS/Storage to reduce the surface water discharge from the site as much as possible.

In accordance with the Building Act 2000 Clause H3.3, positive connection of surface water to a public sewer will only be consented when it can be demonstrated that the hierarchy of disposal methods have been examined and proven to be impracticable. Before we can consider your

surface water needs, you'll need written approval from the lead local flood authority that you have followed the sequential approach to the disposal of surface water and considered all practical means.

The disposal hierarchy being:

1. store rainwater for later use.
2. use infiltration techniques where possible.
3. attenuate rainwater in ponds or open water features for gradual release.
4. attenuate rainwater by storing in tanks or sealed water features for gradual release.
5. discharge rainwater direct to a watercourse.
6. discharge rainwater to a surface water sewer/drain.
7. discharge rainwater to the combined sewer.
8. discharge rainwater to the foul sewer

Where connection to the public sewerage network is still required to manage surface water flows we will accept these flows at a discharge rate in line with CIRIA's best practice guide on SuDS or that stated within the sites planning approval.

If the above surface water hierarchy has been followed and if the flows are restricted to a total of 2 l/s to TW surface water sewer , then Thames Water would not have any objections to the proposal.

Please see the attached 'Planning your wastewater' leaflet for additional information. At the appropriate time, you will have to apply for a S106 connection application to DS Connection team

This confirmation is valid for 12 months or for the life of any planning approval that this information is used to support, to a maximum of three years.

Please note that you must keep us informed of any changes to your design – for example, an increase in the number or density of homes. Such changes could mean there is no longer sufficient sewerage capacity.

What happens next?

Please make sure you submit your connection application, when you are ready, giving us at least 21 days' notice of the date you wish to make your new connection/s.

If you've any further questions, please contact me.

Yours sincerely

Siva Sivarajan

Developer Services- Wastewater Adoptions Engineer
Office:0203 577 7752 Mobile: 07747842608
siva.sivarajan@thameswater.co.uk

Thames Water Utilities Ltd, Clearwater Court, Vastern Road, Reading, Berkshire, RG1 8DB
Find us online at developers.thameswater.co.uk



TW Int ref : DTS 66298

APPENDIX E
LONDON SUSTAINABLE DRAINAGE PROFORMA

| | | |
|---------------------------|---|--|
| 1. Project & Site Details | Project / Site Name (including sub-catchment / stage / phase where appropriate) | St Margaret's Business Car Park |
| | Address & post code | Moor Mead Road Twickenham TW1 1JS |
| | OS Grid ref. (Easting, Northing) | E 516645 N 174123 |
| | LPA reference (if applicable) | N/A |
| | Brief description of proposed work | The proposed development comprises 3 No. residential dwellings with associated gardens and parking spaces. |
| | Total site Area | 628 m ² |
| | Total existing impervious area | 628 m ² |
| | Total proposed impervious area | 628 m ² |
| | Is the site in a surface water flood risk catchment (ref. local Surface Water Management Plan)? | No |
| | Existing drainage connection type and location | Surface water sewer in Godstone Road. |
| | Designer Name | Gareth Crowther |
| | Designer Position | Partner |
| | Designer Company | Simpson TWS |

| | | | |
|---|--|----------------------------|-----------------------|
| 2. Proposed Discharge Arrangements | 2a. Infiltration Feasibility | | |
| | Superficial geology classification | Kempton Park Gravel Member | |
| | Bedrock geology classification | London Clay | |
| | Site infiltration rate | N/A | m/s |
| | Depth to groundwater level | Not known | m below ground level |
| | Is infiltration feasible? | No | |
| | 2b. Drainage Hierarchy | | |
| | | <i>Feasible (Y/N)</i> | <i>Proposed (Y/N)</i> |
| | 1 store rainwater for later use | Y | Y |
| | 2 use infiltration techniques, such as porous surfaces in non-clay areas | N | N |
| | 3 attenuate rainwater in ponds or open water features for gradual release | N | N |
| | 4 attenuate rainwater by storing in tanks or sealed water features for gradual release | Y | Y |
| | 5 discharge rainwater direct to a watercourse | N | N |
| | 6 discharge rainwater to a surface water sewer/drain | Y | Y |
| | 7 discharge rainwater to the combined sewer. | N | N |
| 2c. Proposed Discharge Details | | | |
| Proposed discharge location | Surface water sewer in Godstone Road | | |
| Has the owner/regulator of the discharge location been consulted? | Yes | | |

| 3a. Discharge Rates & Required Storage | | | | |
|--|--------------------------------------|---|--|-------------------------------------|
| | Greenfield (GF) runoff rate (l/s) | Existing discharge rate (l/s) | Required storage for GF rate (m ³) | Proposed discharge rate (l/s) |
| Q _{bar} | 0.9 | 0.9 | 0.9 | 0.9 |
| 1 in 1 | 0.7 | 2.3 | 1.7 | 0.7 |
| 1 in 30 | 1.5 | 5.1 | 4.5 | 1.2 |
| 1 in 100 | 1.7 | 6.6 | 6.2 | 1.4 |
| 1 in 100 + CC | 1.7 | 6.6 | 9.1 | 1.7 |
| Climate change allowance used | | 40% | | |
| 3b. Principal Method of Flow Control | | Pervious Pavement & Hydrobrake flow control | | |
| 3c. Proposed SuDS Measures | | | | |
| | Catchment area (m ²) | Plan area (m ²) | Storage vol. (m ³) | |
| Rainwater harvesting | 0 | 0 | 0 | |
| Infiltration systems | 0 | 0 | 0 | |
| Green roofs | 0 | 0 | 0 | |
| Blue roofs | 0 | 0 | 0 | |
| Filter strips | 0 | 0 | 0 | |
| Filter drains | 0 | 0 | 0 | |
| Bioretention / tree pits | 0 | 0 | 0 | |
| Pervious pavements | 58.4 | 0 | 9.2 | |
| Swales | 0 | 0 | 0 | |
| Basins/ponds | 0 | 0 | 0 | |
| Attenuation tanks | 0 | 0 | 0 | |
| Total | 58.4 | 0 | 9.2 | |

