



Sustainable Drainage System Strategy

Site Address

99 Atbara Road
Teddington
TW11 9PA

Client

Jamie and Beverley McDaid

Report Reference

SWDS-2024-000036

Prepared By

STM Environmental Consultants Ltd

Date



21/08/2024



**CONSULTING ENVIRONMENTAL
ENGINEERS AND SCIENTISTS**

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1 Document Control

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|  | Sustainable Drainage System Strategy |  |
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2 Abbreviations

| Abbreviation | Description |
|--------------|---------------------------------------|
| STM | STM Environmental Consultants Limited |
| BGS | British Geological Survey |
| EA | Environment Agency |
| OS | Ordnance Survey of Great Britain |
| FRA | Flood Risk Assessment |
| NPPF | National Planning Policy Framework |
| FWD | Floodline Warning Direct |
| FRMS | Flood Risk Management Strategy |
| LLFA | Lead Local Flood Authority |
| SWMP | Surface Water Management Plan |
| SFRA | Strategic Flood Risk Assessment |
| CDA | Critical Drainage Area |
| SuDS | Sustainable Drainage Systems |
| GWSPZ | Groundwater Source Protection Zone |

3 Disclaimer

This report and any information or advice which it contains, is provided by STM Environmental Consultants Ltd (STM) and is solely for use by Jamie and Beverley McDaid (Client).

STM has exercised such professional skill, care and diligence as may reasonably be expected of a properly qualified and competent consultant when undertaking works of this nature. However, STM gives no warranty, representation or assurance as to the accuracy or completeness of any information, assessments or evaluations presented within this report. STM accepts no liability for the performance of any drainage system based upon the recommendations of this report. Furthermore, STM accepts no liability whatsoever for any loss or damage arising from the interpretation or use of the information contained within this report. Any party using or placing reliance upon any information contained in this report, do so at their own risk.

3.1 Executive Summary

| BACKGROUND | | | | |
|---|--|---------------------------------|--|---|
| Location | 99 Atbara Road, Teddington TW11 9PA Grid reference: 517085, 170948 | | | |
| Site Area | 374m ² | | | |
| <u>Proposed Development</u> | Demolition of the existing residential bungalow and construction of a new 2-storey residential dwelling with a loft space. | | | |
| Current Site and Surrounding Uses | The site is a residential dwelling with associated garden, garage and amenity space. It is located in a mainly residential area, with 2no. sports grounds and a small number of commercial uses within the vicinity. | | | |
| <u>Topography</u> | The ground level at the site ranges from 6.34mAOD (northeast) to 6.93mAOD (southwest). | | | |
| <u>Hydrology</u> | A watercourse connected with the River Thames is present approximately 80m east of the site. The River Thames is located approximately 340m northeast of the site. | | | |
| <u>Geology</u> | BGS information indicates that the superficial deposits at the site consist of Kempton Park Gravel Formation while the bedrock is classified as belonging to the London Clay Formation. | | | |
| <u>Hydrogeology</u> | BGS information indicates that the site is situated upon a Principal superficial and an Unproductive bedrock aquifer. | | | |
| <u>Permeability</u> | BGS information indicates that the superficial deposits are free draining and the bedrock is classified as poorly draining. | | | |
| <u>Infiltration Potential</u> | <p>BGS information indicates that there are opportunities for bespoke infiltration SuDS.</p> <p>Infiltration testing was undertaken on the 10 – 12th June, 2024. TP01 encountered dark brown Top Soil to a depth of 0.3mbgl, becoming wet, light, brown/orange Sandy Clay to a level of 1.1mbgl. Groundwater was not detected.</p> <p>The infiltration rate obtained on site is indicated to be 1.4×10^{-6}m/s in TP01, which is considered to be a moderate rate. However, this rate is insufficient to discharge all surface waters to ground and ensure a suitable half drain down time. As such, a combined system allowing for infiltration and discharge to the public surface water sewer will be required.</p> | | | |
| <u>Fluvial Flood Risk</u> | Medium – the site lies within EA Flood Zones 2 and 3. Further information regarding flood risk to the site is available in FRA – 2023 – 000041. | | | |
| <u>Surface Water Flood Risk</u> | Very Low – The site remains dry during all modelled scenarios. Further information regarding flood risk to the site is available in FRA – 2023 – 000041. | | | |
| <u>Groundwater Flood Risk</u> | Low - the EA mapping indicates that there is potential for groundwater flooding to occur for properties below ground surface. Groundwater is likely to be less than 3mbgl for at least part of the year. | | | |
| <u>Existing and Proposed Site Layout</u> | Ground Cover | Existing (m²) | Proposed (m²) (Without SuDS) | Proposed (m²) (With SuDS) |
| | Buildings | 107 | 118 | 118 |
| | Driveways/Patio (Impermeable) | 145 | 165 | 96 |
| | Driveways/Patio (Permeable) | 0 | 0 | 69 |
| | Gardens/ Soft landscaping | 122 | 91 | 91 |
| | Total Impermeable Area | 252 | 283 | 214 |

| | | | |
|--|--|--------------------------------|---|
| Changes in Impermeable | Without SuDS, the proposed development would increase the impermeable area of the site by 31m ² (8.3%) and therefore increase the post development runoff rate and volume. With SuDS, the proposed development would decrease the impermeable area by 38m ² (10.2%). | | |
| PROPOSED SUDS | | | |
| <u>Run-Off Rates</u> | Greenfield (GF) (l/s) | MRM Pre - Development (l/s) | MRM Post Development Without SuDS (l/s) |
| Qbar | 0.06 | - | - |
| 1 in 1 | 0.05 | 3.7 | 4.2 |
| 1 in 30 | 0.13 | 8.8 | 9.8 |
| 1 in 100 | 0.18 | 11.1 | 12.4 |
| 1 in 100 + CC (40%) | 0.27 | - | - |
| <u>SuDS Target Requirement</u> | <p>As the development is taking place on a previously developed site, the non-statutory technical standards for sustainable drainage systems S3 (peak flow) and S5 and S6 (volume controls) apply.</p> <p>The proposal should aim to achieve the greenfield runoff rate of 0.06/s for all storm events. However, achieving a discharge a rate this low may not be practical, and may give rise to blockages in the proposed system.</p> | | |
| <u>Drainage Hierarchy</u> | The proposed development cannot discharge to a watercourse. The proposal will allow for infiltration and controlled discharge to the public surface water sewer to ensure suitable half drain down times are achieved. | | |
| <u>Storage Required to meet Planning Requirement</u> | <p>To achieve a discharge rate of 1.0 l/s post development, 8 - 12m³ of storm water attenuation is required.</p> <p>When not including the permeable paving as part of the impermeable catchment area, 5 – 8m³ of storm water attenuation is required.</p> | | |
| <u>SuDS Strategy</u> | <p>The proposal will introduce permeable paving, a rainwater butt, geocellular attenuation within the rear garden and front of the property.</p> <p>The combination of the SuDS measures introduced will provide 200L rainwater re-use and 5.8m³ of attenuation.</p> <p>The SuDS strategy introduced will implement a protected Orifice Control Chamber as to limit the discharge to 1.0 l/s for all storm events into the receiving surface water sewer.</p> | | |
| Conclusion | With the proposed SuDS mitigation measures which have been outline introduced into the scheme, we believe that the proposed development will reduce local flood risk and therefore be in compliance with the LLFA's current planning policy and the NPPF. | | |

4 Introduction

STM Environmental Consultants Limited have been appointed by Jamie and Beverley McDaid to undertake a Sustainable Drainage System (SuDS) Strategy for a proposed development at 99 Atbara Road, Teddington TW11 9PA.

4.1 Proposed Development

The SuDS report is required to support a planning application for the demolition of the existing residential bungalow and construction of a new 2-storey residential dwelling with a loft space. Copies of the development plans are presented in [Appendix 1](#).

4.2 Report Aims and Objectives

This report sets out the proposed drainage strategy that will be employed in the designs to meet the requirements of the planning condition and the National Planning Policy Framework.

4.3 Legislative and Policy Context

4.3.1 Legislative Context

Section H3 of the Building Regulations 2010 requires that adequate provision is made for rainwater to be carried from the building roofs and paved areas, and be preferentially discharged to soakaways or some other adequate infiltration system. Where that is not reasonably practicable, a watercourse; or sewer can be used.

The Flood and Water Management Act was introduced in 2010. The Act defines the role of lead local flood authority (LLFA) for an area. All LLFA are required to develop, maintain, apply and monitor a strategy for local flood risk management in its area, called “local flood risk management strategy”.

Alongside the Act, Flood Risk Regulations (2009) outline the roles and responsibilities of the various authorities, which include preparing Flood Risk Management Plans and identifying how significant flood risks are to be mitigated.

4.3.2 Policy Context

The National Planning Policy Framework (NPPF) sets out the Government's economic, environmental and social planning policies for England. The policies set out in this framework apply to the preparation of local and neighbourhood plans and to decisions on planning applications.

Paragraph 173 of the National Planning Policy Framework (NPPF) states that:

When determining any planning applications, local planning authorities should ensure that flood risk is not increased elsewhere. Where appropriate, applications should be supported by a site-specific flood-risk assessment (See Note 1)
Development should only be allowed in areas at risk of flooding where, in the light of this assessment (and the sequential and exception tests, as applicable) it can be demonstrated that:

- within the site, the most vulnerable development is located in areas of lowest flood risk unless there are overriding reasons to prefer a different location
- the development is appropriately flood resistant and resilient such that, in the event of a flood, it could be quickly brought back into use without significant refurbishment;
- it incorporates sustainable drainage systems, unless there is clear evidence that this would be inappropriate;
- any residual risk can be safely managed; and
- safe access and escape routes are included where appropriate, as part of an agreed emergency plan.

Applications for some minor development and changes of use (See Note.2) should not be subject to the sequential or exception tests but should still meet the requirements for site-specific flood risk assessments set out in (See Note 1).

Paragraph 175 states that:

Major developments should incorporate sustainable drainage systems unless there is clear evidence that this would be inappropriate. The systems used should:

- take account of advice from the lead local flood authority;

- have appropriate proposed minimum operational standards;
- have maintenance arrangements in place to ensure an acceptable standard of operation for the lifetime of the development; and
- where possible, provide multifunctional benefits.

A major development is defined as:

- a residential development: 10 dwellings or more or residential development with a site area of 0.5 hectares or more where the number of dwellings is not yet known
- a non-residential development: provision of a building or buildings where the total floor space to be created is 1000 square metres or more or where the floor area is not yet known, a site area of 1 hectare or more.

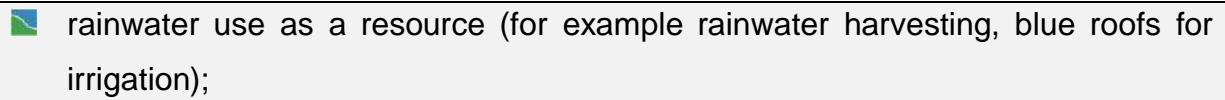
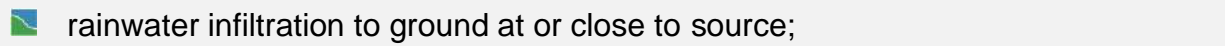
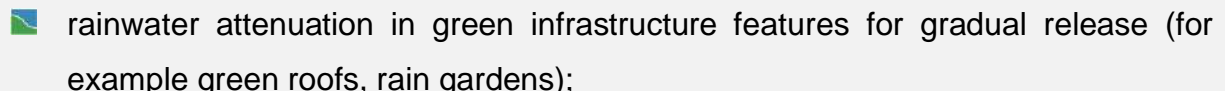
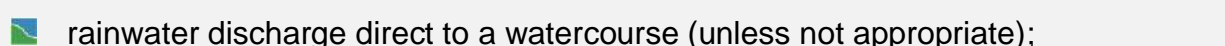

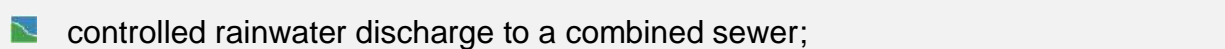
Note. 1 - A site-specific flood risk assessment should be provided for all development in Flood Zones 2 and 3. In Flood Zone 1, an assessment should accompany all proposals involving: sites of 1 hectare or more; land which has been identified by the Environment Agency as having critical drainage problems; land identified in a strategic flood risk assessment as being at increased flood risk in future; or land that may be subject to other sources of flooding, where its development would introduce a more vulnerable use.

Note. 2 - This includes householder development, small non-residential extensions (with a footprint of less than 250m²) and changes of use; except for changes of use to a caravan, camping or chalet site, or to a mobile home or park home site, where the sequential and exception tests should be applied as appropriate.

4.3.3 The London Plan - Policy SI 13 Sustainable drainage

Lead Local Flood Authorities should identify – through their Local Flood Risk Management Strategies and Surface Water Management Plans – areas where there are particular surface water management issues and aim to reduce these risks. Increases in surface water run-off outside these areas also need to be identified and addressed.

Development proposals should aim to achieve greenfield run-off rates and ensure that surface water run-off is managed as close to its source as possible. There should also be a preference for green over grey features, in line with the following drainage hierarchy:

- 
- 
- 
- 
- 
- 

Development proposals for impermeable surfacing should normally be resisted unless they can be shown to be unavoidable, including on small surfaces such as front gardens and driveways.

Drainage should be designed and implemented in ways that promote multiple benefits including increased water use efficiency, improved water quality, and enhanced biodiversity, urban greening, amenity and recreation.

4.4 LLFA Planning Policy - Richmond upon Thames

4.4.1 Policy LP 21 - Flood Risk and Sustainable Drainage

“All developments should avoid, or minimise, contributing to all sources of flooding, including fluvial, tidal, surface water, groundwater and flooding from sewers, taking account of climate change and without increasing flood risk elsewhere. Unacceptable developments and land uses will be refused in line with national policy and guidance [and] the Council's Strategic Flood Risk Assessment (SFRA)”.

Sustainable drainage

The Council will require the use of Sustainable Drainage Systems (SuDS) in all development proposals. Applicants will have to demonstrate that their proposal complies with the following:

1. A reduction in surface water discharge to greenfield run-off rates wherever feasible.
2. Where greenfield run-off rates are not feasible, this will need to be demonstrated by the applicant, and in such instances, the minimum requirement is to achieve at least a 50% attenuation of the site's surface water runoff at peak times based on the levels existing prior to the development.

Also relevant is policy S1 12 of the London Plan (2020) which outlines Flood Risk Management, it states that:

- Current and expected flood risk from all sources across London should be managed in a sustainable and cost-effective way in collaboration with the Environment Agency, the Lead Local Flood Authorities, developers and infrastructure providers;
- Development Plans should use the Mayor's Regional Flood Risk Appraisal and their Strategic Flood Risk Assessment as well as Local Flood Risk Management Strategies, where necessary, to identify areas where particular and cumulative flood risk issues exist and develop actions and policy approaches aimed at reducing these risks. Boroughs should cooperate and jointly address cross-boundary flood risk issues including with authorities outside London;
- Development proposals should ensure that flood risk is minimised and mitigated, and that residual risk is addressed. This should include, where possible, making space for water and aiming for development to be set back from the banks of watercourses;
- Developments Plans and development proposals should contribute to the delivery of the measures set out in Thames Estuary 2100 Plan. The Mayor will work with the Environment Agency and relevant local planning authorities, including authorities outside London, to safeguard an appropriate location for a new Thames Barrier;
- Development proposals for utility services should be designed to remain operational under flood conditions and buildings should be designed for quick recovery following a flood.

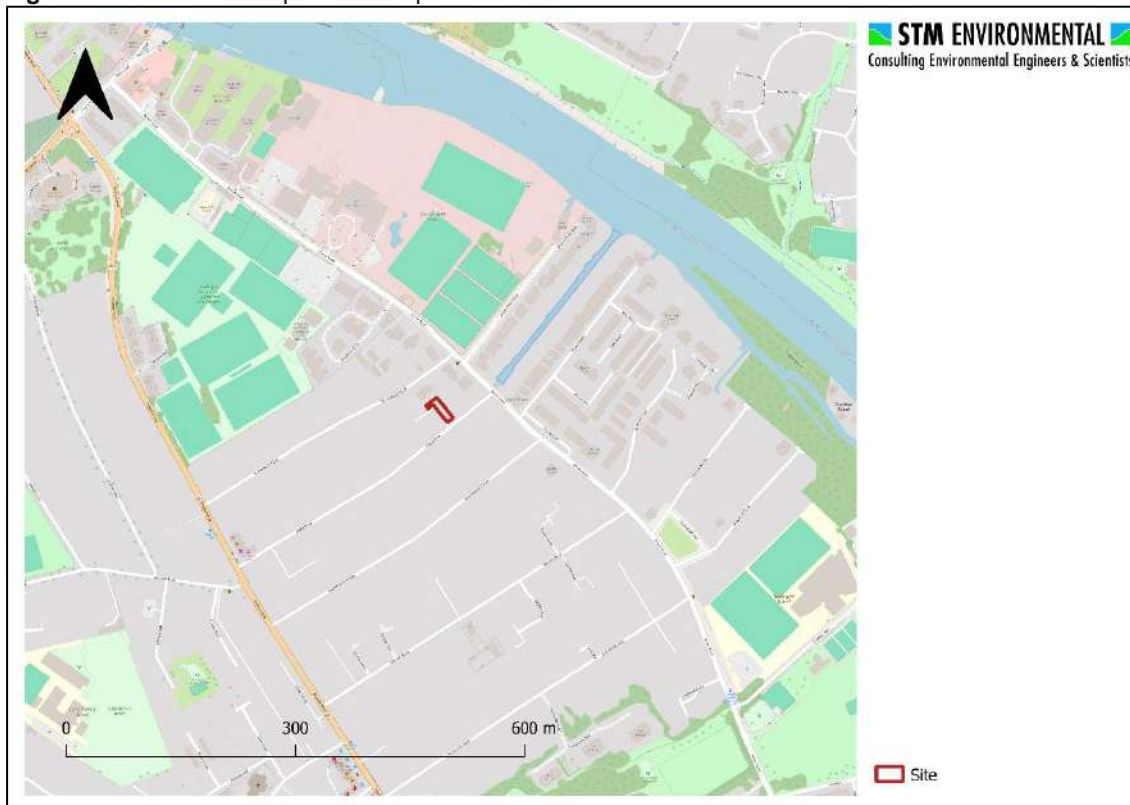
5 Site Characteristics

5.1 Location and Area

The site is centred at national grid reference 517085, 170948 and has an area of 374m².

It falls within the jurisdiction of the London Borough of Richmond upon Thames in terms of the planning consultation process on flood risk and surface water management. Figure 1 provides the site location map and aerial imagery.

Figure 1: Site location map and aerial photo



5.2 Current Site and Surrounding Uses

The site is currently used a residential dwelling. It is located in a mainly residential area, with 2no. sports grounds and a small number of commercial uses within the vicinity.

5.3 Site Topography

The mapping provided in [Appendix 2](#) shows the 1m LiDAR DTM (2022) ground elevations within the site. A topographical survey is also available in Appendix 2.

The ground level at the site ranges from 6.34mAOD in the soft landscaping in the rear garden (northeast) to 6.93mAOD at the roadway (southwest). The surrounding area gradually rises in topography from the lowest elevation, where the River Thames is located, in the east.

5.4 Site Investigation

Infiltration testing was undertaken on the 10th to 12th June, 2024. A trial pit was excavated to a depth of 1.1mbgl for undertaking infiltration testing in accordance with BRE DG 365.

TP01 encountered dark brown Top Soil to a depth of 0.3mbgl, becoming wet, light, brown/orange Sandy Clay to a level of 1.1mbgl. Groundwater was not encounter.

The trial pit was rapidly filled with water from a 1.2m³ water bowser. The trial pit was left to drain for a 24 - hour period or until nearly empty. The water level was continuously monitored using a water level logger. The water level achieved within the trial pit was used as the effective storage depth.

The data from the testing was used to calculate the infiltration rate. The infiltration rate was calculated to be 1.4×10^{-6} m/s in TP01. This is classified as a moderate rate of infiltration.

Full details including photos, graphs, location map and results of the infiltration testing are available in [Appendix 6](#).

5.5 Flood Risk Summary

The overall flood risk to the site is considered to be Medium, with the main source of flooding being the River Thames.

Further information regarding flood risk to the site is available in FRA – 2023 – 000041.

The flood risk maps area available in [Appendix 3](#)

5.6 Existing Surface Water Drainage Features

Drainage plans showing the existing surface water drainage system at the site are presented in [Appendix 5](#).

A utility search was undertaken which identified Thames Water as the local sewage undertaker.

Table 1: Asset Information

| Asset ID | Asset Type | Distance (m) / Location | Manhole Cover Level (mAOD)* | Manhole Invert Level (mAOD) | Depth (m) |
|----------|------------|-------------------------|-----------------------------|-----------------------------|-----------|
| 0908 | SW | 13m SW on Atbara Rd | 7.09 | N/A | N/A |
| 1908 | SW | 63m NE on Broom Rd | 6.27 | N/A | N/A |
| 0806 | SW | 111m SE on Atbara Rd | 7.40 | N/A | N/A |

*Cover Levels taken from DTM LiDAR mapping

A CON29DW Drainage & Water Enquiry was undertaken, confirming the existing surface water connection, and is available in [Appendix 5](#).

6 Hydrological Run-off Assessment

To minimise the impact of the new development on local flood risk, the NPPF requires that the water drainage arrangements for any development site are that the volumes and peak flow rates leaving the site post-development are improved upon those of the existing conditions. The following run-off assessment predicts the Greenfield, pre- and post-development run-off rates and provides the required SuDS necessary for complying with the relevant planning policies.

6.1 Existing and Proposed Ground Cover

Table 2: Breakdown of Ground Cover in the Proposed Development

| Ground Cover | Existing Development Area | | Proposed Development Area | | Difference (m ²) |
|------------------|---------------------------|------------|---------------------------|------------|------------------------------|
| | m ² | % | m ² | % | |
| Buildings | 107 | 28.6 | 118 | 31.6 | 11 |
| Hard Standing | 145 | 38.8 | 165 | 44.1 | 20 |
| Soft landscaping | 122 | 32.6 | 91 | 24.3 | 31 |
| Total | 374 | 100 | 374 | 100 | |

Table 3: Summary of Permeable and Impermeable Areas

| | Impermeable Area | | Permeable Area | | Total Area |
|---------------|------------------|------|----------------|------|----------------|
| | m ² | % | m ² | % | m ² |
| Existing Site | 252 | 67.4 | 122 | 32.6 | 374 |
| Proposed Site | 283 | 75.7 | 91 | 24.3 | 374 |
| Difference | 31 | 8.3 | -31 | -8.3 | |

The proposed development increases the impermeable area of the site by 8.3% to 31m². As such this will have a negative impact on the runoff rate without the introduction of SuDS.

6.2 Peak Flow Control

With regard to peak flow control, the non-statutory technical standards for sustainable drainage systems state that:

■ S3 For developments which were previously developed, the peak runoff rate from the development to any drain, sewer or surface water body for the 1 in 1 year rainfall event and the 1 in 100 year rainfall event must be as close as reasonably practicable to the greenfield runoff rate from the development for the same rainfall event, but should never exceed the rate of discharge from the development prior to redevelopment for that event.

The London Plan SI.13 states that development proposals should aim to achieve greenfield run-off rates and ensure that surface water run-off is managed as close to its source as possible. The London Plan Sustainable Design and Construction SPG (section 3.4.10) states that all developments on Greenfield sites must maintain Greenfield runoff rates. On previously developed sites, runoff rates should not be more than three times the calculated Greenfield rate.

6.3 Volume Control Requirements

With regard to volume control, the non-statutory technical standards for sustainable drainage systems state that:

- S5 Where reasonably practicable, for developments which have been previously developed, the runoff volume from the development to any highway drain, sewer or surface water body in the 1 in 100 year, 6 hour rainfall event must be constrained to a value as close as is reasonably practicable to the greenfield runoff volume for the same event, but should never exceed the runoff volume from the development site prior to redevelopment for that event.
- S6 Where it is not reasonably practicable to constrain the volume of runoff to any drain, sewer or surface water body in accordance with S4 or S5 above, the runoff volume must be discharged at a rate that does not adversely affect flood risk.

6.4 Run-off and Storage Calculations

The IH124 & MRM methods were applied to calculate the Greenfield, pre and post-development run-off rates including allowances for climate change. The full calculations and results are presented in [Appendix 4](#). The table below gives a summary of the results:

Table 4: Calculation of post-development run-off rates for the site.

| | Greenfield (l/s) | Pre - Development (l/s) | Post Development (l/s) |
|----------------------|---------------------|----------------------------|---------------------------|
| Qbar | 0.06 | 0.15 | 0.16 |
| 1 in 1 | 0.05 | 0.13 | 0.14 |
| 1 in 30 | 0.13 | 0.35 | 0.37 |
| 1 in 100 | 0.18 | 0.48 | 0.52 |
| 1 in 100 + CC | 0.27 | 0.71 | 0.77 |

Table 5: Modified Rational Method (MRM)

| | Pre – Development (l/s) | Pre - Development No SuDS (l/s) |
|-----------------|----------------------------|------------------------------------|
| 1 in 1 | 3.7 | 4.2 |
| 1 in 30 | 8.8 | 9.8 |
| 1 in 100 | 11.1 | 12.4 |

As the development is taking place on a previously developed site S3 (peak flow) and S5 and S6 (volume controls) apply.

The Qbar (0.06 l/s) for the greenfield runoff rate should be the aim for the post-development scenario. However, achieving a discharge a rate this low may not be practical, and may give rise to blockages in the proposed system.

The storage volume required to achieve the 1.0 l/s discharge rate for all storm events, is estimated to be up to **8 - 12m³**.







When taking into consideration the installation of permeable paving, in place of hardstanding, the storm water attenuation volume reduces to **5 – 8m³**.

Screenshots of the quick storage estimate and variables are available [Appendix 4](#).

7 SuDS

7.1 SuDS Hierarchy

The SuDS Hierarchy sets out the preferred method of selecting which Sustainable Drainage System should be used.

-  rainwater use as a resource (for example rainwater harvesting, blue roofs for irrigation);
-  rainwater infiltration to ground at or close to source;
-  rainwater attenuation in green infrastructure features for gradual release (for example green roofs, rain gardens);
-  rainwater discharge direct to a watercourse (unless not appropriate);
-  controlled rainwater discharge to a surface water sewer or drain;
-  controlled rainwater discharge to a combined sewer;

The table outlined on the page below summarises the available SuDS, there potential suitability and the benefits.

7.2 Drainage Hierarchy Discussion

7.2.1 Rainwater Harvesting

The development has good potential to provide rainwater harvesting. As such, this is recommended in the form of rainwater butts.

7.2.2 Green, Blue or Brown Roofs

Based on the proposed roof design, which include pitched roofs, the use of alternative roofing is not deemed to be suitable.

7.2.3 Infiltration To Ground

On site infiltration testing was undertaken. The data from the testing was used to calculate the infiltration rate. The infiltration rate was calculated to be 1.4×10^{-6} m/s in TP01. This is classified as a moderate rate of infiltration.

Based on these findings, infiltration SuDS methods are considered to be partially suitable for the site. The discharge rate achieved cannot ensure suitable half drain down times within 24 hours, so an alternative discharge point will be required.

7.2.4 Permeable Surfaces and Filter Drains

32% of the development will consist of outdoor space and patios, which can be formed from alternative permeable surfaces. On site infiltration has been shown to be successful, but is too low to accommodate additional inflow areas. As such the permeable surfaces may discharge directly to ground and will not be included in the total positive catchment area.

7.3 Appraisal of Potential SuDS Options

7.3.1 SuDS Options

Table 6: SuDS Appraisal; Feasibility of various SuDS and the potential uses on site.

| Key | H | M | L | Y | ? | N | N/A | Flow Rate Control / Events | | | Site Potential | Included | Discussion / Details | Potential Storage Provided | Potential Storage Provided |
|--------------------------|----------------------------|--------|------------|-----|-------|----|----------------|----------------------------|---------------|-----------|----------------|----------|--|----------------------------|----------------------------|
| | High Impact | Medium | Low Impact | Yes | Maybe | No | Not Applicable | 1-2 Years | 10 - 30 Years | 100 Years | | | | | |
| Source Control Measure | Green / Brown Roof | NA | NA | NA | NA | H | H | H | H | L | N | N | Poorly compatible with proposed; | 0 | 0 |
| | Rain Water harvesting | M | L | L | L | NA | M | M | H | L | Y | Y | Good compatibility - Rain Water Butts | 200L | 200L |
| Infiltration Methods | Infiltration trench | H | H | H | M | H | H | H | H | L | N | N | Limited Infiltration | 0 | 0 |
| | Permeable Pavement | H | H | H | H | H | H | H | H | H | Y | Y | Limited Space Available for Paving to be Useful. Will not act as impermeable catchment, and will act as conveyance route | 0 | 0 |
| | Infiltration basin | H | H | H | M | H | H | H | H | H | N | N | Limited Space | 0 | 0 |
| | Soakaway | H | H | H | M | H | H | H | H | L | N | N | Limited Infiltration | 0 | 0 |
| Filtration | Filtration Surface sand | H | H | H | M | H | L | H | H | L | N | N | Limited Space | 0 | 0 |
| | Sub-surface sand filter | H | H | H | M | H | L | H | H | L | N | N | Limited Space | 0 | 0 |
| | Perimeter sand filter | H | H | H | M | H | L | H | H | L | N | N | Limited Space | 0 | 0 |
| | Bioretention/filter strips | H | H | H | M | H | L | H | H | L | Y | N | Partially Suitable through SuDS Planters | 0 | 0 |
| | Filter trench | H | H | H | M | H | L | H | H | L | N | N | Limited Space | 0 | 0 |
| Channels Features (Open) | Open channels Conveyance | H | M | M | M | H | M | H | H | H | N | N | Limited Space | 0 | 0 |
| | Enhanced dry swale | H | H | H | M | H | M | H | H | H | N | N | Limited Space | 0 | 0 |
| | Enhanced wet swale | H | H | M | H | H | L | H | H | H | N | N | Limited Space | 0 | 0 |
| Wet SuDS | Wetland Shallow wetland | H | M | H | M | H | L | H | M | L | N | N | Limited Space | 0 | 0 |
| | Extended detention wetland | H | M | H | M | H | L | H | M | L | N | N | Limited Space | 0 | 0 |
| | Pond / wetland | H | M | H | M | H | L | H | M | L | N | N | Limited Space | 0 | 0 |
| | Pocket wetland | H | M | H | M | H | L | H | M | L | N | N | Limited Space | 0 | 0 |
| | Submerged gravel wetland | H | M | H | M | H | L | H | M | L | N | N | Limited Space | 0 | 0 |
| | Wetland channel | H | M | H | M | H | L | H | M | L | N | N | Limited Space | 0 | 0 |
| Retention | Retention pond | H | M | M | M | H | L | H | H | H | N | N | Limited Space | 0 | 0 |
| Detention | Detention basin | M | M | L | L | L | L | H | H | H | N | N | Limited Space | 0 | 0 |
| Tank Storage | Sub-surface storage (Tank) | L | L | L | L | L | L | H | H | H | Y | Y | Good Compatibility | 5.8 | 5.8 |
| | | | | | | | | | | | | | | Total | 5.8 |

7.4 SuDS Strategy

7.4.1 SuDS Options

The proposal will introduce a rainwater butt, permeable paving and Geocellular attenuation storage.

The SuDS strategy introduced will implement an protected Orifice Control Chamber, to limit the discharge to 1.0 l/s, during all storm events into the receiving surface water sewer. The combination of the SuDS measures introduced will provide 5.8m³ of attenuation; the details are outline in the table below.

Table 7: Proposed SuDS

| Option A | | | |
|---------------|---------------------------------|-------------------------------------|--|
| Location | Proposed Area (m ²) | SuDS Option | Estimated Storage Provided (m ³) |
| Rear Garden | - | Rainwater Butt | 200L |
| Rear Garden | 20 | 0.25m thick Geocellular Attenuation | 4.8 |
| Front of Site | 2 | 0.5m thick Geocellular Attenuation | 1.0 |
| Total | | | 5.8 |

The drainage layout, model sections and model results are available in [Appendix 7](#)

The descriptions of the proposed SuDS and how they interact with the different features is outlined below.

7.4.2 Rainwater Butt

1no. Rainwater harvesting Butt (200 litre) will be fitted to the rear garden downpipe to allow for rainwater re-use within the garden.

Excess storm water will discharge into the geocellular attenuation structure, feeding into the attenuation once at capacity.

7.4.3 Geocellular Attenuation

The geocellular storage will be placed below the patio at the front of the property, and below the patio within the rear garden.

The front structure will cover a total area of 2m² with a thickness of 0.5m. The rear structure will cover a total area of 20m² with a thickness of 0.25m. The geocellular storage crates ([AquaCell Drainage Crates](#) or similar) will have a porosity of 95% and will be stacked together to create the desired storage volume 5.8m³.

7.4.4 Surface Water Discharge Points

The surface water will discharge via the existing surface water connection into the public sewer network, as discussed in [Section 5.6](#).

7.4.5 Treatment of Run-off

Treatment of roof water runoff will be provided through the provision of the permeable paving, rainwater butt and the inspection chamber sumps to intercept gross solids and sediment; guidance will be provided to the developer on appropriate maintenance requirements including regular cleaning of gullies.

7.4.6 Exceedance Flows

The ground level at the site ranges from 6.34mAOD (northeast) to 6.93mAOD (southwest).





The elevation review of the LIDAR 1m DTM Mapping indicates that in the event of exceedance on the site upon completion, overland flows will be retained within the soft landscaping on site, away from the building ensuring safe access and egress can be maintained during such an event. It should be noted that CFS will allow for the excavation of land to the rear of the site, providing a substantial area for storage within the soft landscaping.

7.5 Maintenance and Adoption of SuDS







All SuDS features will be properly installed by competent persons. They will be maintained regularly to ensure that their design capacity and attenuation characteristics provide the required storage volume.