3. Drainage Strategy

| 4a. Discharge & Drainage Strategy | | Page/section of drainage report |
|---|--|---------------------------------|
| Infiltration feasibility (2a) – geotechnical factual and interpretive reports, including infiltration results | | Page 4 / Paragraph 2.4 |
| Drainage hierarchy (2b) | | Page 16 / Table 1 |
| Proposed discharge details (2c) – utility plans, correspondence / approval from owner/regulator of discharge location | | Appendix D |
| Discharge rates & storage (3a) – detailed hydrologic and hydraulic calculations | | Appendix F & H |
| Proposed SuDS measures & specifications (3b) | | Page 19 / Paragraph 8.18 |
| 4b. Other Supporting Details | | Page/section of drainage report |
| Detailed Development Layout | | Appendix B |
| Detailed drainage design drawings, including exceedance flow routes | | Appendix G |
| Detailed landscaping plans | | Appendix B |
| Maintenance strategy | | Page 21 / Paragraph 8.27 |
| Demonstration of how the proposed SuDS measures improve: | | |
| a) water quality of the runoff? | | Page 21 / Table 6 |
| b) biodiversity? | | Page 21 / Paragraph 8.26 |
| c) amenity? | | Page 21 / Paragraph 8.26 |

4. Supporting Information

**APPENDIX F
RUNOFF CALCULATIONS**

4TH FLOOR
 43 EAGLE STREET
 LONDON WC1R 4AT



Date 07/08/2020 14:13
 File Permeable Paving & Atte...

Designed by garethcrowther
 Checked by

XP Solutions

Source Control 2018.1.1

ICP SUDS Mean Annual Flood

Input

| | | | |
|-----------------------|-------|---------------|----------|
| Return Period (years) | 100 | Soil | 0.500 |
| Area (ha) | 0.060 | Urban | 0.750 |
| SAAR (mm) | 700 | Region Number | Region 6 |

Results 1/s

QBAR Rural 0.3
 QBAR Urban 0.9

Q100 years 1.7

Q1 year 0.7
 Q30 years 1.5
 Q100 years 1.7

P20-435, St Margarets Business Car Park - Modified Rational Method Runoff Calculations (Pre-Development)

Peak Runoff Rate = $3.61 \times \text{Runoff Volume Coefficient (Cv)} \times \text{Area (A)} \times \text{Peak Rainfall Intensity (I}_{\text{peak}})$

Runoff Volume = $\text{Runoff Coefficient (C)} \times \text{Area (A)} \times \text{Average Rainfall intensity (I}_{\text{ave}}) \times \text{Storm Duration}$

Pre-development Runoff

| Return Period | Cv | I _(peak) (mm) | I _(ave) (mm) | A (Ha) | Peak Runoff Rate (l/s) | Runoff Volume (m ³) |
|---------------|------|--------------------------|-------------------------|--------|------------------------|---------------------------------|
| 1 | 0.75 | 14.118 | 3.601 | 0.060 | 2.3 | 9.7 |
| 30 | 0.75 | 31.172 | 7.952 | 0.060 | 5.1 | 21.5 |
| 100 | 0.75 | 40.444 | 10.317 | 0.060 | 6.6 | 27.9 |



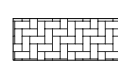

Notes

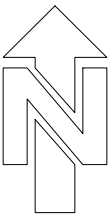
1. Rainfall intensities generated from the FSR rainfall model facility in MicroDrainage.
2. Peak and average rainfall intensities are based on the following FSR data:

Storm Duration: 360 min (6hrs)
M5-60 (mm): 20.000
Ratio R 0.410

APPENDIX G
PROPOSED DRAINAGE STRATEGY PLAN


LEGEND

-  PROPOSED SURFACE WATER DRAINAGE
-  PROPOSED COLLECTOR / DISTRIBUTOR DRAIN
-  PROPOSED PERMEABLE PAVING AREA = 58m²
-  SITE BOUNDARY.



| | |
|---|-----------------------|
| P1 First Issue | GSC 11.03.22 |
| | |
| | |
| | |
| DRAWING STATUS | |
| PLANNING | |
| DRAWING TITLE | |
| SURFACE WATER DRAINAGE STRATEGY PLAN | |
| PROJECT Project Number P20-435 | |
| ST MARGARET'S BUSINESS CENTRE MOOR MEAD ROAD TWICKENHAM TW1 1JS | |
|  | |
| 8 Friday Street Henley on Thames Oxfordshire RG9 1AH T: 01491 576221 | |
|  | |
| London, Henley-on-Thames, Gloucester and Exeter | |
| Drawn J.J.H. | Chkd G.S.C. |
| Scales 1:100@A1 | Date AUG20 |
| PLANNING | |
| Drawing Number P20-435A-SK01 | Revision P1 |

**APPENDIX H
DRAINAGE STRATEGY DESIGN RESULTS**

| | | |
|--|--|---|
| SIMPSON ASSOCIATES | | Page 1 |
| 4TH FLOOR 43 EAGLE STREET LONDON WC1R 4AT | |  |
| Date 11/03/2022 15:14 File Permeable Paving Design... | Designed by garethcrowther Checked by | |
| XP Solutions | | Source Control 2018.1.1 |

Model Details

Storage is Online Cover Level (m) 6.250

Porous Car Park Structure

| | | | |
|--------------------------------------|---------|-------------------------|------|
| Infiltration Coefficient Base (m/hr) | 0.00000 | Width (m) | 4.0 |
| Membrane Percolation (mm/hr) | 1000 | Length (m) | 14.6 |
| Max Percolation (l/s) | 16.2 | Slope (1:X) | 0.0 |
| Safety Factor | 2.0 | Depression Storage (mm) | 5 |
| Porosity | 0.30 | Evaporation (mm/day) | 3 |
| Invert Level (m) | 5.515 | Membrane Depth (m) | 0 |

Hydro-Brake® Optimum Outflow Control

| | |
|-----------------------------------|----------------------------|
| Unit Reference | MD-SCU-0046-1700-0525-1700 |
| Design Head (m) | 0.525 |
| Design Flow (l/s) | 1.7 |
| Flush-Flo™ | Calculated |
| Objective | Linear discharge profile |
| Application | Surface |
| Sump Available | Yes |
| Diameter (mm) | 46 |
| Invert Level (m) | 5.540 |
| Minimum Outlet Pipe Diameter (mm) | 75 |
| Suggested Manhole Diameter (mm) | 1200 |

| Control Points | Head (m) | Flow (l/s) |
|---------------------------|----------|------------|
| Design Point (Calculated) | 0.525 | 1.7 |
| Flush-Flo™ | 0.069 | 0.7 |
| Kick-Flo® | 0.069 | 0.7 |
| Mean Flow over Head Range | - | 1.2 |

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

| Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) |
|-----------|------------|-----------|------------|-----------|------------|-----------|------------|
| 0.100 | 0.8 | 1.200 | 2.5 | 3.000 | 3.8 | 7.000 | 5.7 |
| 0.200 | 1.1 | 1.400 | 2.7 | 3.500 | 4.1 | 7.500 | 5.9 |
| 0.300 | 1.3 | 1.600 | 2.8 | 4.000 | 4.4 | 8.000 | 6.1 |
| 0.400 | 1.5 | 1.800 | 3.0 | 4.500 | 4.6 | 8.500 | 6.3 |
| 0.500 | 1.7 | 2.000 | 3.1 | 5.000 | 4.8 | 9.000 | 6.5 |
| 0.600 | 1.8 | 2.200 | 3.3 | 5.500 | 5.1 | 9.500 | 6.7 |
| 0.800 | 2.1 | 2.400 | 3.4 | 6.000 | 5.3 | | |
| 1.000 | 2.3 | 2.600 | 3.6 | 6.500 | 5.5 | | |

Summary of Results for 1 year Return Period

Half Drain Time : 42 minutes.


| Storm Event | Max Level (m) | Max Depth (m) | Max Infiltration (l/s) | Max Control (l/s) | Max Σ Outflow (l/s) | Max Volume (m ³) | Status |
|------------------|---------------|---------------|------------------------|-------------------|---------------------|------------------------------|--------|
| 15 min Summer | 5.579 | 0.064 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 30 min Summer | 5.592 | 0.077 | 0.0 | 0.6 | 0.6 | 1.3 | O K |
| 60 min Summer | 5.602 | 0.087 | 0.0 | 0.7 | 0.7 | 1.5 | O K |
| 120 min Summer | 5.605 | 0.090 | 0.0 | 0.7 | 0.7 | 1.6 | O K |
| 180 min Summer | 5.603 | 0.088 | 0.0 | 0.7 | 0.7 | 1.5 | O K |
| 240 min Summer | 5.599 | 0.084 | 0.0 | 0.6 | 0.6 | 1.5 | O K |
| 360 min Summer | 5.592 | 0.077 | 0.0 | 0.6 | 0.6 | 1.4 | O K |
| 480 min Summer | 5.586 | 0.071 | 0.0 | 0.5 | 0.5 | 1.2 | O K |
| 600 min Summer | 5.582 | 0.067 | 0.0 | 0.5 | 0.5 | 1.2 | O K |
| 720 min Summer | 5.579 | 0.064 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 960 min Summer | 5.574 | 0.059 | 0.0 | 0.4 | 0.4 | 1.0 | O K |
| 1440 min Summer | 5.569 | 0.054 | 0.0 | 0.3 | 0.3 | 0.9 | O K |
| 2160 min Summer | 5.564 | 0.049 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 2880 min Summer | 5.562 | 0.047 | 0.0 | 0.2 | 0.2 | 0.8 | O K |
| 4320 min Summer | 5.558 | 0.043 | 0.0 | 0.1 | 0.1 | 0.8 | O K |
| 5760 min Summer | 5.556 | 0.041 | 0.0 | 0.1 | 0.1 | 0.7 | O K |
| 7200 min Summer | 5.555 | 0.040 | 0.0 | 0.1 | 0.1 | 0.7 | O K |
| 8640 min Summer | 5.554 | 0.039 | 0.0 | 0.1 | 0.1 | 0.7 | O K |
| 10080 min Summer | 5.553 | 0.038 | 0.0 | 0.1 | 0.1 | 0.7 | O K |
| 15 min Winter | 5.588 | 0.073 | 0.0 | 0.5 | 0.5 | 1.3 | O K |

| Storm Event | Rain (mm/hr) | Flooded Volume (m ³) | Discharge Volume (m ³) | Time-Peak (mins) |
|------------------|--------------|----------------------------------|------------------------------------|------------------|
| 15 min Summer | 31.246 | 0.0 | 0.8 | 16 |
| 30 min Summer | 20.306 | 0.0 | 1.3 | 25 |
| 60 min Summer | 12.800 | 0.0 | 1.9 | 42 |
| 120 min Summer | 7.903 | 0.0 | 2.5 | 74 |
| 180 min Summer | 5.931 | 0.0 | 2.8 | 106 |
| 240 min Summer | 4.833 | 0.0 | 3.2 | 136 |
| 360 min Summer | 3.601 | 0.0 | 3.6 | 196 |
| 480 min Summer | 2.913 | 0.0 | 3.9 | 256 |
| 600 min Summer | 2.471 | 0.0 | 4.2 | 314 |
| 720 min Summer | 2.161 | 0.0 | 4.4 | 376 |
| 960 min Summer | 1.748 | 0.0 | 4.8 | 492 |
| 1440 min Summer | 1.296 | 0.0 | 5.4 | 736 |
| 2160 min Summer | 0.962 | 0.0 | 6.0 | 1100 |
| 2880 min Summer | 0.779 | 0.0 | 6.5 | 1456 |
| 4320 min Summer | 0.577 | 0.0 | 7.2 | 2200 |
| 5760 min Summer | 0.467 | 0.0 | 7.6 | 2936 |
| 7200 min Summer | 0.396 | 0.0 | 8.0 | 3664 |
| 8640 min Summer | 0.347 | 0.0 | 8.3 | 4408 |
| 10080 min Summer | 0.310 | 0.0 | 8.6 | 5096 |
| 15 min Winter | 31.246 | 0.0 | 1.0 | 16 |

Summary of Results for 1 year Return Period

| Storm Event | Max Level (m) | Max Depth (m) | Max Infiltration (l/s) | Max Control (l/s) | Max Σ Outflow (l/s) | Max Volume (m³) | Status |
|------------------|---------------|---------------|------------------------|-------------------|---------------------|-----------------|--------|
| 30 min Winter | 5.602 | 0.087 | 0.0 | 0.7 | 0.7 | 1.5 | O K |
| 60 min Winter | 5.611 | 0.096 | 0.0 | 0.7 | 0.7 | 1.7 | O K |
| 120 min Winter | 5.609 | 0.094 | 0.0 | 0.7 | 0.7 | 1.6 | O K |
| 180 min Winter | 5.602 | 0.087 | 0.0 | 0.7 | 0.7 | 1.5 | O K |
| 240 min Winter | 5.595 | 0.080 | 0.0 | 0.6 | 0.6 | 1.4 | O K |
| 360 min Winter | 5.586 | 0.071 | 0.0 | 0.5 | 0.5 | 1.2 | O K |
| 480 min Winter | 5.580 | 0.065 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 600 min Winter | 5.575 | 0.060 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 720 min Winter | 5.573 | 0.058 | 0.0 | 0.3 | 0.3 | 1.0 | O K |
| 960 min Winter | 5.569 | 0.054 | 0.0 | 0.3 | 0.3 | 0.9 | O K |
| 1440 min Winter | 5.564 | 0.049 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 2160 min Winter | 5.560 | 0.045 | 0.0 | 0.1 | 0.1 | 0.8 | O K |
| 2880 min Winter | 5.558 | 0.043 | 0.0 | 0.1 | 0.1 | 0.8 | O K |
| 4320 min Winter | 5.555 | 0.040 | 0.0 | 0.1 | 0.1 | 0.7 | O K |
| 5760 min Winter | 5.554 | 0.039 | 0.0 | 0.1 | 0.1 | 0.7 | O K |
| 7200 min Winter | 5.553 | 0.038 | 0.0 | 0.1 | 0.1 | 0.7 | O K |
| 8640 min Winter | 5.552 | 0.037 | 0.0 | 0.1 | 0.1 | 0.6 | O K |
| 10080 min Winter | 5.551 | 0.036 | 0.0 | 0.1 | 0.1 | 0.6 | O K |