Landscaping and adjacent areas will be designed such that they do not cause soil, mulch and other materials to be washed onto the permeable surfaces and into drains causing clogging.



Owners of the properties/persons responsible for maintenance of SuDS components will be provided with operation and maintenance manuals which will include information such as:

-  the location of SuDS components;
-  an explanation of design intent and objective of the SuDS;
-  the requirements for regular and occasional inspection and maintenance;
-  visual indicators that may trigger maintenance.

Regular maintenance of SuDS components is relatively straightforward with the main tasks consisting of:

-  Regular visual inspections – checking inlets are not blocked and verifying that clogging has not occurred;
-  Litter and debris removal;
-  Grass cutting;
-  Preventive sweeping;
-  Weeding and invasive plant control;
-  Oil and stain removal.

Occasional maintenance activities to ensure the long-term performance of the SuDS features include:

-  Sediment removal
-  Vegetation and plant replacement

These simple measures will ensure that the storage capacity of the system is maintained and that the need for reconstruction and replacement of components is minimised.

Further details on SuDS maintenance measures that will be employed at the site can be found in [Appendix 8](#).

8 Conclusion and Recommendations

With the proposed SuDS mitigation measures in place, it is considered that the proposed development will reduce local flood risk and enhance the local environment and will therefore be in compliance with the LLFA's current planning policy and the NPPF.

9 References

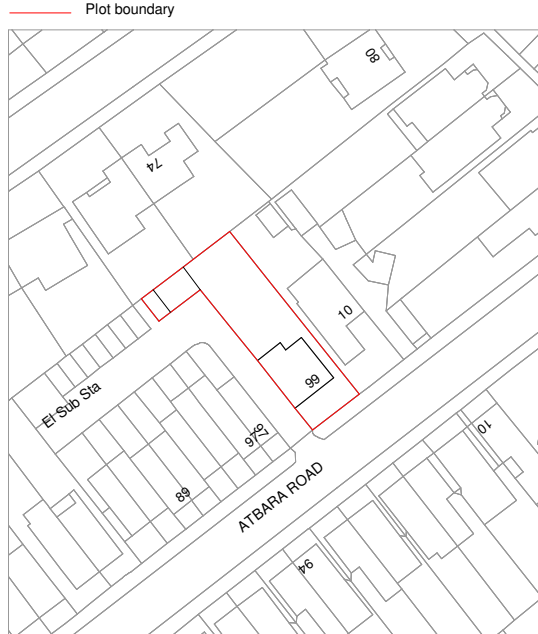
1. Communities and Local Government - National Planning Policy Framework NPPF, 2019.
2. The London Plan – The Spatial Development Strategy for Greater London - March 2021
3. CIRIA, Defra, Environment Agency – UK SuDS Manual, 2015.
4. Local Plan, London Borough of Richmond upon Thames, 2018.
5. Sustainable drainage systems - <https://new.enfield.gov.uk/services/planning/sustainable-drainage-systems/> - Accessed Nov 2023.

10 Appendices

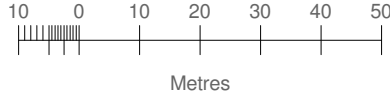
10.1 Appendix 1 – Development Plans & Photos

10.1.1 Development Plans

PDF to follow this page.



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Location Map

1 : 1250



EXTENSION PLANS

Extension Plans. Ealing Cross, 85 Uxbridge Rd, London W5 5BW

99 Atbara Road,
Teddington
TW11 9PA

PROJECT ADDRESS:

Jamie & Beverley McDaid

CLIENT:

Date: 12.05.2023

Scale (@ A4) 1:100

Rev. Date

Rev.

Drawn by: GB

AR-R00-EX-101

PROJECT:

New 4 Bed House

DRAWING TITLE:

LOCATION MAP

Checked by:

DRAWING NUMBER:

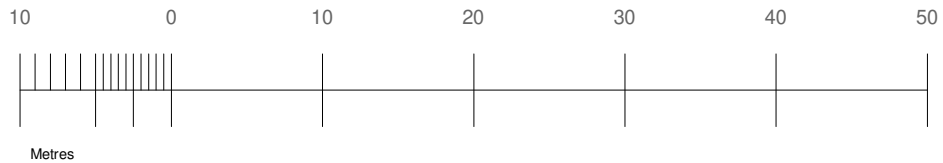



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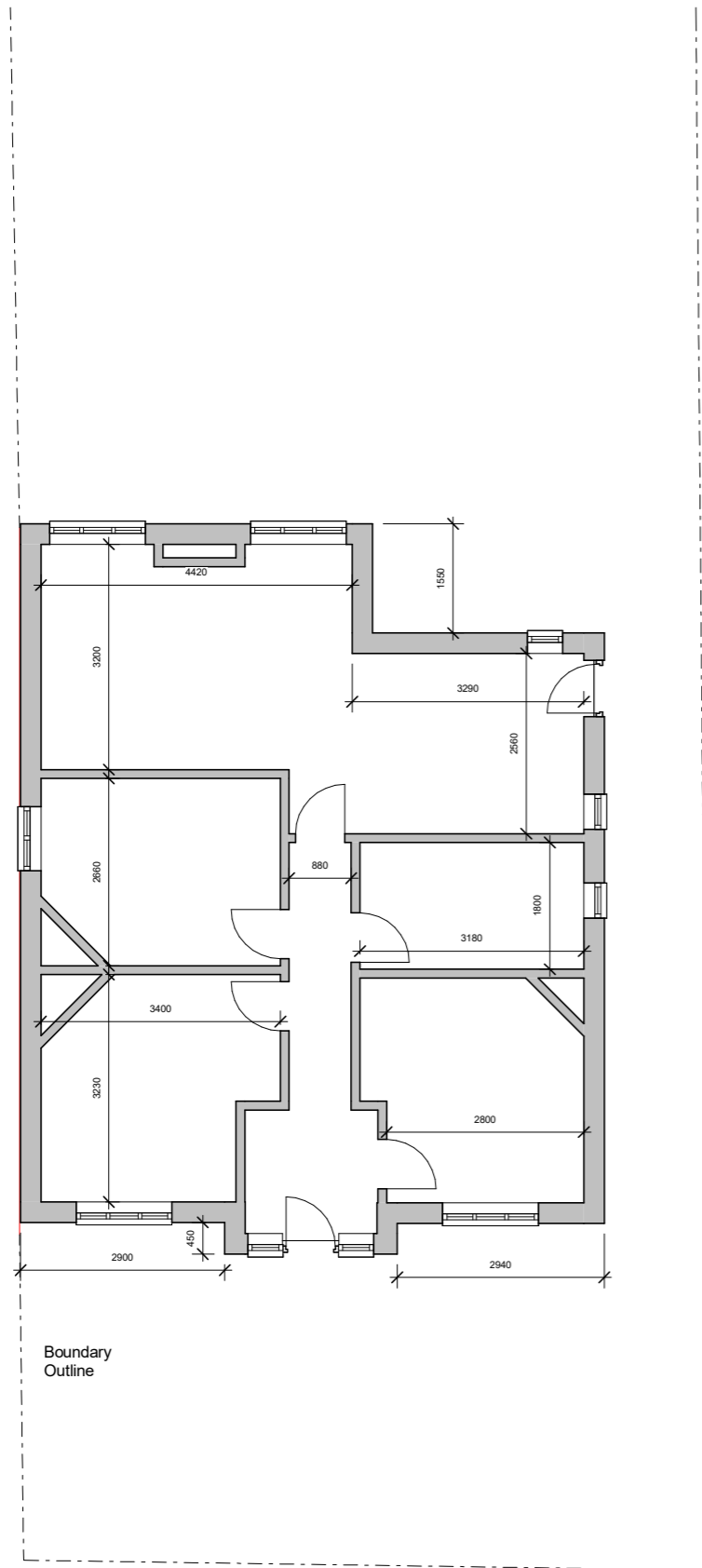
Development
 Property boundary

Site Plan

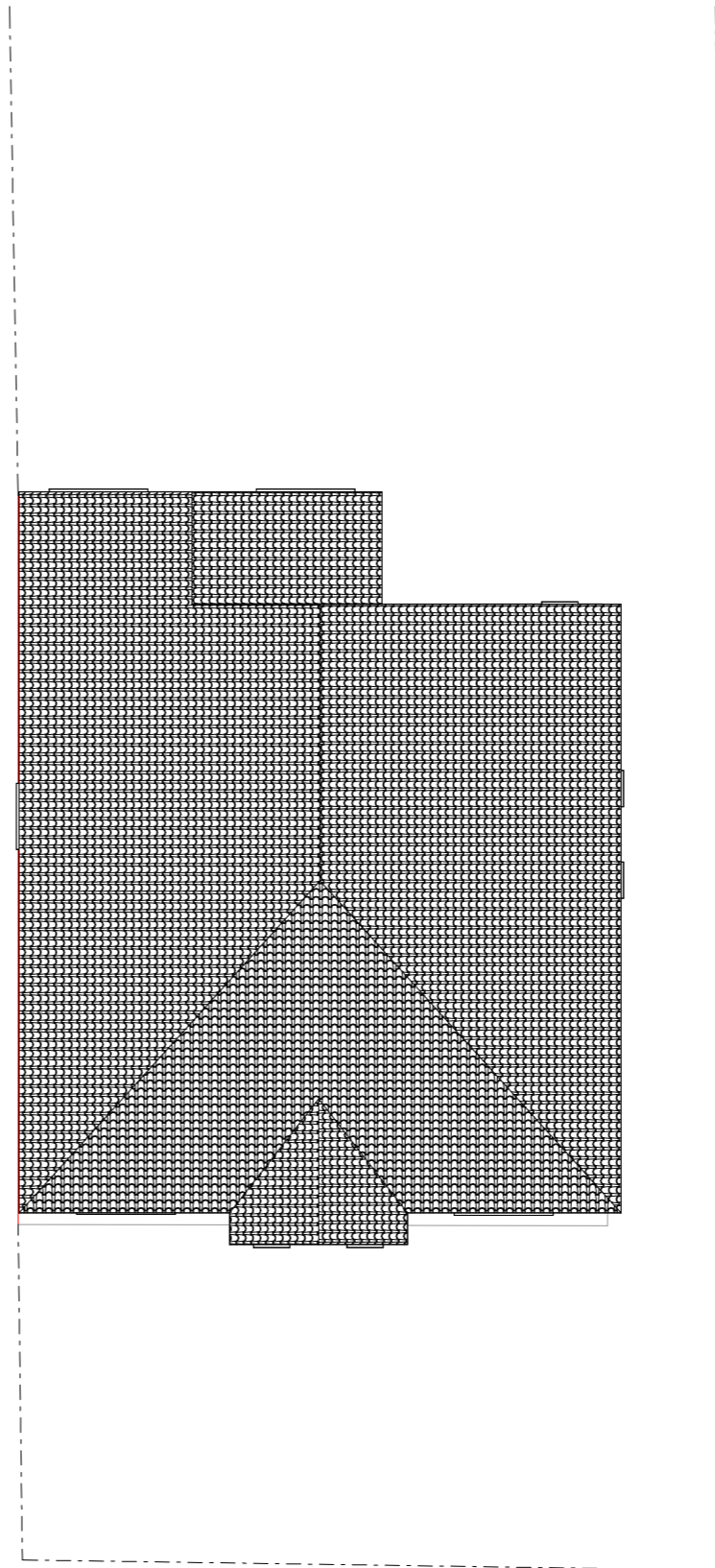
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| | PROJECT ADDRESS: | 22/09/2023 Date: | Scale (@ A4) | Rev. Date | Rev. |
| PROJECT: New 4 Bed House | DRAWING TITLE: SITE PLAN | Drawn by: LG | AR-R00-PR-101 | | |
| | DRAWING TITLE: | Checked by: JH | DRAWING NUMBER: | | |



GF Lvl
1 : 100



ROOF PLAN
1 : 100



PROGRAMME:

REVISION NOTES:

| REV: | DATE: | DESCRIPTION: |
|------|-------|--------------|
|------|-------|--------------|

GENERAL NOTES:

1. All Dimensions are in millimetres unless otherwise stated
2. All work to be carried out in accordance with the current edition of the building regulations 1991 (including amendments) and all relevant british standards/codes of practice.
3. The Contractor is responsible for the correct setting out of the works on site, all dimensions to be checked prior to fabrication of materials and commencement of works.
4. This Drawing is to be read in conjunction with all relevant drawings and specifications
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6. Steels imbedded into ceiling may be charged additionally by your contractor
7. All proposed materials are to be similar in appearance to that of the existing house, unless otherwise
8. Skylights mustn't protrude past the roof slope by more than 150mm
9. Glazing which exceeds 25% of the added floor area will result in extra charges for S.A.P Calculations



Extension Plans. 16 Shakespeare Road W7 1LR

CLIENT: Jamie & Beverley McDaid

PROJECT: New 4 Bed House

PROJECT ADDRESS: 99 Atbara Road,
Teddington
TW11 9PA

DRAWING TITLE: EXISTING FLOOR PLANS

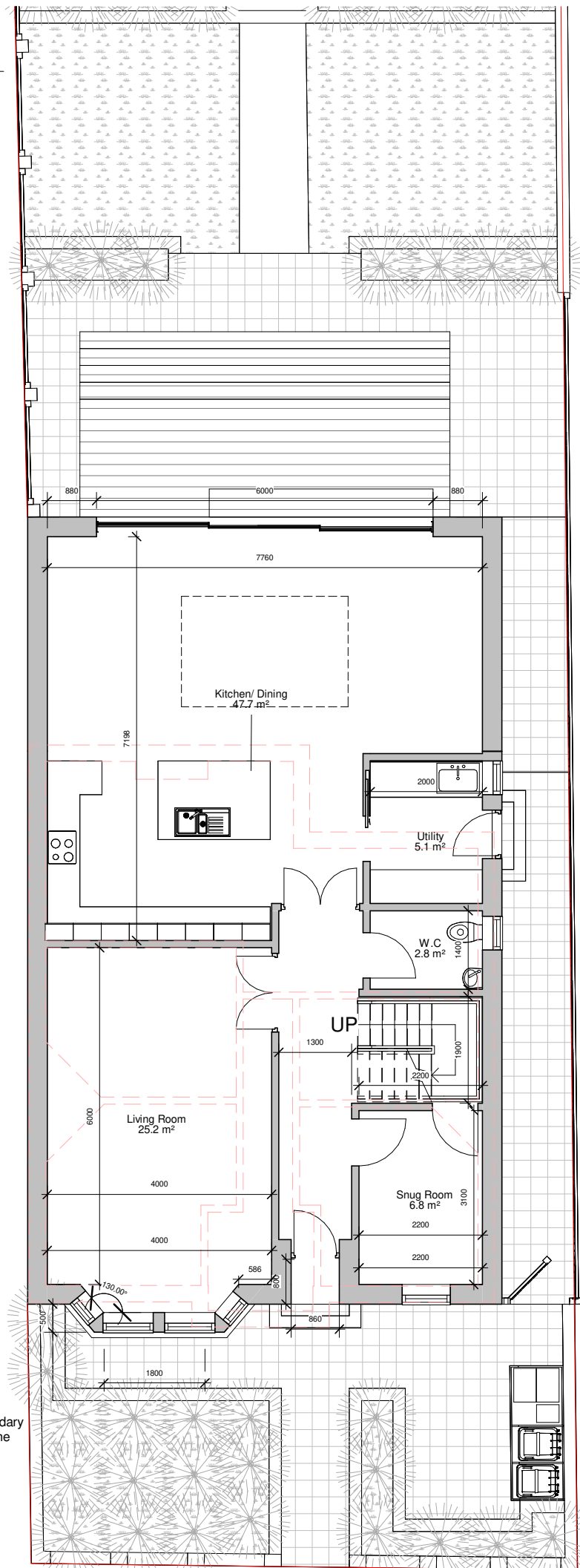
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| DRAWN BY: LG | CHECKED BY: JH |
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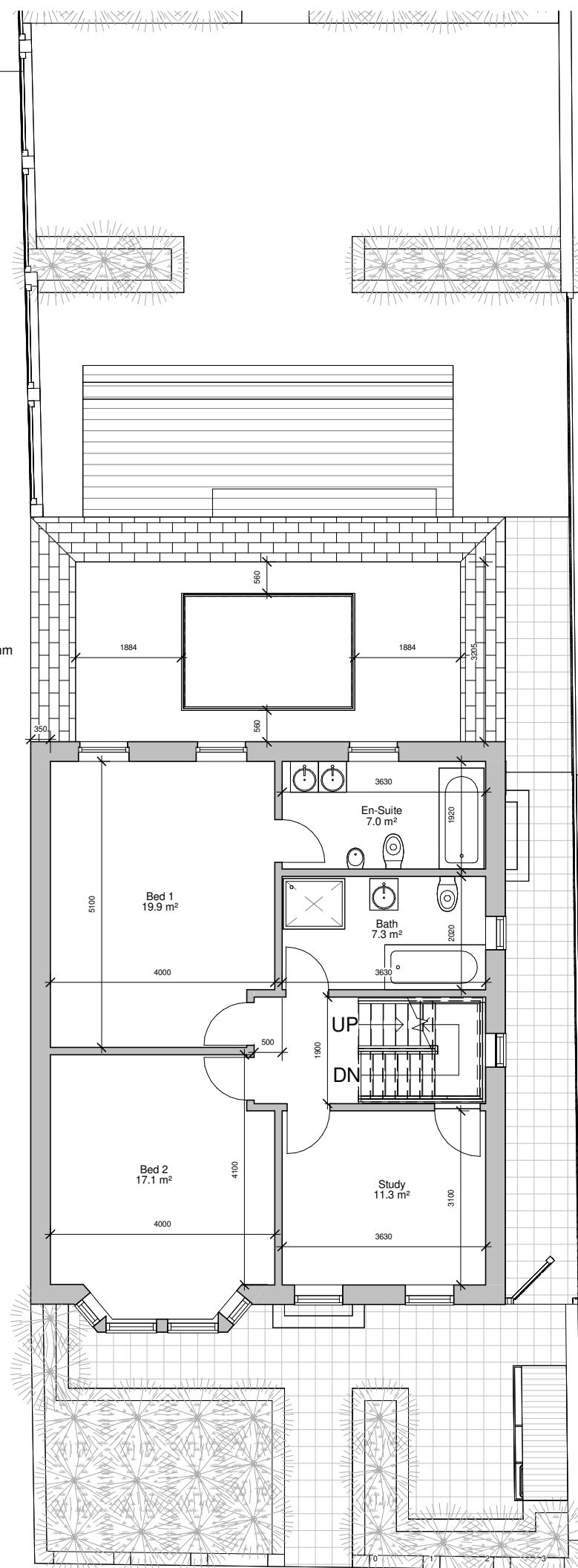
GF Lvl