| Storm Event | Rain (mm/hr) | Flooded Volume (m³) | Discharge Volume (m³) | Time-Peak (mins) |
|------------------|--------------|---------------------|-----------------------|------------------|
| 30 min Winter | 20.306 | 0.0 | 1.6 | 26 |
| 60 min Winter | 12.800 | 0.0 | 2.2 | 44 |
| 120 min Winter | 7.903 | 0.0 | 2.8 | 80 |
| 180 min Winter | 5.931 | 0.0 | 3.3 | 110 |
| 240 min Winter | 4.833 | 0.0 | 3.6 | 142 |
| 360 min Winter | 3.601 | 0.0 | 4.1 | 200 |
| 480 min Winter | 2.913 | 0.0 | 4.5 | 258 |
| 600 min Winter | 2.471 | 0.0 | 4.8 | 320 |
| 720 min Winter | 2.161 | 0.0 | 5.1 | 376 |
| 960 min Winter | 1.748 | 0.0 | 5.5 | 492 |
| 1440 min Winter | 1.296 | 0.0 | 6.1 | 734 |
| 2160 min Winter | 0.962 | 0.0 | 6.9 | 1104 |
| 2880 min Winter | 0.779 | 0.0 | 7.4 | 1452 |
| 4320 min Winter | 0.577 | 0.0 | 8.2 | 2204 |
| 5760 min Winter | 0.467 | 0.0 | 8.7 | 2936 |
| 7200 min Winter | 0.396 | 0.0 | 9.2 | 3560 |
| 8640 min Winter | 0.347 | 0.0 | 9.6 | 4408 |
| 10080 min Winter | 0.310 | 0.0 | 9.9 | 5120 |

| | | |
|--|--|---|
| SIMPSON ASSOCIATES | | Page 3 |
| 4TH FLOOR 43 EAGLE STREET LONDON WC1R 4AT | |  |
| Date 11/03/2022 15:18 File Permeable Paving Design... | Designed by garethcrowther Checked by | |
| XP Solutions | Source Control 2018.1.1 | |

Rainfall Details

| | | | |
|-----------------------|-------------------|-----------------------|-------|
| Rainfall Model | FSR | Winter Storms | Yes |
| Return Period (years) | 1 | Cv (Summer) | 0.750 |
| Region | England and Wales | Cv (Winter) | 0.840 |
| M5-60 (mm) | 20.000 | Shortest Storm (mins) | 15 |
| Ratio R | 0.410 | Longest Storm (mins) | 10080 |
| Summer Storms | Yes | Climate Change % | +0 |

Time Area Diagram

Total Area (ha) 0.027

| Time (mins) | | Area |
|-------------|-----|-------|
| From: | To: | (ha) |
| 0 | 4 | 0.027 |

Summary of Results for 30 year Return Period

Half Drain Time : 46 minutes.


| Storm Event | Max Level (m) | Max Depth (m) | Max Infiltration (l/s) | Max Control (l/s) | Max Σ Outflow (l/s) | Max Volume (m ³) | Status |
|------------------|---------------|---------------|------------------------|-------------------|---------------------|------------------------------|--------|
| 15 min Summer | 5.691 | 0.176 | 0.0 | 1.0 | 1.0 | 3.1 | O K |
| 30 min Summer | 5.727 | 0.212 | 0.0 | 1.1 | 1.1 | 3.7 | O K |
| 60 min Summer | 5.747 | 0.232 | 0.0 | 1.1 | 1.1 | 4.1 | O K |
| 120 min Summer | 5.747 | 0.232 | 0.0 | 1.1 | 1.1 | 4.1 | O K |
| 180 min Summer | 5.733 | 0.218 | 0.0 | 1.1 | 1.1 | 3.8 | O K |
| 240 min Summer | 5.716 | 0.201 | 0.0 | 1.0 | 1.0 | 3.5 | O K |
| 360 min Summer | 5.685 | 0.170 | 0.0 | 1.0 | 1.0 | 3.0 | O K |
| 480 min Summer | 5.661 | 0.146 | 0.0 | 0.9 | 0.9 | 2.6 | O K |
| 600 min Summer | 5.643 | 0.128 | 0.0 | 0.8 | 0.8 | 2.2 | O K |
| 720 min Summer | 5.628 | 0.113 | 0.0 | 0.8 | 0.8 | 2.0 | O K |
| 960 min Summer | 5.607 | 0.092 | 0.0 | 0.7 | 0.7 | 1.6 | O K |
| 1440 min Summer | 5.589 | 0.074 | 0.0 | 0.6 | 0.6 | 1.3 | O K |
| 2160 min Summer | 5.578 | 0.063 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 2880 min Summer | 5.573 | 0.058 | 0.0 | 0.3 | 0.3 | 1.0 | O K |
| 4320 min Summer | 5.567 | 0.052 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 5760 min Summer | 5.564 | 0.049 | 0.0 | 0.2 | 0.2 | 0.8 | O K |
| 7200 min Summer | 5.561 | 0.046 | 0.0 | 0.2 | 0.2 | 0.8 | O K |
| 8640 min Summer | 5.560 | 0.045 | 0.0 | 0.1 | 0.1 | 0.8 | O K |
| 10080 min Summer | 5.558 | 0.043 | 0.0 | 0.1 | 0.1 | 0.8 | O K |
| 15 min Winter | 5.716 | 0.201 | 0.0 | 1.0 | 1.0 | 3.5 | O K |