1 : 100



FF Lvl

1 : 100



1No. 3000 x 2000 mm skylight proposed

Bin store to fit 360l bin, 2x 55l recycle boxes, 23l food waste, 240l garden waste

PROGRAMME:

KEY:

| | | | |
|-----------|----------------------|------------|-------------------|
| | Neighbouring context | RWP | Rain Water Pipe |
| | Existing walls | SVP | Soil Vent Pipe |
| | Proposed walls | | Boundary line |
| | Proposed rooflight | | Existing removed |
| MH | Manhole | | Existing beam |
| B | Boiler | | 1.2 m head height |
| EM | Electric Meter | | 1.5 m head height |
| GM | Gas Meter | | Ridge line |

REVISION NOTES:

| REV: | DATE: | DESCRIPTION: |
|------|-------|--------------|
|------|-------|--------------|

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Extension Plans. Ealing Cross, 85 Uxbridge Rd, London W5 5BW

CLIENT: Jamie & Beverley McDaid

PROJECT: New 4 Bed House

PROJECT ADDRESS: 99 Atbara Road, Teddington TW11 9PA

PROPOSED FLOOR PLANS

DRAWING TITLE:

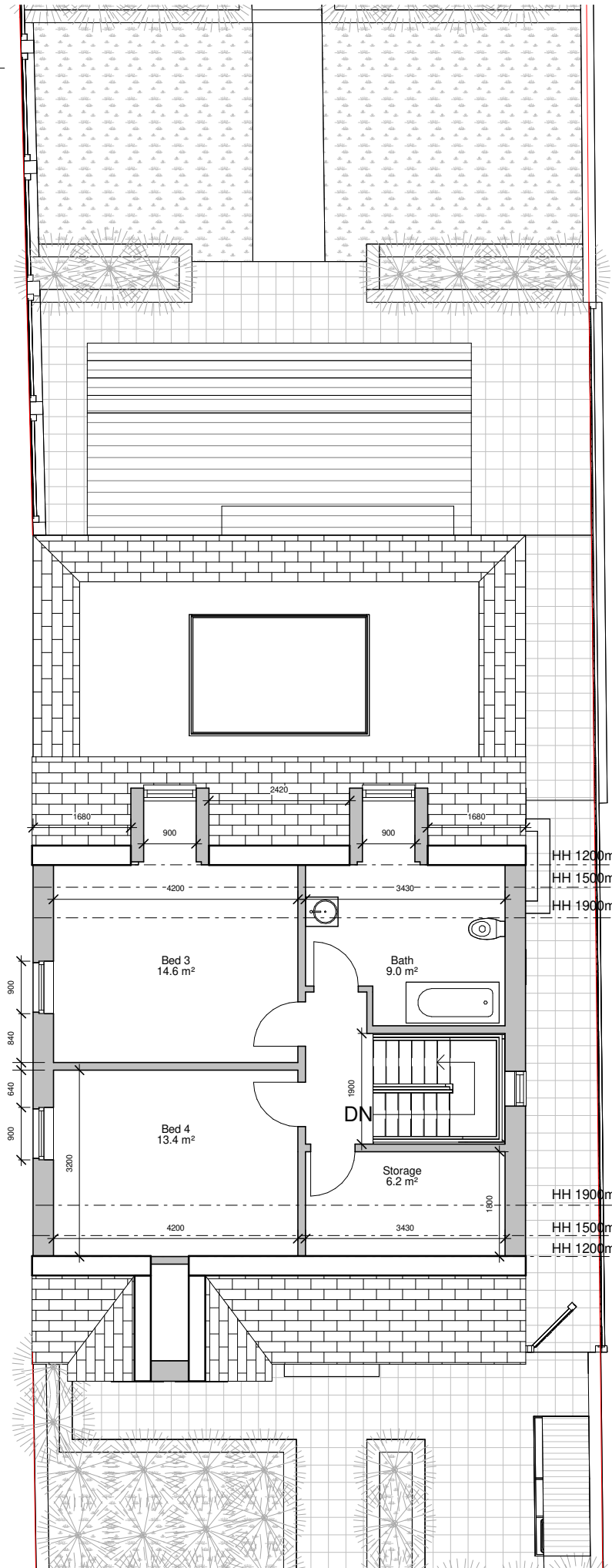
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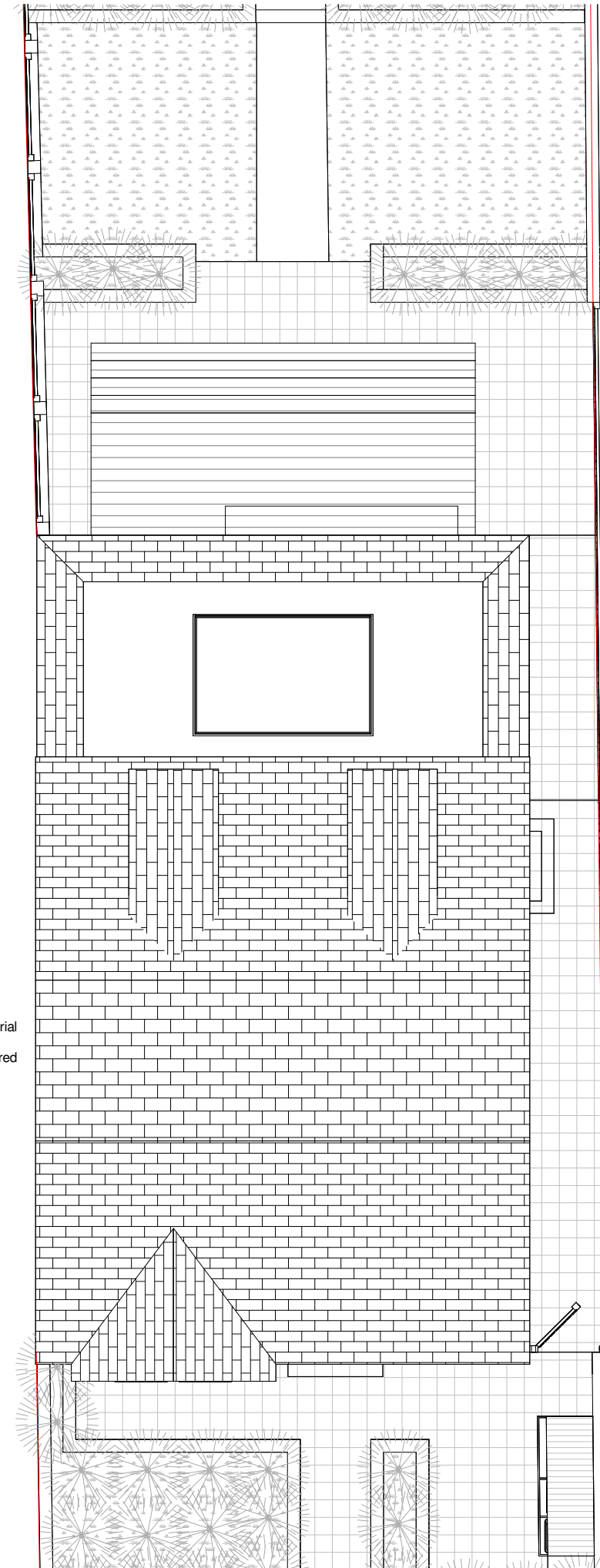
Loft Lvl

1 : 100



ROOF PLAN

1 : 100



Roof material to be gray slate with red ridge tiles

PROGRAMME:

KEY:

| | | | |
|-----------|----------------------|------------|-------------------|
| | Neighbouring context | RWP | Rain Water Pipe |
| | Existing walls | SVP | Soil Vent Pipe |
| | Proposed walls | | Boundary line |
| | Proposed rooflight | | Existing removed |
| MH | Manhole | | Existing beam |
| B | Boiler | | 1.2 m head height |
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| GM | Gas Meter | | Ridge line |

REVISION NOTES:

REV: | DATE: | DESCRIPTION:

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Extension Plans. Ealing Cross, 85 Uxbridge Rd, London W5 5BW

CLIENT: Jamie & Beverley McDaid

PROJECT: New 4 Bed House

99 Atbara Road,
Teddington
TW11 9PA

PROJECT ADDRESS:

PROPOSED FLOOR PLANS 2

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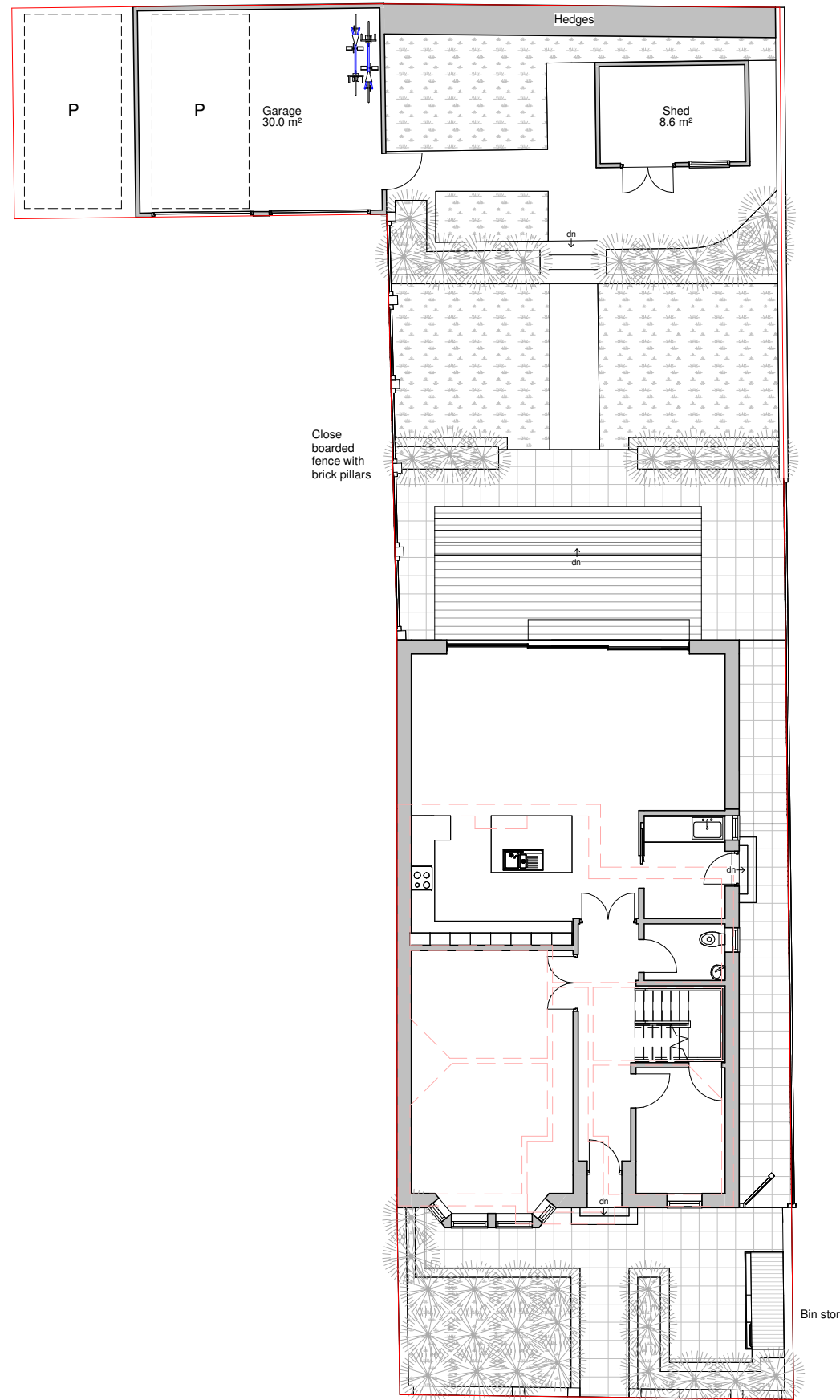
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DATE: 22/09/2023 | Rev: | Rev. DATE:

SCALE@A3: 1:100 | DRAWING No: AR-R02-PR-103

Full Plan

1 : 150



PROGRAMME:

KEY:

| | | | |
|-----------|----------------------|------------|-------------------|
| | Neighbouring context | RWP | Rain Water Pipe |
| | Existing walls | SVP | Soil Vent Pipe |
| | Proposed walls | | Boundary line |
| | Proposed rooflight | | Existing removed |
| MH | Manhole | | Existing beam |
| B | Boiler | | 1.2 m head height |
| EM | Electric Meter | | 1.5 m head height |
| GM | Gas Meter | | Ridge line |

REVISION NOTES:

REV: | DATE: | DESCRIPTION:

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Extension Plans. Ealing Cross, 85 Uxbridge Rd, London W5 5BW

CLIENT: Jamie & Beverley McDaid

PROJECT: New 4 Bed House

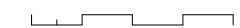
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DRAWN BY: LG | CHECKED BY: JH

DATE: 22/09/2023 | Rev: | Rev. DATE:

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PROPOSED STREET SCENE

1 : 100



PROGRAMME:

KEY:

| | | | |
|-----------|----------------------|------------|-------------------|
| | Neighbouring context | RWP | Rain Water Pipe |
| | Existing walls | SVP | Soil Vent Pipe |
| | Proposed walls | | Boundary line |
| | Proposed rooflight | | Existing removed |
| MH | Manhole | | Existing beam |
| B | Boiler | | 1.2 m head height |
| EM | Electric Meter | | 1.5 m head height |
| GM | Gas Meter | | Ridge line |

REVISION NOTES:

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Extension Plans. Ealing Cross, 85 Uxbridge Rd, London W5 5BW

CLIENT: Jamie & Beverley McDaid

PROJECT: New 4 Bed House

PROJECT ADDRESS: 99 Atbara Road,
Teddington
TW11 9PA

DRAWING TITLE: PROPOSED STREET SCENE

DRAWN BY: LG | CHECKED BY: JH

DATE: 22/09/2023 | Rev: | Rev. DATE:

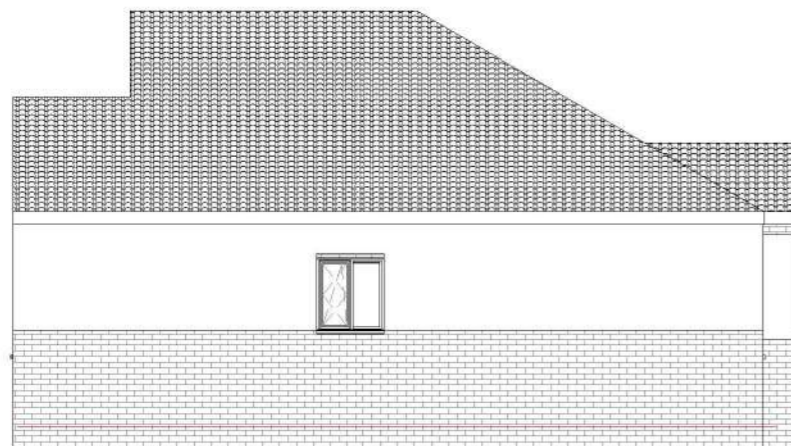
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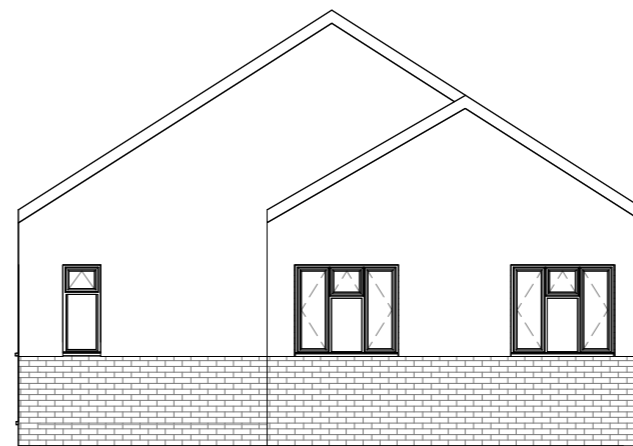
RH ELEVATION
1 : 100



FRONT ELEVATION
1 : 100



LH ELEVATION
1 : 100



REAR ELEVATION
1 : 100



PROGRAMME:

REVISION NOTES:

REV: | DATE: | DESCRIPTION:

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EXTENSION PLANS

Extension Plans. 16 Shakespeare Road W7 1LR

Jamie & Beverley McDaid

CLIENT:

New 4 Bed House

PROJECT:

99 Atbara Road,
Teddington
TW11 9PA

PROJECT ADDRESS:

EXISTING ELEVATIONS

DRAWING TITLE:

DRAWN BY: LG

CHECKED BY: JH

DATE: 22/09/2023

Rev:

Rev. DATE:

SCALE@A3: 1:100

DRAWING No: HR-R00-EX-103

FRONT ELEVATION

1 : 100



RH ELEVATION

1 : 100



PROGRAMME:

KEY:

| | | | |
|-----------|----------------------|------------|-------------------|
| | Neighbouring context | RWP | Rain Water Pipe |
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| MH | Manhole | | Existing beam |
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REVISION NOTES:

REV: | DATE: | DESCRIPTION:

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Extension Plans. Ealing Cross, 85 Uxbridge Rd, London W5 5BW

CLIENT: Jamie & Beverley McDaid

PROJECT: New 4 Bed House

99 Atbara Road,
Teddington
TW11 9PA

PROJECT ADDRESS:

PROPOSED ELEVATIONS

DRAWING TITLE:

DRAWN BY: LG | CHECKED BY: JH

DATE: 22/09/2023 | Rev: | Rev. DATE:

SCALE@A3: 1:100 | DRAWING No: AR-R02-PR-105

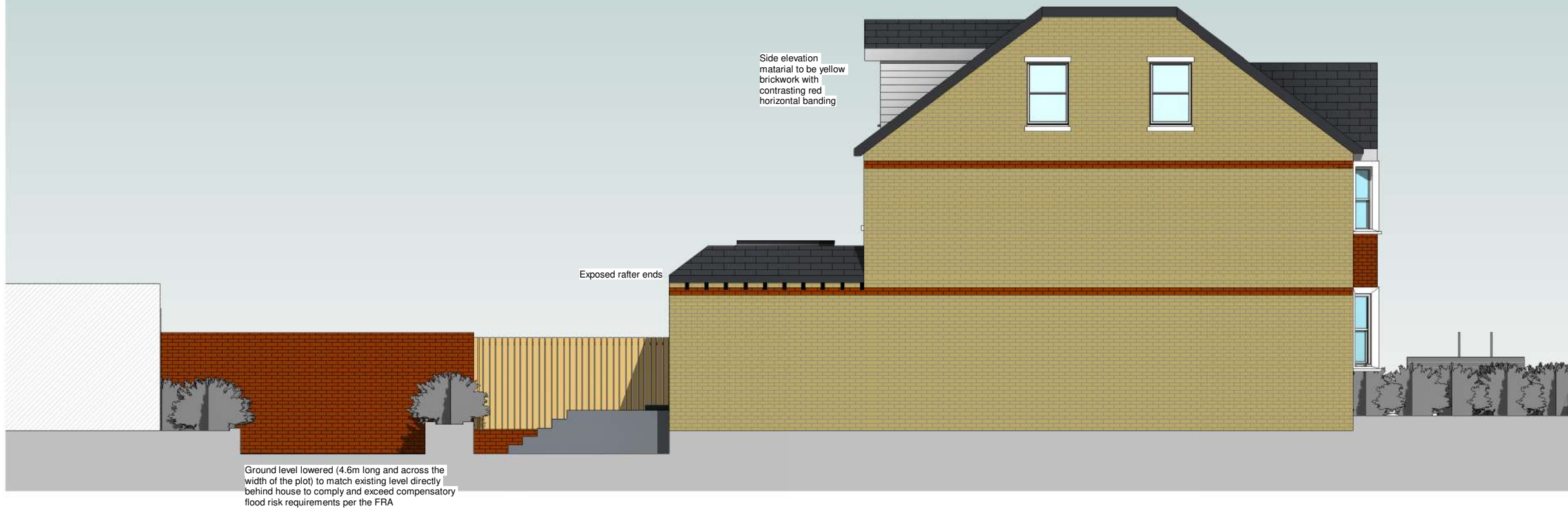
REAR ELEVATION

1 : 100



LH ELEVATION

1 : 100



PROGRAMME:

KEY:

| | | | |
|-----------|----------------------|------------|-------------------|
| | Neighbouring context | RWP | Rain Water Pipe |
| | Existing walls | SVP | Soil Vent Pipe |
| | Proposed walls | | Boundary line |
| | Proposed rooflight | | Existing removed |
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| GM | Gas Meter | | Ridge line |

REVISION NOTES:

| REV: | DATE: | DESCRIPTION: |
|------|-------|--------------|
|------|-------|--------------|

- GENERAL NOTES:
- All Dimensions are in millimetres unless otherwise stated
 - All work to be carried out in accordance with current building regulations and all relevant british standards/codes of practice.
 - The Contractor is responsible for the correct setting out of the works on site, all dimensions to be checked prior to fabrication of materials and commencement of works.
 - This Drawing is to be read in conjunction with all relevant drawings and specifications
 - Exact SVP and Boiler position to be determined onsite by contractor
 - A 'macerator toilet' would be required for a certain designs if the toilet location is away from existing SVP
 - Steels imbedded into ceiling may be charged additionally by your contractor
 - All proposed materials are to be similar in appearance to that of the existing house, unless otherwise stated.
 - Skylights must not protrude past the roof slope by more than 150mm
 - Glazing which exceeds 25% of the added floor area will result in extra charges for S.A.P Calculations
 - Windows on a side elevation at first floor level or above must be obscured glazing and non openable below 1.7m
 - Load-bearing partitions and/or posts are shown in a rough position. The exact position is to be confirmed by a structural engineer prior to construction.



Extension Plans. Ealing Cross, 85 Uxbridge Rd, London W5 5BW

CLIENT: Jamie & Beverley McDaid

PROJECT: New 4 Bed House

PROJECT ADDRESS: 99 Atbara Road, Teddington TW11 9PA

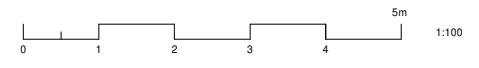
PROPOSED ELEVATIONS

DRAWING TITLE:

DRAWN BY: LG | CHECKED BY: JH

DATE: 22/09/2023 | Rev: | Rev. DATE:

SCALE@A3: 1:100 | DRAWING No: AR-R02-PR-106

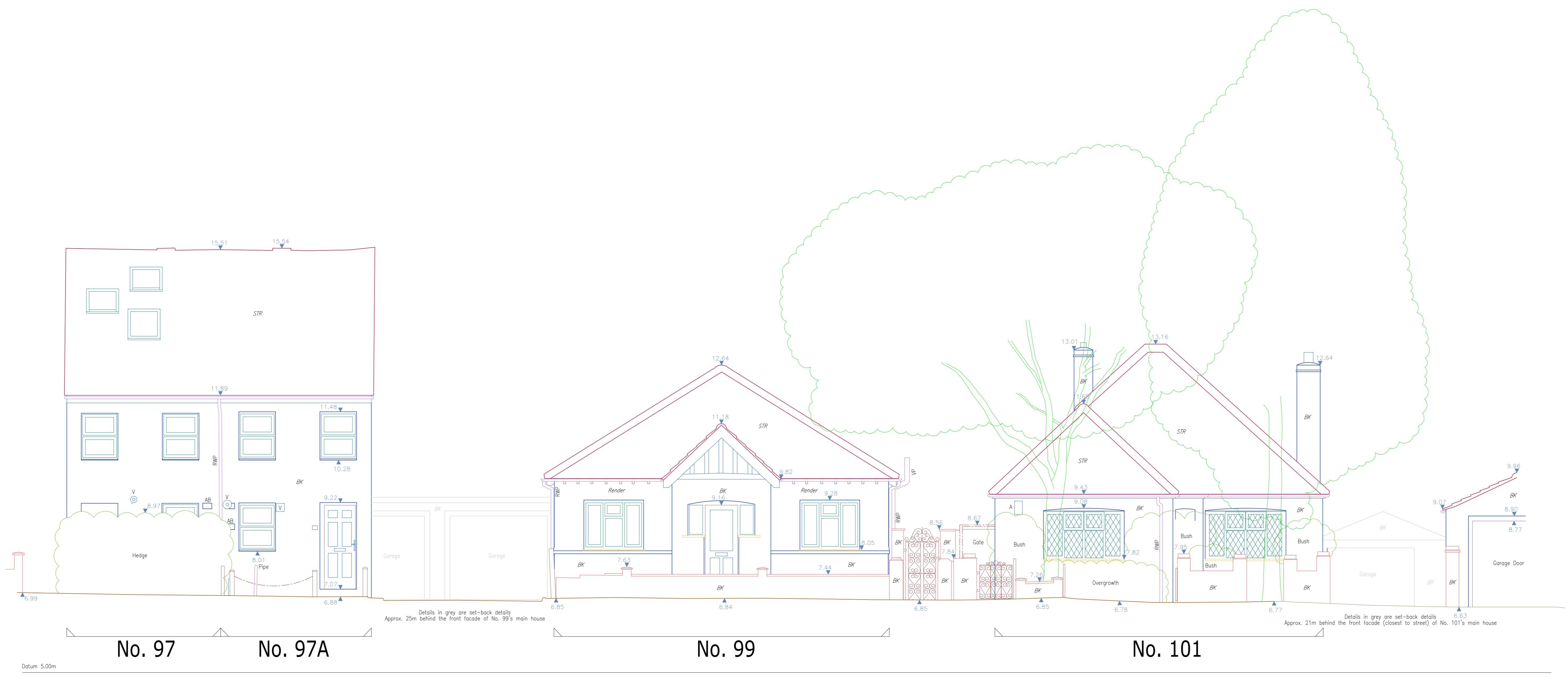


| Abbreviations | | | |
|---------------|-----------------------|-----|------------------|
| A | Alarm Box | L | Light |
| AB | Air Brick | RRP | Rain Water Pipe |
| ACU | Air Conditioning Unit | STR | Steep Tiled Roof |
| BC | Brick | STP | Soil Vent Pipe |
| CC | Column | TB | Telecoms Box |
| CM | Gas Meter | V | Vent |
| HR | Handrail | WP | Wet Pipe |
| JR | Junction Box | WV | Waste Pipe |

Survey Datum
 Ordnance Datum Newlyn (ODN) - GPS Derived Orthometric Heights related to OSGM15



| Rev | Notes | Date | By |
|-----|------------------------|----------|----|
| A | Added set-back details | 13/07/23 | LW |
| | | | |
| | | | |



Street Scene Elevation

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Regulated by RICS

Client: Jamie McDaid

Drawing Title: Street Scene Elevation

Project: 99 Albara Road
 Teddington TW11 9PA

Surveyed MG | Checked LW | Status: FINAL | Size: A0
 Scale: 1:50
 Date: Jul 2023 | Ref No: 2391_01 | Sheet: 01 of 01

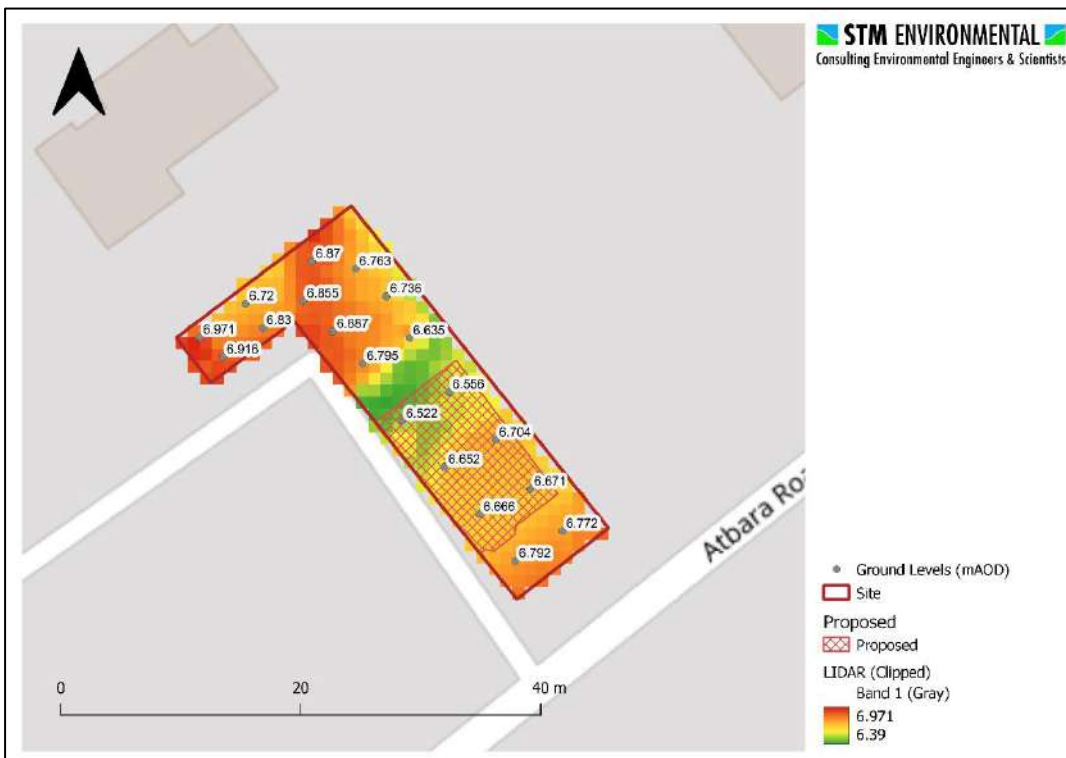
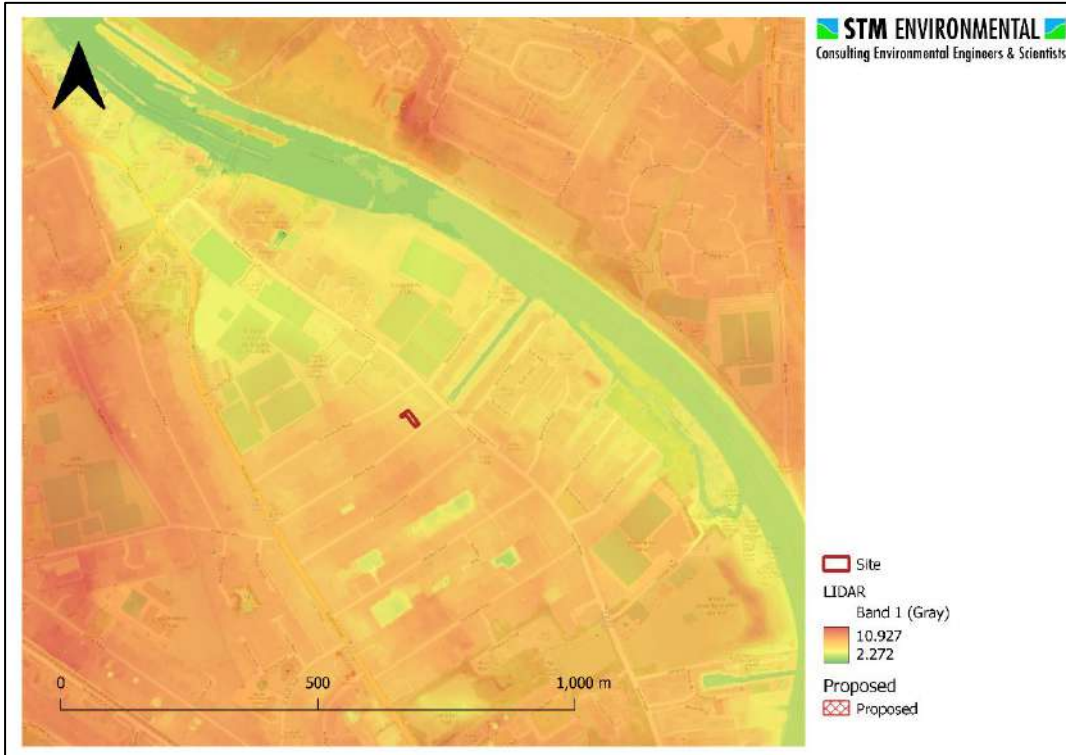
10.1.2 Site Photos





10.2 Appendix 2– Site Topography and Drainage Characteristics

10.2.1 LIDAR Mapping showing Site Topography - (Source: LiDAR DTM 2022)



10.2.2 Topographic Survey

PDF to follow this page.