| Storm Event | Rain (mm/hr) | Flooded Volume (m ³) | Discharge Volume (m ³) | Time-Peak (mins) |
|------------------|--------------|----------------------------------|------------------------------------|------------------|
| 15 min Summer | 76.671 | 0.0 | 3.1 | 17 |
| 30 min Summer | 49.712 | 0.0 | 4.3 | 29 |
| 60 min Summer | 30.811 | 0.0 | 5.5 | 44 |
| 120 min Summer | 18.537 | 0.0 | 6.8 | 78 |
| 180 min Summer | 13.628 | 0.0 | 7.5 | 112 |
| 240 min Summer | 10.910 | 0.0 | 8.1 | 144 |
| 360 min Summer | 7.952 | 0.0 | 8.9 | 208 |
| 480 min Summer | 6.352 | 0.0 | 9.5 | 268 |
| 600 min Summer | 5.333 | 0.0 | 10.0 | 328 |
| 720 min Summer | 4.621 | 0.0 | 10.4 | 388 |
| 960 min Summer | 3.685 | 0.0 | 11.1 | 502 |
| 1440 min Summer | 2.675 | 0.0 | 12.1 | 738 |
| 2160 min Summer | 1.940 | 0.0 | 13.1 | 1100 |
| 2880 min Summer | 1.543 | 0.0 | 13.9 | 1468 |
| 4320 min Summer | 1.117 | 0.0 | 15.0 | 2200 |
| 5760 min Summer | 0.887 | 0.0 | 15.8 | 2912 |
| 7200 min Summer | 0.742 | 0.0 | 16.4 | 3664 |
| 8640 min Summer | 0.641 | 0.0 | 16.9 | 4376 |
| 10080 min Summer | 0.567 | 0.0 | 17.3 | 5040 |
| 15 min Winter | 76.671 | 0.0 | 3.6 | 17 |

Summary of Results for 30 year Return Period

| Storm Event | Max Level (m) | Max Depth (m) | Max Infiltration (l/s) | Max Control (l/s) | Max Σ Outflow (l/s) | Max Volume (m³) | Status |
|------------------|---------------|---------------|------------------------|-------------------|---------------------|-----------------|--------|
| 30 min Winter | 5.756 | 0.241 | 0.0 | 1.1 | 1.1 | 4.2 | O K |
| 60 min Winter | 5.775 | 0.260 | 0.0 | 1.2 | 1.2 | 4.5 | O K |
| 120 min Winter | 5.765 | 0.250 | 0.0 | 1.2 | 1.2 | 4.4 | O K |
| 180 min Winter | 5.740 | 0.225 | 0.0 | 1.1 | 1.1 | 4.0 | O K |
| 240 min Winter | 5.715 | 0.200 | 0.0 | 1.0 | 1.0 | 3.5 | O K |
| 360 min Winter | 5.673 | 0.158 | 0.0 | 0.9 | 0.9 | 2.8 | O K |
| 480 min Winter | 5.643 | 0.128 | 0.0 | 0.8 | 0.8 | 2.2 | O K |
| 600 min Winter | 5.621 | 0.106 | 0.0 | 0.7 | 0.7 | 1.9 | O K |
| 720 min Winter | 5.605 | 0.090 | 0.0 | 0.7 | 0.7 | 1.6 | O K |
| 960 min Winter | 5.591 | 0.076 | 0.0 | 0.6 | 0.6 | 1.3 | O K |
| 1440 min Winter | 5.578 | 0.063 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 2160 min Winter | 5.571 | 0.056 | 0.0 | 0.3 | 0.3 | 1.0 | O K |
| 2880 min Winter | 5.567 | 0.052 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 4320 min Winter | 5.562 | 0.047 | 0.0 | 0.2 | 0.2 | 0.8 | O K |
| 5760 min Winter | 5.560 | 0.045 | 0.0 | 0.1 | 0.1 | 0.8 | O K |
| 7200 min Winter | 5.558 | 0.043 | 0.0 | 0.1 | 0.1 | 0.7 | O K |
| 8640 min Winter | 5.556 | 0.041 | 0.0 | 0.1 | 0.1 | 0.7 | O K |
| 10080 min Winter | 5.555 | 0.040 | 0.0 | 0.1 | 0.1 | 0.7 | O K |

| Storm Event | Rain (mm/hr) | Flooded Volume (m³) | Discharge Volume (m³) | Time-Peak (mins) |
|------------------|--------------|---------------------|-----------------------|------------------|
| 30 min Winter | 49.712 | 0.0 | 4.9 | 30 |
| 60 min Winter | 30.811 | 0.0 | 6.2 | 48 |
| 120 min Winter | 18.537 | 0.0 | 7.7 | 84 |
| 180 min Winter | 13.628 | 0.0 | 8.5 | 120 |
| 240 min Winter | 10.910 | 0.0 | 9.1 | 154 |
| 360 min Winter | 7.952 | 0.0 | 10.0 | 218 |
| 480 min Winter | 6.352 | 0.0 | 10.7 | 278 |
| 600 min Winter | 5.333 | 0.0 | 11.3 | 338 |
| 720 min Winter | 4.621 | 0.0 | 11.8 | 390 |
| 960 min Winter | 3.685 | 0.0 | 12.5 | 504 |
| 1440 min Winter | 2.675 | 0.0 | 13.6 | 738 |
| 2160 min Winter | 1.940 | 0.0 | 14.8 | 1104 |
| 2880 min Winter | 1.543 | 0.0 | 15.7 | 1468 |
| 4320 min Winter | 1.117 | 0.0 | 17.0 | 2152 |
| 5760 min Winter | 0.887 | 0.0 | 17.9 | 2912 |
| 7200 min Winter | 0.742 | 0.0 | 18.6 | 3624 |
| 8640 min Winter | 0.641 | 0.0 | 19.2 | 4248 |
| 10080 min Winter | 0.567 | 0.0 | 19.6 | 5040 |

| | | |
|--|--|---|
| SIMPSON ASSOCIATES | | Page 3 |
| 4TH FLOOR 43 EAGLE STREET LONDON WC1R 4AT | |  |
| Date 11/03/2022 15:17 File Permeable Paving Design... | Designed by garethcrowther Checked by | |
| XP Solutions | | Source Control 2018.1.1 |

Rainfall Details

| | | | |
|-----------------------|-------------------|-----------------------|-------|
| Rainfall Model | FSR | Winter Storms | Yes |
| Return Period (years) | 30 | Cv (Summer) | 0.750 |
| Region | England and Wales | Cv (Winter) | 0.840 |
| M5-60 (mm) | 20.000 | Shortest Storm (mins) | 15 |
| Ratio R | 0.410 | Longest Storm (mins) | 10080 |
| Summer Storms | Yes | Climate Change % | +0 |

Time Area Diagram

Total Area (ha) 0.027

| Time (mins) | | Area |
|-------------|-----|-------|
| From: | To: | (ha) |
| 0 | 4 | 0.027 |