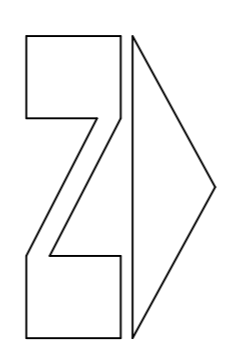
LEGEND

| | | | | | |
|------|-------------------------|-----|---------------------|-----|-----------------|
| Keo | Tree Lash | AP | Anchor Point | UP | Lamp Post |
| AV | Air Valve | AV | Air Valve | URS | Lamp Post Short |
| BH | Berchole | BH | Berchole | MH | Manhole |
| BL | Ballard | WK | Service Marker Post | | |
| BT | British Telecom cover | GBF | Open Board Fence | | |
| BWF | Barbed Wire Fence | PA | Parking Marker | | |
| CANY | Cable Television Cover | RRF | Post and Rail Fence | | |
| CH | Chainlink Fence | RE | Rodding Eye | | |
| CLF | Chainlink Fence | RS | Road Sign | | |
| CPS | Concrete pointing slabs | SC | Stop Cock | | |
| CV | Cable Television Point | PWF | Post and Wire Fence | | |
| DN | Column | SV | Slide Valve | | |
| DP | Downpipe | TCB | Telephone Call Box | | |
| DPC | Damp Proof Course | TPW | Tactile Paving | | |
| EC | Electricity Cover | TKT | Ticket Machine | | |
| EP | Electricity Pole | TP | Telephone Pole | | |
| FLL | Finished Floor Level | TS | Traffic Signal | | |
| FH | Fire Hydrant | UL | Softly/upper level | | |
| FP | Fence Post | UNT | Unable to fit | | |
| GP | Gate Post | VP | Vent Pipe | | |
| G | Gully | WO | Wash Out | | |
| KO | Keel Outlet | WM | Water Meter | | |
| LB | Letter Box | WVF | Wire Mesh Fence | | |

NOTE: The Survey has been oriented to the O.S. National Grid (OSGB36) via a Global Position System and the O.S. Active Network (OS Net) OSGB36. True OSGB36 coordinates have been established at a point near the site centre and a further OSGB36 point established to create a true O.S. bearing for angle orientation. All levels are based on OS datum. Note that the datum used for the application of the O.S. Coordinate System is the datum used for the O.S. Coordinate System which would require scale factors to be applied to all distances. The Survey Station table should be used to establish any on-site coordinates.

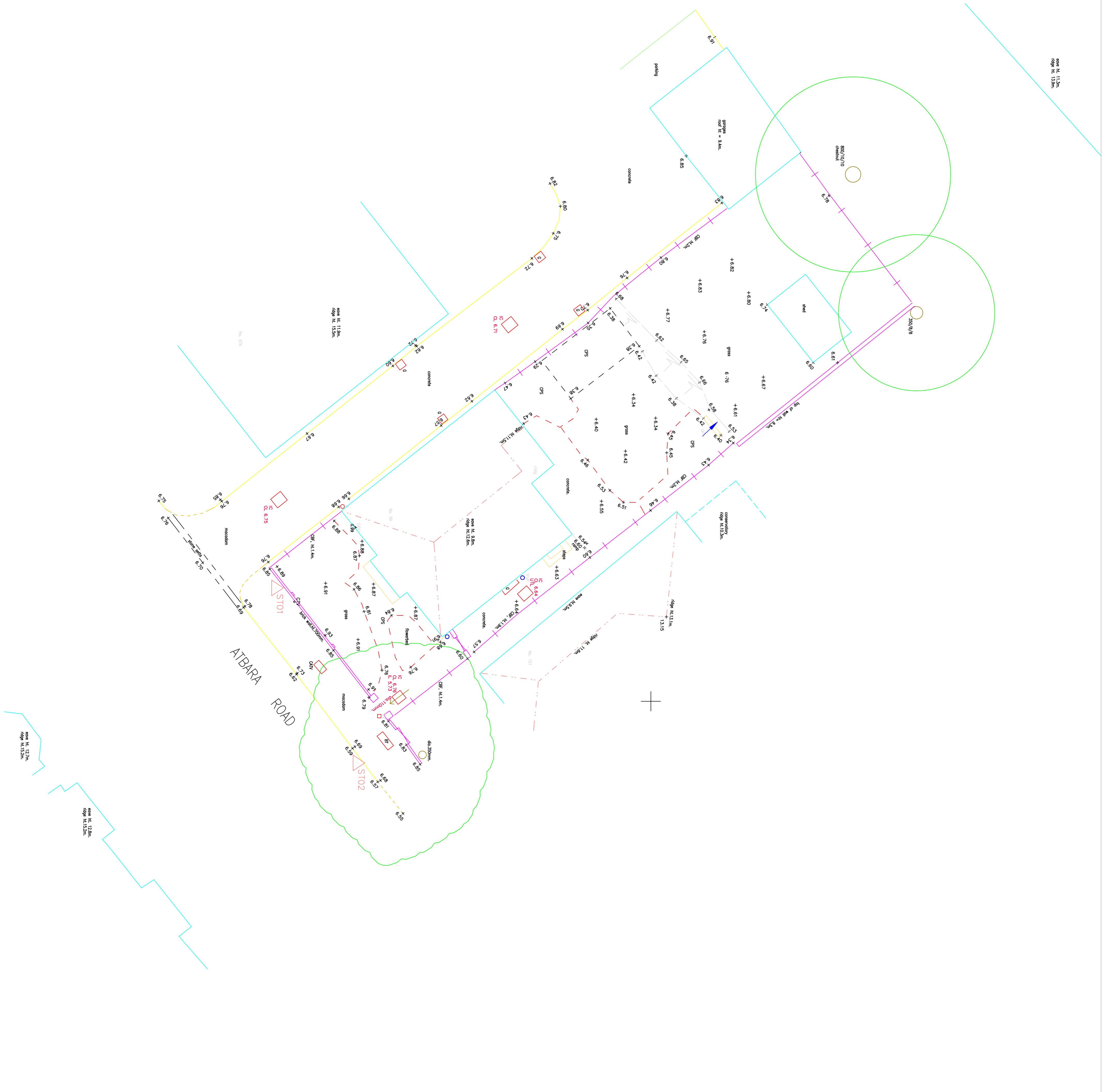
- NOTE:**
- This is a topographic survey and as such the physical features shown are not necessarily legal boundaries.
 - Drainage information is by surface inspection only and cannot be guaranteed.
 - This survey has been carried out on an accuracy comparable with the scales shown on the title certificate with the scales shown on the title certificate. The accuracy of the surveying by digital means will not increase the accuracy of the survey.

Tree Information
 400/7/8 bole dia.(mm)/spread(m)/height(m)
 Tree species should be checked by an expert if identification is critical.
 Trees shown overage spread unless otherwise shown.
 Tree heights are by visual estimation and are not measured.



SURVEY STATIONS

| | | | | |
|---------|----------|--------|-------|------|
| Station | Spotting | Height | Level | Type |
| ST01 | 51703116 | 6.81 | 6.81 | NS |
| ST02 | 11703495 | 6.81 | 6.81 | NS |



PRECISION AND RELIABILITY

AT LAND SURVEYS
 86, Hightown Gardens,
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Project
99, ATBARA ROAD
TEDDINGTON
TW11 9PA

Drawing Title
SITE SURVEY

| | | | |
|-------|----------|---------|----------|
| Drawn | Date | Checked | Date |
| AT | MAY 2023 | AT | MAY 2023 |

Scale
1:100 (A1 SIZE)

Drawing Number
2330-S20

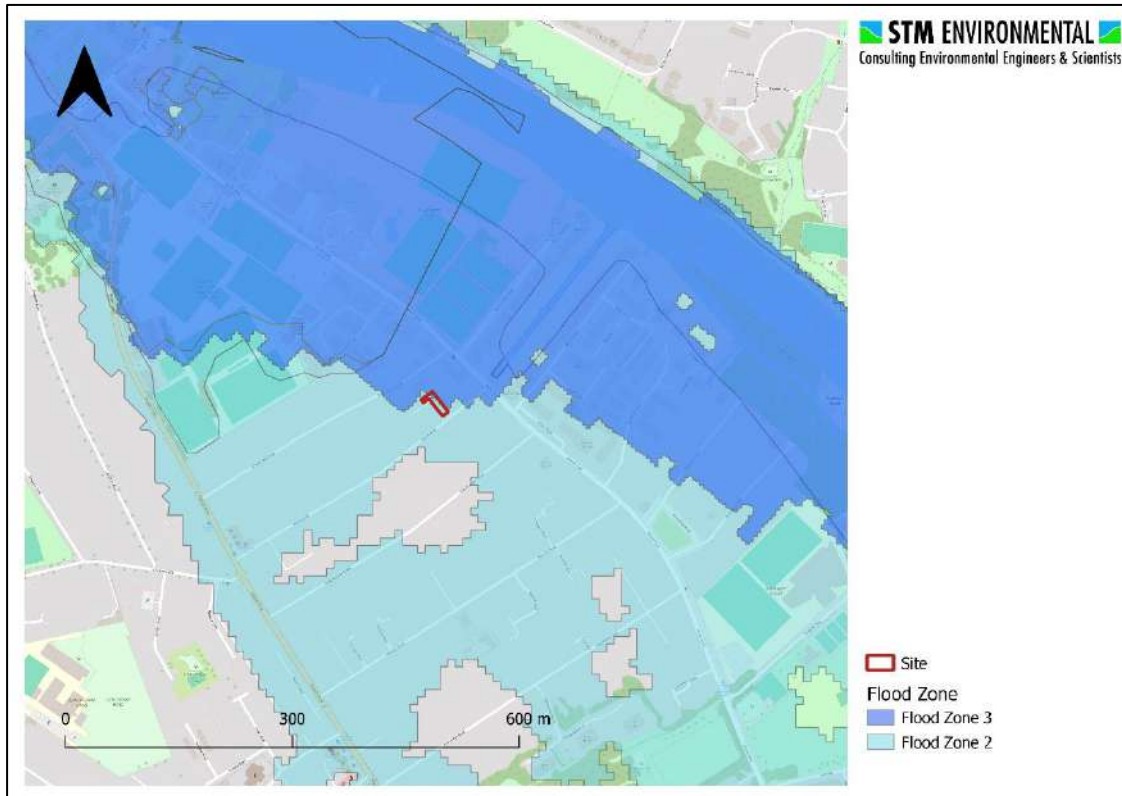
Rev
A

Revision

| | | | |
|----------|--------|------|-------------|
| Revision | Author | Appr | Date |
| A | | | 14 May 2024 |

Trees removed

10.2.3 Hydrology Map



10.2.4 Bedrock Geology, Hydrogeology & Permeability (Source: BGS, 2016)



10.2.5 Superficial Deposits, Hydrogeology, & Permeability (Source: BGS, 2016)



10.2.6 Infiltration Drainage Potential (Source: BGS, 2016)



10.2.7 Groundwater Susceptibility and Table Depth (Source: BGS 2016)



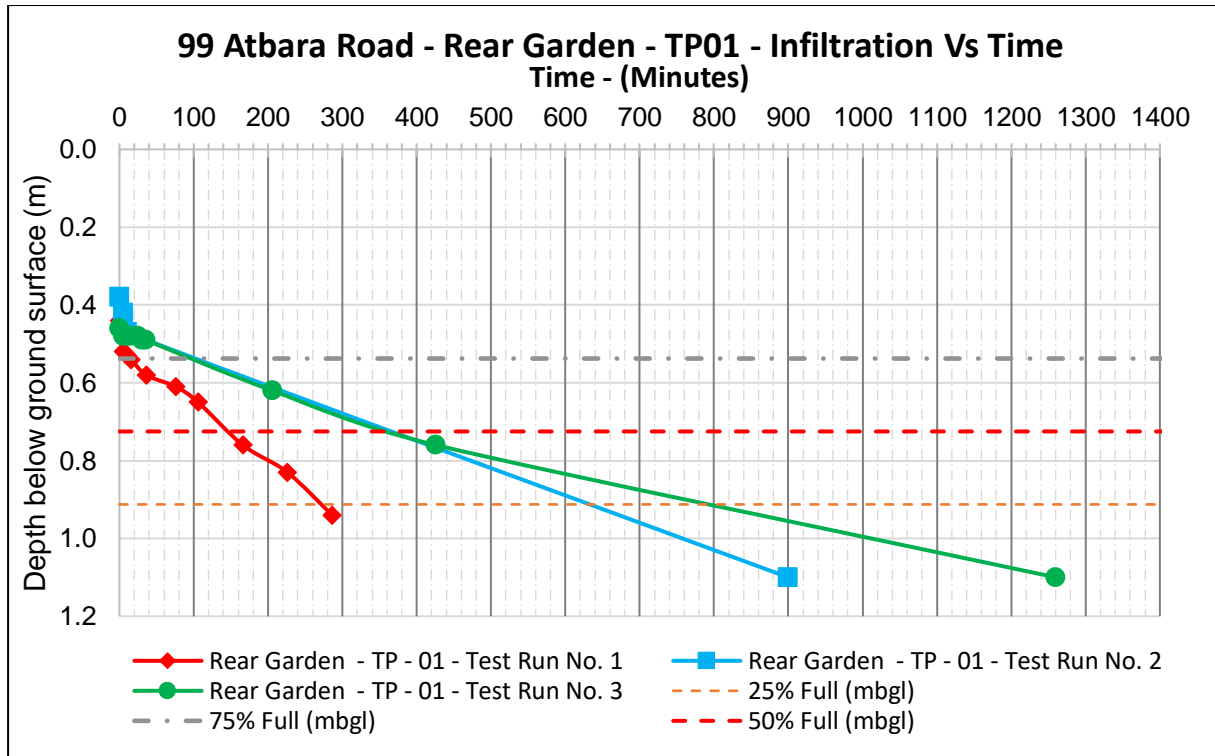
10.2.8 Site Investigation Photos

PDF to follow this page.