Summary of Results for 100 year Return Period

Half Drain Time : 44 minutes.


| Storm Event | Max Level (m) | Max Depth (m) | Max Infiltration (l/s) | Max Control (l/s) | Max Σ Outflow (l/s) | Max Volume (m³) | Status |
|------------------|---------------|---------------|------------------------|-------------------|---------------------|-----------------|--------|
| 15 min Summer | 5.751 | 0.236 | 0.0 | 1.1 | 1.1 | 4.1 | O K |
| 30 min Summer | 5.803 | 0.288 | 0.0 | 1.2 | 1.2 | 5.0 | O K |
| 60 min Summer | 5.830 | 0.315 | 0.0 | 1.3 | 1.3 | 5.5 | O K |
| 120 min Summer | 5.831 | 0.316 | 0.0 | 1.3 | 1.3 | 5.5 | O K |
| 180 min Summer | 5.813 | 0.298 | 0.0 | 1.3 | 1.3 | 5.2 | O K |
| 240 min Summer | 5.791 | 0.276 | 0.0 | 1.2 | 1.2 | 4.8 | O K |
| 360 min Summer | 5.750 | 0.235 | 0.0 | 1.1 | 1.1 | 4.1 | O K |
| 480 min Summer | 5.717 | 0.202 | 0.0 | 1.0 | 1.0 | 3.5 | O K |
| 600 min Summer | 5.691 | 0.176 | 0.0 | 1.0 | 1.0 | 3.1 | O K |
| 720 min Summer | 5.670 | 0.155 | 0.0 | 0.9 | 0.9 | 2.7 | O K |
| 960 min Summer | 5.639 | 0.124 | 0.0 | 0.8 | 0.8 | 2.2 | O K |
| 1440 min Summer | 5.604 | 0.089 | 0.0 | 0.7 | 0.7 | 1.6 | O K |
| 2160 min Summer | 5.587 | 0.072 | 0.0 | 0.5 | 0.5 | 1.3 | O K |
| 2880 min Summer | 5.579 | 0.064 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 4320 min Summer | 5.571 | 0.056 | 0.0 | 0.3 | 0.3 | 1.0 | O K |
| 5760 min Summer | 5.567 | 0.052 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 7200 min Summer | 5.564 | 0.049 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 8640 min Summer | 5.562 | 0.047 | 0.0 | 0.2 | 0.2 | 0.8 | O K |
| 10080 min Summer | 5.560 | 0.045 | 0.0 | 0.1 | 0.1 | 0.8 | O K |
| 15 min Winter | 5.783 | 0.268 | 0.0 | 1.2 | 1.2 | 4.7 | O K |

| Storm Event | Rain (mm/hr) | Flooded Volume (m³) | Discharge Volume (m³) | Time-Peak (mins) |
|------------------|--------------|---------------------|-----------------------|------------------|
| 15 min Summer | 99.536 | 0.0 | 4.3 | 17 |
| 30 min Summer | 65.075 | 0.0 | 5.8 | 30 |
| 60 min Summer | 40.510 | 0.0 | 7.5 | 46 |
| 120 min Summer | 24.362 | 0.0 | 9.1 | 80 |
| 180 min Summer | 17.855 | 0.0 | 10.1 | 114 |
| 240 min Summer | 14.239 | 0.0 | 10.8 | 148 |
| 360 min Summer | 10.317 | 0.0 | 11.8 | 212 |
| 480 min Summer | 8.210 | 0.0 | 12.5 | 274 |
| 600 min Summer | 6.871 | 0.0 | 13.1 | 334 |
| 720 min Summer | 5.939 | 0.0 | 13.6 | 394 |
| 960 min Summer | 4.714 | 0.0 | 14.4 | 512 |
| 1440 min Summer | 3.400 | 0.0 | 15.6 | 740 |
| 2160 min Summer | 2.448 | 0.0 | 16.9 | 1100 |
| 2880 min Summer | 1.937 | 0.0 | 17.7 | 1468 |
| 4320 min Summer | 1.391 | 0.0 | 19.0 | 2180 |
| 5760 min Summer | 1.099 | 0.0 | 19.9 | 2912 |
| 7200 min Summer | 0.915 | 0.0 | 20.6 | 3672 |
| 8640 min Summer | 0.787 | 0.0 | 21.2 | 4376 |
| 10080 min Summer | 0.693 | 0.0 | 21.6 | 5136 |
| 15 min Winter | 99.536 | 0.0 | 4.9 | 17 |

Summary of Results for 100 year Return Period

| Storm Event | Max Level (m) | Max Depth (m) | Max Infiltration (l/s) | Max Control (l/s) | Max Σ Outflow (l/s) | Max Volume (m³) | Status |
|------------------|---------------|---------------|------------------------|-------------------|---------------------|-----------------|--------|
| 30 min Winter | 5.843 | 0.328 | 0.0 | 1.3 | 1.3 | 5.7 | O K |
| 60 min Winter | 5.870 | 0.355 | 0.0 | 1.4 | 1.4 | 6.2 | O K |
| 120 min Winter | 5.861 | 0.346 | 0.0 | 1.4 | 1.4 | 6.1 | O K |
| 180 min Winter | 5.831 | 0.316 | 0.0 | 1.3 | 1.3 | 5.5 | O K |
| 240 min Winter | 5.798 | 0.283 | 0.0 | 1.2 | 1.2 | 5.0 | O K |
| 360 min Winter | 5.741 | 0.226 | 0.0 | 1.1 | 1.1 | 4.0 | O K |
| 480 min Winter | 5.698 | 0.183 | 0.0 | 1.0 | 1.0 | 3.2 | O K |
| 600 min Winter | 5.666 | 0.151 | 0.0 | 0.9 | 0.9 | 2.6 | O K |
| 720 min Winter | 5.642 | 0.127 | 0.0 | 0.8 | 0.8 | 2.2 | O K |
| 960 min Winter | 5.610 | 0.095 | 0.0 | 0.7 | 0.7 | 1.7 | O K |
| 1440 min Winter | 5.587 | 0.072 | 0.0 | 0.5 | 0.5 | 1.3 | O K |
| 2160 min Winter | 5.576 | 0.061 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 2880 min Winter | 5.571 | 0.056 | 0.0 | 0.3 | 0.3 | 1.0 | O K |
| 4320 min Winter | 5.565 | 0.050 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 5760 min Winter | 5.562 | 0.047 | 0.0 | 0.2 | 0.2 | 0.8 | O K |
| 7200 min Winter | 5.560 | 0.045 | 0.0 | 0.1 | 0.1 | 0.8 | O K |
| 8640 min Winter | 5.558 | 0.043 | 0.0 | 0.1 | 0.1 | 0.8 | O K |
| 10080 min Winter | 5.557 | 0.042 | 0.0 | 0.1 | 0.1 | 0.7 | O K |