10.2.9 Infiltration Testing Graph



10.2.10 Infiltration Data and Results

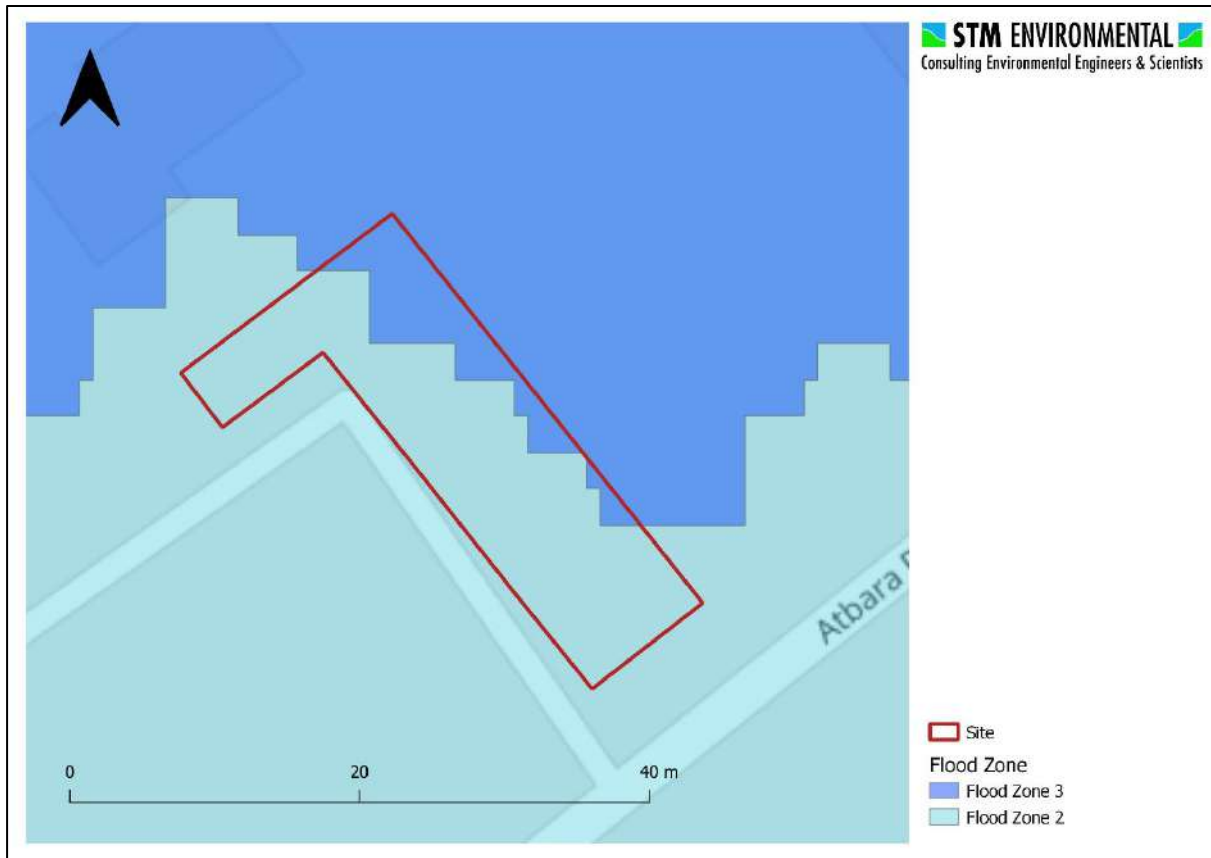
| Rear Garden - TP - 01 - Test Run No. 1 | | | | | | | | | | |
|---|------------------------|--------------|--------------|----------------|----------|-------|-----------------|-----------------|-----------------|--------|
| insert time according to the measured units | | | | | | | | | | |
| Dip Reading | Water Level Above Base | Depth (mbgl) | Time (hours) | Time (minutes) | Time (s) | Time | 25% Full (mbgl) | 50% Full (mbgl) | 75% Full (mbgl) | |
| | 0.66 | 0.4 | 0.00 | 0 | 0 | 0:00 | 11:44:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.58 | 0.5 | 0.08 | 5 | 300.00 | 0:05 | 11:49:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.57 | 0.5 | 0.17 | 10 | 600.00 | 0:10 | 11:54:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.56 | 0.5 | 0.27 | 16 | 960.00 | 0:16 | 12:00:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.52 | 0.6 | 0.60 | 36 | 2160.00 | 0:36 | 12:20:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.49 | 0.6 | 1.27 | 76 | 4560.00 | 1:16 | 13:00:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.45 | 0.7 | 1.77 | 106 | 6360.00 | 1:46 | 13:30:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.34 | 0.8 | 2.77 | 166 | 9960.00 | 2:46 | 14:30:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.27 | 0.8 | 3.77 | 226 | 13560.00 | 3:46 | 15:30:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.16 | 0.9 | 4.77 | 286 | 17160.00 | 4:46 | 16:30:00 | 0.9125 | 0.73 | 0.5375 |
| | | | | 496 | | 8:16 | 20:00:00 | 0.9125 | 0.73 | 0.5375 |
| | | | | 1560 | | 02:00 | 20:00:00 | 0.9125 | 0.73 | 0.5375 |
| Reached 25% within 24 hours. Second run undertaken. | | | | | | | | | | |
| Rear Garden - TP - 01 - Test Run No. 2 | | | | | | | | | | |
| insert time according to the measured units | | | | | | | | | | |
| Dip Reading | Water Level Above Base | Depth (mbgl) | Time (hours) | Time (minutes) | Time (s) | Time | 25% Full (mbgl) | 50% Full (mbgl) | 75% Full (mbgl) | |
| | 0.72 | 0.4 | 0.00 | 0 | 0 | 0:00 | 16:40:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.68 | 0.4 | 0.08 | 5 | 300.00 | 0:05 | 16:45:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.63 | 0.5 | 0.17 | 10 | 600.00 | 0:10 | 16:50:00 | 0.9125 | 0.73 | 0.5375 |
| | 0 | 1.1 | 15.00 | 900 | 54000.00 | 15:00 | | | | |
| Reached 25% within 24 hours. Second run undertaken. | | | | | | | | | | |
| Rear Garden - TP - 01 - Test Run No. 3 | | | | | | | | | | |
| insert time according to the measured units | | | | | | | | | | |
| Dip Reading | Water Level Above Base | Depth (mbgl) | Time (hours) | Time (minutes) | Time (s) | Time | 25% Full (mbgl) | 50% Full (mbgl) | 75% Full (mbgl) | |
| | 0.64 | 0.5 | 0.00 | 0 | 0 | 0:00 | 08:54:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.62 | 0.5 | 0.08 | 5 | 300.00 | 0:05 | 08:59:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.62 | 0.5 | 0.17 | 10 | 600.00 | 0:10 | 09:04:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.62 | 0.5 | 0.25 | 15 | 900.00 | 0:15 | 09:09:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.62 | 0.5 | 0.42 | 25 | 1500.00 | 0:25 | 09:19:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.61 | 0.5 | 0.50 | 30 | 1800.00 | 0:30 | 09:24:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.61 | 0.5 | 0.58 | 35 | 2100.00 | 0:35 | 09:29:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.48 | 0.6 | 3.43 | 206 | 12360.00 | 3:26 | 12:20:00 | 0.9125 | 0.73 | 0.5375 |
| | 0.34 | 0.8 | 7.10 | 426 | 25560.00 | 7:06 | 16:00:00 | 0.9125 | 0.73 | 0.5375 |
| | 0 | 1.1 | 21.00 | 1260 | 75600.00 | 21:00 | | | | |

10.2.11 Soakaway Test Location Map

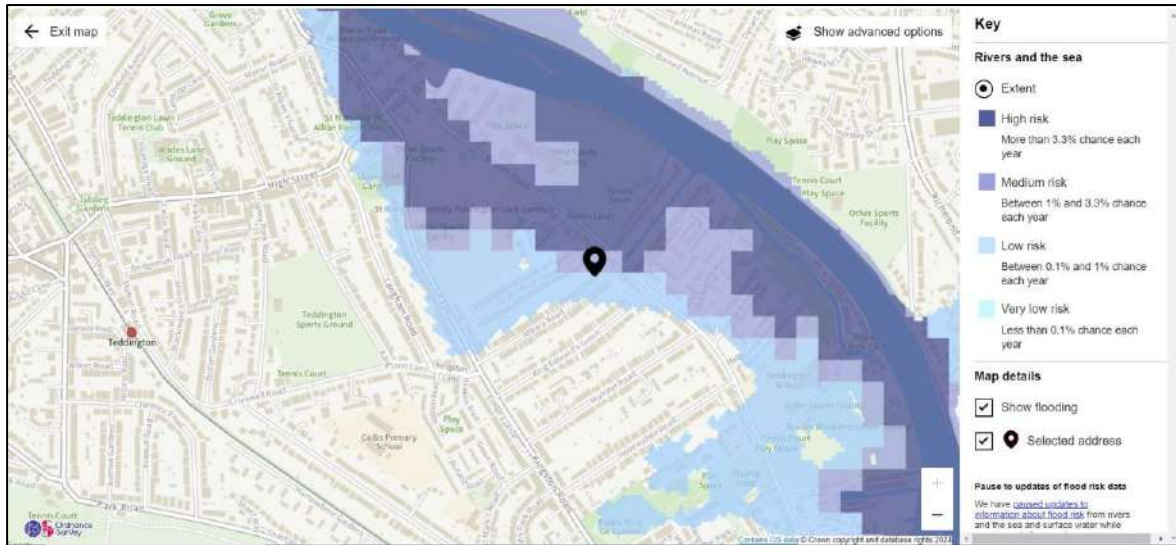


10.3 Appendix 3 – Flood Risk Mapping

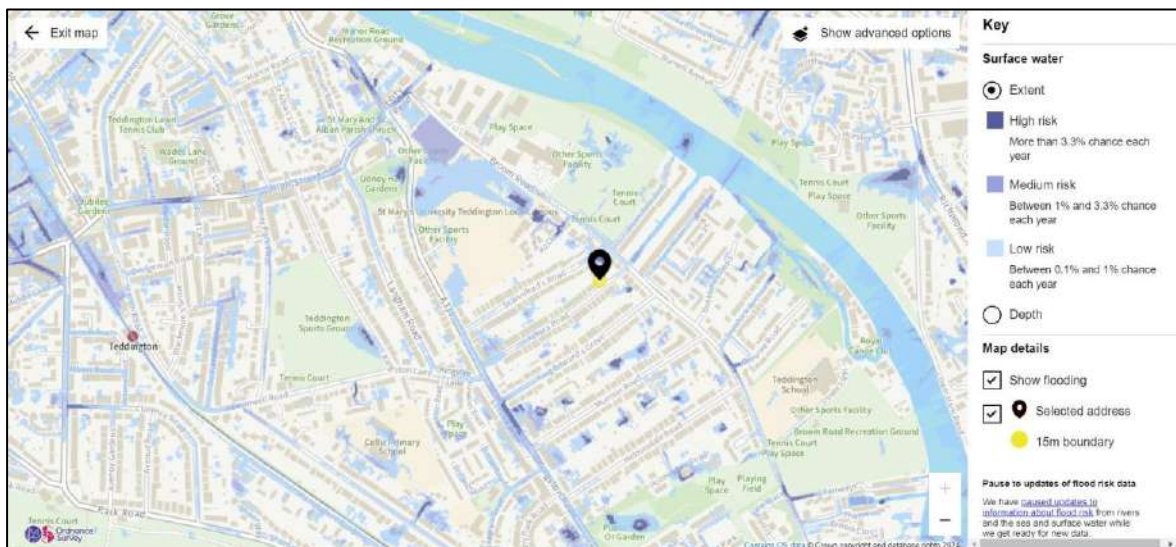
10.3.1 Flood Map For Planning (EA)



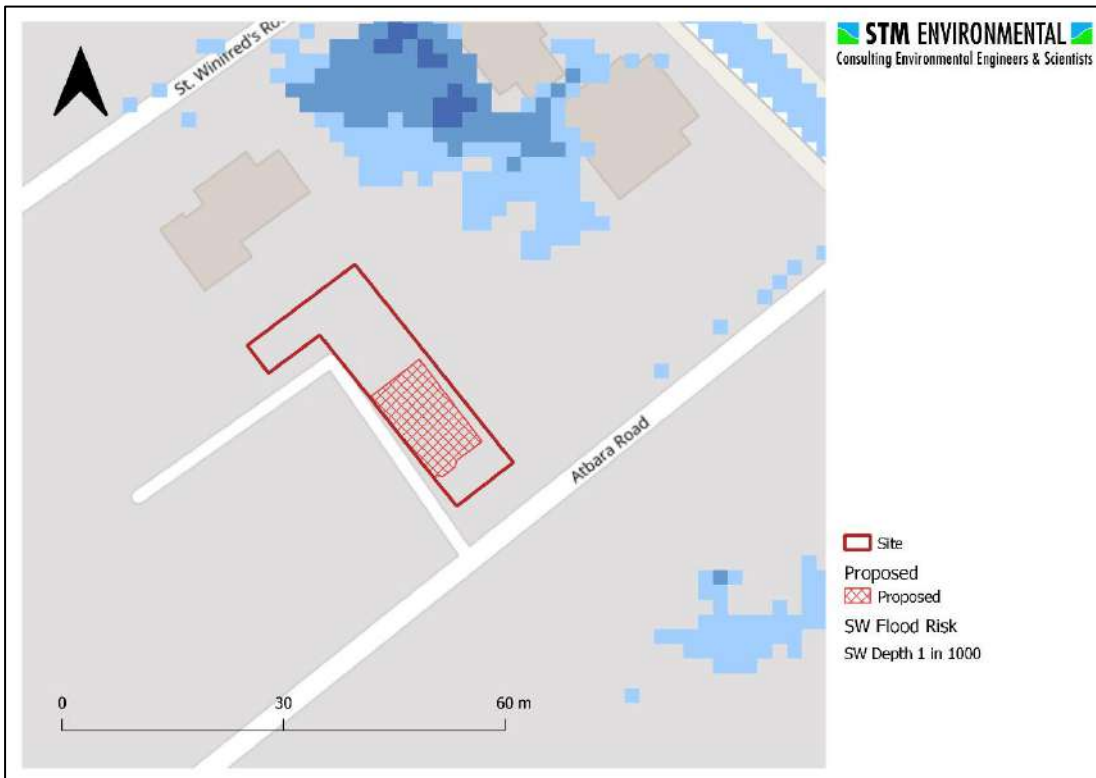
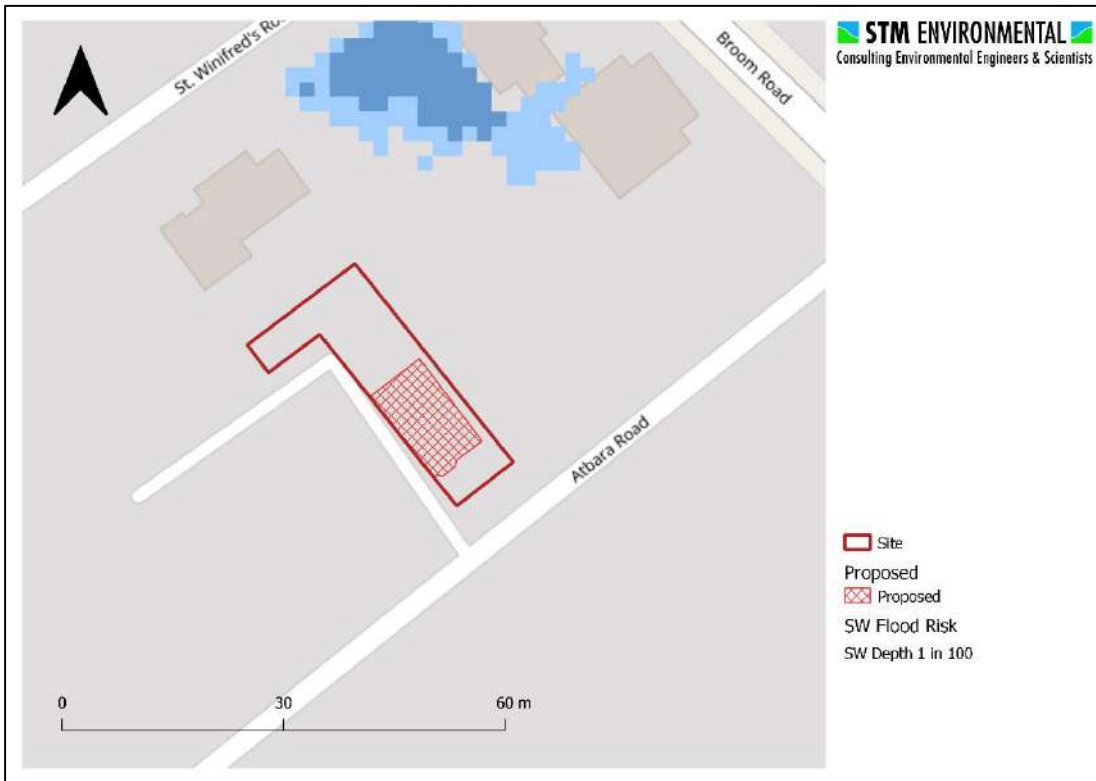
10.3.2 Long Term Fluvial Flood Risk Map (EA)



10.3.3 Long Term Pluvial Flood Risk Map (EA)



10.3.4 Surface water flood depth during the 1 in 100 and 1 in 1000 year rainfall return periods (Source: EA, 2016).



10.3.5 Groundwater flooding susceptibility (Source: BGS, 2016).



10.4 Appendix 4 – Runoff Rate and Storage Calculations

10.4.1 UK SuDS

PDF to follow this page.

Calculated by:

Site name:

Site location:

Site Details

Latitude:

Longitude:

Reference:

Date:

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Runoff estimation approach

Site characteristics

Total site area (ha):

Methodology

Q_{BAR} estimation method:

SPR estimation method:

Notes

(1) Is $Q_{BAR} < 2.0$ l/s/ha?

When Q_{BAR} is < 2.0 l/s/ha then limiting discharge rates are set at 2.0 l/s/ha.

Soil characteristics

| | Default | Edited |
|--------------|----------------------------------|----------------------------------|
| SOIL type: | <input type="text" value="2"/> | <input type="text" value="2"/> |
| HOST class: | <input type="text" value="N/A"/> | <input type="text" value="N/A"/> |
| SPR/SPRHOST: | <input type="text" value="0.3"/> | <input type="text" value="0.3"/> |

(2) Are flow rates < 5.0 l/s?

Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.

Hydrological characteristics

| | Default | Edited |
|--------------------------------|-----------------------------------|-----------------------------------|
| SAAR (mm): | <input type="text" value="600"/> | <input type="text" value="600"/> |
| Hydrological region: | <input type="text" value="6"/> | <input type="text" value="6"/> |
| Growth curve factor 1 year: | <input type="text" value="0.85"/> | <input type="text" value="0.85"/> |
| Growth curve factor 30 years: | <input type="text" value="2.3"/> | <input type="text" value="2.3"/> |
| Growth curve factor 100 years: | <input type="text" value="3.19"/> | <input type="text" value="3.19"/> |
| Growth curve factor 200 years: | <input type="text" value="3.74"/> | <input type="text" value="3.74"/> |

(3) Is $SPR/SPRHOST \leq 0.3$?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

Greenfield runoff rates

Default Edited

| | | |
|-------------------------------|------|------|
| Q_{BAR} (l/s): | 0.15 | 0.15 |
| 1 in 1 year (l/s): | 0.13 | 0.13 |
| 1 in 30 years (l/s): | 0.35 | 0.35 |
| 1 in 100 year (l/s): | 0.49 | 0.49 |
| 1 in 200 years (l/s): | 0.57 | 0.57 |

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement , which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

| | |
|----------------|--------------|
| Calculated by: | Yonas Makoni |
| Site name: | TW11 9PA |
| Site location: | TW11 9PA |

This is an estimation of the storage volume requirements that are needed to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). It is not to be used for detailed design of drainage systems. It is recommended that hydraulic modelling software is used to calculate volume requirements and design details before finalising the design of the drainage scheme.