| Storm Event | Rain (mm/hr) | Flooded Volume (m³) | Discharge Volume (m³) | Time-Peak (mins) |
|------------------|--------------|---------------------|-----------------------|------------------|
| 30 min Winter | 65.075 | 0.0 | 6.6 | 30 |
| 60 min Winter | 40.510 | 0.0 | 8.4 | 48 |
| 120 min Winter | 24.362 | 0.0 | 10.3 | 86 |
| 180 min Winter | 17.855 | 0.0 | 11.4 | 122 |
| 240 min Winter | 14.239 | 0.0 | 12.2 | 158 |
| 360 min Winter | 10.317 | 0.0 | 13.3 | 222 |
| 480 min Winter | 8.210 | 0.0 | 14.1 | 286 |
| 600 min Winter | 6.871 | 0.0 | 14.8 | 346 |
| 720 min Winter | 5.939 | 0.0 | 15.3 | 404 |
| 960 min Winter | 4.714 | 0.0 | 16.3 | 520 |
| 1440 min Winter | 3.400 | 0.0 | 17.6 | 750 |
| 2160 min Winter | 2.448 | 0.0 | 19.0 | 1100 |
| 2880 min Winter | 1.937 | 0.0 | 20.0 | 1468 |
| 4320 min Winter | 1.391 | 0.0 | 21.5 | 2132 |
| 5760 min Winter | 1.099 | 0.0 | 22.5 | 2936 |
| 7200 min Winter | 0.915 | 0.0 | 23.3 | 3672 |
| 8640 min Winter | 0.787 | 0.0 | 23.9 | 4256 |
| 10080 min Winter | 0.693 | 0.0 | 24.5 | 5176 |

| | | |
|--|--|---|
| SIMPSON ASSOCIATES | | Page 3 |
| 4TH FLOOR 43 EAGLE STREET LONDON WC1R 4AT | |  |
| Date 11/03/2022 15:16 File Permeable Paving Design... | Designed by garethcrowther Checked by | |
| XP Solutions | | Source Control 2018.1.1 |

Rainfall Details

| | | | |
|-----------------------|-------------------|-----------------------|-------|
| Rainfall Model | FSR | Winter Storms | Yes |
| Return Period (years) | 100 | Cv (Summer) | 0.750 |
| Region | England and Wales | Cv (Winter) | 0.840 |
| M5-60 (mm) | 20.000 | Shortest Storm (mins) | 15 |
| Ratio R | 0.410 | Longest Storm (mins) | 10080 |
| Summer Storms | Yes | Climate Change % | +0 |

Time Area Diagram

Total Area (ha) 0.027

| Time (mins) | | Area |
|-------------|-----|-------|
| From: | To: | (ha) |
| 0 | 4 | 0.027 |

Summary of Results for 100 year Return Period (+40%)

Half Drain Time : 55 minutes.


| Storm Event | Max Level (m) | Max Depth (m) | Max Infiltration (l/s) | Max Control (l/s) | Max Σ Outflow (l/s) | Max Volume (m ³) | Status |
|------------------|---------------|---------------|------------------------|-------------------|---------------------|------------------------------|--------|
| 15 min Summer | 5.857 | 0.342 | 0.0 | 1.4 | 1.4 | 6.0 | O K |
| 30 min Summer | 5.934 | 0.419 | 0.0 | 1.5 | 1.5 | 7.3 | O K |
| 60 min Summer | 5.975 | 0.460 | 0.0 | 1.6 | 1.6 | 8.1 | O K |
| 120 min Summer | 5.980 | 0.465 | 0.0 | 1.6 | 1.6 | 8.1 | O K |
| 180 min Summer | 5.958 | 0.443 | 0.0 | 1.5 | 1.5 | 7.8 | O K |
| 240 min Summer | 5.929 | 0.414 | 0.0 | 1.5 | 1.5 | 7.3 | O K |
| 360 min Summer | 5.875 | 0.360 | 0.0 | 1.4 | 1.4 | 6.3 | O K |
| 480 min Summer | 5.830 | 0.315 | 0.0 | 1.3 | 1.3 | 5.5 | O K |
| 600 min Summer | 5.792 | 0.277 | 0.0 | 1.2 | 1.2 | 4.9 | O K |
| 720 min Summer | 5.761 | 0.246 | 0.0 | 1.2 | 1.2 | 4.3 | O K |
| 960 min Summer | 5.714 | 0.199 | 0.0 | 1.0 | 1.0 | 3.5 | O K |
| 1440 min Summer | 5.654 | 0.139 | 0.0 | 0.9 | 0.9 | 2.4 | O K |
| 2160 min Summer | 5.609 | 0.094 | 0.0 | 0.7 | 0.7 | 1.6 | O K |
| 2880 min Summer | 5.593 | 0.078 | 0.0 | 0.6 | 0.6 | 1.4 | O K |
| 4320 min Summer | 5.579 | 0.064 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 5760 min Summer | 5.573 | 0.058 | 0.0 | 0.3 | 0.3 | 1.0 | O K |
| 7200 min Summer | 5.569 | 0.054 | 0.0 | 0.3 | 0.3 | 0.9 | O K |
| 8640 min Summer | 5.567 | 0.052 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 10080 min Summer | 5.565 | 0.050 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 15 min Winter | 5.902 | 0.387 | 0.0 | 1.4 | 1.4 | 6.8 | O K |

| Storm Event | Rain (mm/hr) | Flooded Volume (m ³) | Discharge Volume (m ³) | Time-Peak (mins) |
|------------------|--------------|----------------------------------|------------------------------------|------------------|
| 15 min Summer | 139.350 | 0.0 | 6.3 | 17 |
| 30 min Summer | 91.106 | 0.0 | 8.5 | 31 |
| 60 min Summer | 56.713 | 0.0 | 10.7 | 48 |
| 120 min Summer | 34.106 | 0.0 | 13.1 | 82 |
| 180 min Summer | 24.997 | 0.0 | 14.4 | 116 |
| 240 min Summer | 19.934 | 0.0 | 15.4 | 150 |
| 360 min Summer | 14.444 | 0.0 | 16.8 | 216 |
| 480 min Summer | 11.493 | 0.0 | 17.8 | 280 |
| 600 min Summer | 9.620 | 0.0 | 18.7 | 342 |
| 720 min Summer | 8.314 | 0.0 | 19.4 | 404 |
| 960 min Summer | 6.600 | 0.0 | 20.5 | 522 |
| 1440 min Summer | 4.760 | 0.0 | 22.2 | 764 |
| 2160 min Summer | 3.427 | 0.0 | 24.0 | 1108 |
| 2880 min Summer | 2.712 | 0.0 | 25.3 | 1468 |
| 4320 min Summer | 1.948 | 0.0 | 27.1 | 2200 |
| 5760 min Summer | 1.538 | 0.0 | 28.5 | 2936 |
| 7200 min Summer | 1.281 | 0.0 | 29.5 | 3656 |
| 8640 min Summer | 1.102 | 0.0 | 30.4 | 4368 |
| 10080 min Summer | 0.970 | 0.0 | 31.0 | 5128 |
| 15 min Winter | 139.350 | 0.0 | 7.2 | 17 |

Summary of Results for 100 year Return Period (+40%)

| Storm Event | Max Level (m) | Max Depth (m) | Max Infiltration (l/s) | Max Control (l/s) | Max Σ Outflow (l/s) | Max Volume (m³) | Status |
|------------------|---------------|---------------|------------------------|-------------------|---------------------|-----------------|--------|
| 30 min Winter | 5.991 | 0.476 | 0.0 | 1.6 | 1.6 | 8.3 | O K |
| 60 min Winter | 6.036 | 0.521 | 0.0 | 1.7 | 1.7 | 9.1 | O K |
| 120 min Winter | 6.032 | 0.517 | 0.0 | 1.7 | 1.7 | 9.1 | O K |
| 180 min Winter | 5.995 | 0.480 | 0.0 | 1.6 | 1.6 | 8.4 | O K |
| 240 min Winter | 5.952 | 0.437 | 0.0 | 1.5 | 1.5 | 7.7 | O K |
| 360 min Winter | 5.875 | 0.360 | 0.0 | 1.4 | 1.4 | 6.3 | O K |
| 480 min Winter | 5.814 | 0.299 | 0.0 | 1.3 | 1.3 | 5.2 | O K |
| 600 min Winter | 5.766 | 0.251 | 0.0 | 1.2 | 1.2 | 4.4 | O K |
| 720 min Winter | 5.728 | 0.213 | 0.0 | 1.1 | 1.1 | 3.7 | O K |
| 960 min Winter | 5.674 | 0.159 | 0.0 | 0.9 | 0.9 | 2.8 | O K |
| 1440 min Winter | 5.615 | 0.100 | 0.0 | 0.7 | 0.7 | 1.8 | O K |
| 2160 min Winter | 5.588 | 0.073 | 0.0 | 0.5 | 0.5 | 1.3 | O K |
| 2880 min Winter | 5.579 | 0.064 | 0.0 | 0.4 | 0.4 | 1.1 | O K |
| 4320 min Winter | 5.571 | 0.056 | 0.0 | 0.3 | 0.3 | 1.0 | O K |
| 5760 min Winter | 5.567 | 0.052 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 7200 min Winter | 5.564 | 0.049 | 0.0 | 0.2 | 0.2 | 0.9 | O K |
| 8640 min Winter | 5.562 | 0.047 | 0.0 | 0.2 | 0.2 | 0.8 | O K |
| 10080 min Winter | 5.561 | 0.046 | 0.0 | 0.2 | 0.2 | 0.8 | O K |

| Storm Event | Rain (mm/hr) | Flooded Volume (m³) | Discharge Volume (m³) | Time-Peak (mins) |
|------------------|--------------|---------------------|-----------------------|------------------|
| 30 min Winter | 91.106 | 0.0 | 9.6 | 31 |
| 60 min Winter | 56.713 | 0.0 | 12.1 | 52 |
| 120 min Winter | 34.106 | 0.0 | 14.7 | 88 |
| 180 min Winter | 24.997 | 0.0 | 16.3 | 126 |
| 240 min Winter | 19.934 | 0.0 | 17.3 | 162 |
| 360 min Winter | 14.444 | 0.0 | 18.9 | 228 |
| 480 min Winter | 11.493 | 0.0 | 20.1 | 294 |
| 600 min Winter | 9.620 | 0.0 | 21.0 | 356 |
| 720 min Winter | 8.314 | 0.0 | 21.8 | 418 |
| 960 min Winter | 6.600 | 0.0 | 23.1 | 538 |
| 1440 min Winter | 4.760 | 0.0 | 25.0 | 766 |
| 2160 min Winter | 3.427 | 0.0 | 27.0 | 1104 |
| 2880 min Winter | 2.712 | 0.0 | 28.4 | 1464 |
| 4320 min Winter | 1.948 | 0.0 | 30.5 | 2204 |
| 5760 min Winter | 1.538 | 0.0 | 32.1 | 2808 |
| 7200 min Winter | 1.281 | 0.0 | 33.2 | 3744 |
| 8640 min Winter | 1.102 | 0.0 | 34.2 | 4352 |
| 10080 min Winter | 0.970 | 0.0 | 35.0 | 5216 |

| | | |
|--|--|---|
| SIMPSON ASSOCIATES | | Page 3 |
| 4TH FLOOR 43 EAGLE STREET LONDON WC1R 4AT | |  |
| Date 11/03/2022 15:13 File Permeable Paving Design... | Designed by garethcrowther Checked by | |
| XP Solutions | | Source Control 2018.1.1 |

Rainfall Details

| | | | |
|-----------------------|-------------------|-----------------------|-------|
| Rainfall Model | FSR | Winter Storms | Yes |
| Return Period (years) | 100 | Cv (Summer) | 0.750 |
| Region | England and Wales | Cv (Winter) | 0.840 |
| M5-60 (mm) | 20.000 | Shortest Storm (mins) | 15 |
| Ratio R | 0.410 | Longest Storm (mins) | 10080 |
| Summer Storms | Yes | Climate Change % | +40 |

Time Area Diagram

Total Area (ha) 0.027

| Time (mins) | | Area |
|-------------|-----|-------|
| From: | To: | (ha) |
| 0 | 4 | 0.027 |

Henley-On-Thames

8 Friday Street

Henley-on-Thames

Oxfordshire

RG9 1AH

+44 (0)1491 576 22

Gloucester

Unit B10

Elmbridge Court Business
Park

Gloucester

GL3 1JZ

+44 (0)1452 309 727

London

3 Dufferin Avenue

Barbican

London

EC1Y 8PQ

+44 (0)207 253 2626

Online

www.simpsoneng.com

mail@simpsoneng.com