Site Details

| | |
|------------|-------------------|
| Latitude: | 51.42536° N |
| Longitude: | 0.31712° W |
| Reference: | 3638428206 |
| Date: | Jul 24 2024 15:48 |

Site characteristics

| | |
|--|----------------------|
| Total site area (ha): | 0.0374 |
| Significant public open space (ha): | 0.0091 |
| Area positively drained (ha): | 0.028300000000000002 |
| Impermeable area (ha): | 0.0283 |
| Percentage of drained area that is impermeable (%): | 100 |
| Impervious area drained via infiltration (ha): | 0 |
| Return period for infiltration system design (year): | 10 |
| Impervious area drained to rainwater harvesting (ha): | 0 |
| Return period for rainwater harvesting system (year): | 10 |
| Compliance factor for rainwater harvesting system (%): | 66 |
| Net site area for storage volume design (ha): | 0.03 |
| Net impermeable area for storage volume design (ha): | 0.03 |
| Pervious area contribution to runoff (%): | 30 |

Methodology

| | |
|-------------------------------------|-----------------------------|
| esti | IH124 |
| Q _{BAR} estimation method: | Calculate from SPR and SAAR |
| SPR estimation method: | Calculate from SOIL type |

Soil characteristics

| | Default | Edited |
|------------|---------|--------|
| SOIL type: | 2 | 2 |
| SPR: | 0.3 | 0.3 |

Hydrological characteristics

| | Default | Edited |
|------------------------------|---------|--------|
| Rainfall 100 yrs 6 hrs: | -- | 63 |
| Rainfall 100 yrs 12 hrs: | -- | 97.79 |
| FEH / FSR conversion factor: | 1.27 | 1.27 |
| SAAR (mm): | 600 | 600 |
| M5-60 Rainfall Depth (mm): | 20 | 20 |
| 'r' Ratio M5-60/M5-2 day: | 0.4 | 0.4 |
| Hydrological region: | 6 | 6 |
| Growth curve factor 1 year: | 0.85 | 0.85 |
| Growth curve factor 10 year: | 1.62 | 1.62 |
| Growth curve factor 30 year: | 2.3 | 2.3 |

* where rainwater harvesting or infiltration has been used for managing surface water runoff such that the effective impermeable area is less than 50% of the 'area positively drained', the 'net site area' and the estimates of Q_{BAR} and other flow rates will have been reduced accordingly.

Design criteria

| | | | | |
|-----------------------------------|-----------------------|---|------|------|
| Climate change allowance factor: | 1.4 | Growth curve factor 100 years: | 3.19 | 3.19 |
| Urban creep allowance factor: | 1.1 | Q _{BAR} for total site area (l/s): | 0.06 | 0.06 |
| Volume control approach | Use long term storage | Q _{BAR} for net site area (l/s): | 0.04 | 0.04 |
| Interception rainfall depth (mm): | 5 | | | |
| Minimum flow rate (l/s): | 2 | | | |

| Site discharge rates | Default | | Edited | | Estimated storage volumes | Default | | Edited | |
|----------------------|---------|---|--------|---|--|---------|---|--------|---|
| | | | | | | | | | |
| 1 in 1 year (l/s): | 2 | 2 | 2 | 2 | Attenuation storage 1/100 years (m ³): | 7 | 7 | 7 | 7 |
| 1 in 30 years (l/s): | 2 | 2 | 2 | 2 | Long term storage 1/100 years (m ³): | 0 | 0 | 0 | 0 |
| 1 in 100 year (l/s): | 2 | 2 | 2 | 2 | Total storage 1/100 years (m ³): | 7 | 7 | 7 | 7 |

This report was produced using the storage estimation tool developed by HRWallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at <http://uksuds.com/terms-and-conditions.htm>. The outputs from this tool have been used to estimate storage volume requirements. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of these data in the design or operational characteristics of any drainage scheme.

10.4.2 IH24 Method

| Item | Value | | Greenfield Run-off Rate -1 in 100 + CC (l/s) | 0.2691 | |
|--|---------------|---|--|---------------------------------|--------------------------------------|
| Climate Change Allowance Factor | 1.40 | | Total Post Development Run-off Rate - 1 in 100 + CC (l/s) | 0.7656 | |
| SAAR(mm) - Current | 600.00 | | Difference between Greenfield and Post Development Run Off Rates - 1 in 100 + CC (l/s) | 0.4965 | |
| SAAR (mm) + CC | 840.00 | | Volume of Storage Required to meet Greenfield Discharge - Difference between Post Development and Greenfield 1 in 100 + CC volumes (m3) | 10.7248 | |
| SPR (Greenfield) | 0.30 | | Difference between 3 * Greenfield and Post Development 1 in 100 + CC Run Off Rates | -0.0417 | |
| SPR (Impermeable) | 0.53 | | Volume of Storage Required to meet 3 * Greenfield Discharge - Difference between Proposed Development and 3 * Greenfield 1 in 100 +CC (m3) | -0.9015 | |
| Site Area (ha) | 0.0374 | | | | |
| Impermeable Area (Pre Development - ha) | 0.02520 | | | | |
| Permeable Area (Pre Development - ha) | 0.0122000 | | Greenfield (l/s) | Pre - Development (l/s) | Post Development (l/s) |
| Impermeable Area (Post Development - ha) | 0.0283000 | Qbar | 0.06 | 0.15 | 0.16 |
| Permeable Area (Post Development - ha) | 0.0091000 | 1 in 1 | 0.05 | 0.13 | 0.14 |
| GCF (1 in 1) | 0.85 | 1 in 30 | 0.13 | 0.35 | 0.37 |
| GCF (1 in 30) | 2.30 | 1 in 100 | 0.18 | 0.48 | 0.52 |
| GCF (1 in 100) | 3.18 | 1 in 100 + CC | 0.27 | 0.71 | 0.77 |
| Hydrological Region | 6 | | | | |
| Soil Type | 2 | | | | |
| Rainfall 100 Yrs 6 hours mm | 63 | | | | |
| GREENFIELD RUN-OFF | QBAR50 | Run-Off Rate l/s | l/s/ha (QBarA) | 3 times greenfield (l/s) | Volume (6 hr) - Standard (m3) |
| Qbar | 76.0847 | 0.0569 | 1.5217 | | |
| 1 in 1 | | 0.0484 | 1.2934 | 0.1451 | 1.0449 |
| 1 in 30 | | 0.1309 | 3.4999 | 0.3927 | 2.8274 |
| 1 in 100 | | 0.1815 | 4.8542 | 0.5446 | 3.9214 |
| GREENFIELD RUN-OFF + CC | | | | | |
| Qbar Impermeable | 112.7891 | 0.0844 | 2.2558 | 0.2531 | 1.8223 |
| 1 in 1 +CC | | 0.0717 | 1.9174 | 0.2151 | 1.5490 |
| 1 in 30 + CC | | 0.1940 | 5.1883 | 0.5821 | 4.1913 |
| 1 in 100 + CC | | 0.2691 | 7.1959 | 0.8074 | 5.8132 |
| PRE -DEVELOPMENT RUN-OFF (i.e. same rainfall) | | Impermeable Surface Run-Off (l/s/ha (QBarA)) | | | Volume (6 hr) |
| Impermeable Surface Calculation | | | | | |
| Qbar Impermeable | 261.5909 | 0.1318 | 5.2318 | 0.3955 | 2.8478 |
| 1 in 1 | | 0.1121 | 4.4470 | 0.3362 | 2.4206 |
| 1 in 30 | | 0.3032 | 12.0332 | 0.9097 | 6.5499 |
| 1 in 100 | | 0.4206 | 16.6895 | 1.2617 | 9.0844 |
| Permeable Surface Calculation | | Permeable Surface Run-off (l/s) | | | |
| Qbar Permeable | 76.0847 | 0.0186 | 2.0401 | 0.0557 | 0.3408 |
| 1 in 1 | | 0.0158 | 1.7341 | 0.0473 | 0.3408 |
| 1 in 30 | | 0.0427 | 4.6922 | 0.1281 | 0.9223 |
| 1 in 100 | | 0.0592 | 6.5078 | 0.1777 | 1.2792 |
| Impermeable Surface Calculation + Permeable Surface Calculation | | | | | |
| Qbar | 337.6756 | 0.1504 | 7.2719 | 0.4512 | 2.8478 |
| 1 in 1 | | 0.1278 | 6.1911 | 0.3835 | 2.7615 |
| 1 in 30 | | 0.3459 | 16.7263 | 1.0378 | 7.4722 |
| 1 in 100 | | 0.4798 | 23.1973 | 1.4394 | 10.3636 |
| PRE DEVELOPMENT RUN-OFF + CC (increased rainfall) | | Impermeable Surface Run-Off (l/s) | | | |
| Impermeable Surface Calculation | | | | | |
| Qbar Impermeable | 387.7863 | 0.1954 | 6.9062 | 0.42216 | 3.5884 |
| 1 in 1 +CC | | 0.1661 | 5.8702 | 0.3672 | 3.7097 |
| 1 in 30 + CC | | 0.4495 | 15.8243 | 0.9097 | 13.4669 |
| 1 in 100 + CC | | 0.6235 | 22.0306 | 1.2617 | 13.4669 |
| Permeable Surface Calculation | | Permeable Surface Run-off (l/s) | | | |
| Qbar Permeable | 112.7891 | 0.0275 | 3.0242 | 0.0826 | 0.5053 |
| 1 in 1 +CC | | 0.0234 | 2.5706 | 0.0702 | 0.5053 |
| 1 in 30 + CC | | 0.0633 | 6.9571 | 0.1899 | 1.8953 |
| 1 in 100 + CC | | 0.0878 | 9.6473 | 0.2634 | 1.8953 |
| Impermeable Surface Calculation + Permeable Surface Calculation | | | | | |
| Qbar | 500.5754 | 0.2230 | 9.9304 | 0.0826 | 4.2216 |
| 1 in 1 +CC | | 0.1895 | 8.4408 | 0.0702 | 4.0936 |
| 1 in 30 + CC | | 0.5128 | 22.8399 | 0.1899 | 11.0769 |
| 1 in 100 + CC | | 0.7113 | 31.6780 | 0.2634 | 15.3632 |
| POST DEVELOPMENT RUN-OFF (i.e. same rainfall) | | Impermeable Surface Run-Off (l/s/ha (QBarA)) | | | Volume (6 hr) |
| Impermeable Surface Calculation | | | | | |
| Qbar Impermeable | 261.5909 | 0.1481 | 5.2318 | 0.4442 | 2.7184 |
| 1 in 1 | | 0.1259 | 4.4470 | 0.3776 | 2.7184 |
| 1 in 30 | | 0.3405 | 12.0332 | 1.0216 | 7.3556 |
| 1 in 100 | | 0.4723 | 16.6895 | 1.4169 | 10.2020 |
| Permeable Surface Calculation | | Permeable Surface Run-off (l/s) | | | |
| Qbar Permeable | 76.0847 | 0.0138 | 1.5217 | 0.0415 | 0.2542 |
| 1 in 1 | | 0.0118 | 1.2934 | 0.0353 | 0.2542 |
| 1 in 30 | | 0.0318 | 3.4999 | 0.0955 | 0.6879 |
| 1 in 100 | | 0.0442 | 4.8542 | 0.1325 | 0.9541 |
| Impermeable Surface Calculation + Permeable Surface Calculation | | | | | |
| Qbar Permeable | 337.6756 | 0.1619 | 6.7535 | 0.4857 | 2.9726 |
| 1 in 1 | 0.0000 | 0.1376 | 5.7495 | 0.4129 | 4.0298 |
| 1 in 30 | 0.0000 | 0.3724 | 15.5331 | 1.1172 | 8.0436 |
| 1 in 100 | 0.0000 | 0.5165 | 21.5437 | 1.5495 | 11.1561 |
| POST DEVELOPMENT RUN-OFF + CC (increased rainfall) | | Impermeable Surface Run-Off (l/s) | | | |
| Impermeable Surface Calculation | | | | | |
| Qbar Impermeable | 387.7863 | 0.2195 | 7.7557 | 0.47409 | 4.7409 |
| 1 in 1 +CC | | 0.1866 | 6.5924 | 0.0298 | 4.0298 |
| 1 in 30 + CC | | 0.5048 | 17.8382 | 1.0341 | 10.9041 |
| 1 in 100 + CC | | 0.7092 | 24.7408 | 1.51235 | 15.1235 |
| Permeable Surface Calculation | | Permeable Surface Run-off (l/s) | | | |
| Qbar Permeable | 112.7891 | 0.0205 | 2.2558 | 0.0616 | 0.3769 |
| 1 in 1 +CC | | 0.0174 | 1.9174 | 0.0523 | 0.3769 |
| 1 in 30 + CC | | 0.0472 | 5.1883 | 0.1416 | 1.0198 |
| 1 in 100 + CC | | 0.0655 | 7.1959 | 0.1964 | 1.4144 |
| Impermeable Surface Calculation + Permeable Surface Calculation | | | | | |
| Qbar | 500.5754 | 0.2400 | 10.0115 | 0.0616 | 4.7409 |
| 1 in 1 +CC | | 0.2040 | 8.5098 | 0.0523 | 4.4067 |
| 1 in 30 + CC | | 0.5520 | 23.0265 | 0.1416 | 11.9239 |
| 1 in 100 + CC | | 0.7656 | 31.9367 | 0.1964 | 16.5380 |

10.4.3 MRM – Pre - Development

| Rainfall Methodology | FSR | | | | | | | | |
|---|---|-----------------------|---------|---|-----|----|-----|-----|------|
| FSR Region | England & Wales | | | | | | | | |
| M5-60 (mm) | 20.000 | | | | | | | | |
| Ratio-R | 0.400 | | | | | | | | |
| Summer CV | <input checked="" type="checkbox"/> 0.750 | | | | | | | | |
| Winter CV | <input type="checkbox"/> 0.840 | | | | | | | | |
| Analysis Speed | Normal | | | | | | | | |
| Skip Steady State | <input type="checkbox"/> | | | | | | | | |
| Drain Down Time (mins) | 240 | | | | | | | | |
| Additional Storage (m³/ha) | 20.0 | | | | | | | | |
| <input checked="" type="checkbox"/> Check Discharge Rate(s) | Calc | | | | | | | | |
| <table border="1"> <thead> <tr> <th>Return Period (years)</th> <th>Q (l/s)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>3.7</td> </tr> <tr> <td>30</td> <td>8.8</td> </tr> <tr> <td>100</td> <td>11.1</td> </tr> </tbody> </table> | | Return Period (years) | Q (l/s) | 1 | 3.7 | 30 | 8.8 | 100 | 11.1 |
| Return Period (years) | Q (l/s) | | | | | | | | |
| 1 | 3.7 | | | | | | | | |
| 30 | 8.8 | | | | | | | | |
| 100 | 11.1 | | | | | | | | |
| <input checked="" type="checkbox"/> Check Discharge Volume | Calc | | | | | | | | |
| 100 year 360 minute (m³) | 12 | | | | | | | | |

10.4.4 MRM – Post - Development

| Rainfall Methodology | FSR | | | | | | | | |
|---|---|-----------------------|---------|---|-----|----|-----|-----|------|
| FSR Region | England & Wales | | | | | | | | |
| M5-60 (mm) | 20.000 | | | | | | | | |
| Ratio-R | 0.400 | | | | | | | | |
| Summer CV | <input checked="" type="checkbox"/> 0.750 | | | | | | | | |
| Winter CV | <input type="checkbox"/> 0.840 | | | | | | | | |
| Analysis Speed | Normal | | | | | | | | |
| Skip Steady State | <input type="checkbox"/> | | | | | | | | |
| Drain Down Time (mins) | 240 | | | | | | | | |
| Additional Storage (m³/ha) | 20.0 | | | | | | | | |
| <input checked="" type="checkbox"/> Check Discharge Rate(s) | Calc | | | | | | | | |
| <table border="1"> <thead> <tr> <th>Return Period (years)</th> <th>Q (l/s)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>4.2</td> </tr> <tr> <td>30</td> <td>9.8</td> </tr> <tr> <td>100</td> <td>12.4</td> </tr> </tbody> </table> | | Return Period (years) | Q (l/s) | 1 | 4.2 | 30 | 9.8 | 100 | 12.4 |
| Return Period (years) | Q (l/s) | | | | | | | | |
| 1 | 4.2 | | | | | | | | |
| 30 | 9.8 | | | | | | | | |
| 100 | 12.4 | | | | | | | | |
| <input checked="" type="checkbox"/> Check Discharge Volume | Calc | | | | | | | | |
| 100 year 360 minute (m³) | 13 | | | | | | | | |

10.4.5 Causeway Flow Calculations – With Permeable Paving

| <u>Storage Estimate</u> | | |
|---|--------------------------------------|---------------------------------------|
| Return Period (years) | <input type="text" value="100"/> | <input type="button" value="OK"/> |
| Climate Change (%) | <input type="text" value="40"/> | <input type="button" value="Cancel"/> |
| Impermeable Area (ha) | <input type="text" value="0.028"/> | <input type="button" value="Update"/> |
| Peak Discharge (l/s) | <input type="text" value="1.000"/> | |
| Infiltration Coefficient (m/hr) (leave blank if no infiltration) | <input type="text" value="0.00500"/> | <input type="button" value="Calc"/> |
| Required Storage (m ³) | <input type="button" value="Calc"/> | |
| from | <input type="text" value="8"/> | |
| to | <input type="text" value="12"/> | |
| With infiltration (m ³) | | |
| from | <input type="text" value="8"/> | |
| to | <input type="text" value="12"/> | |

10.4.6 Causeway Flow Storage Calculations – Without Permeable Paving

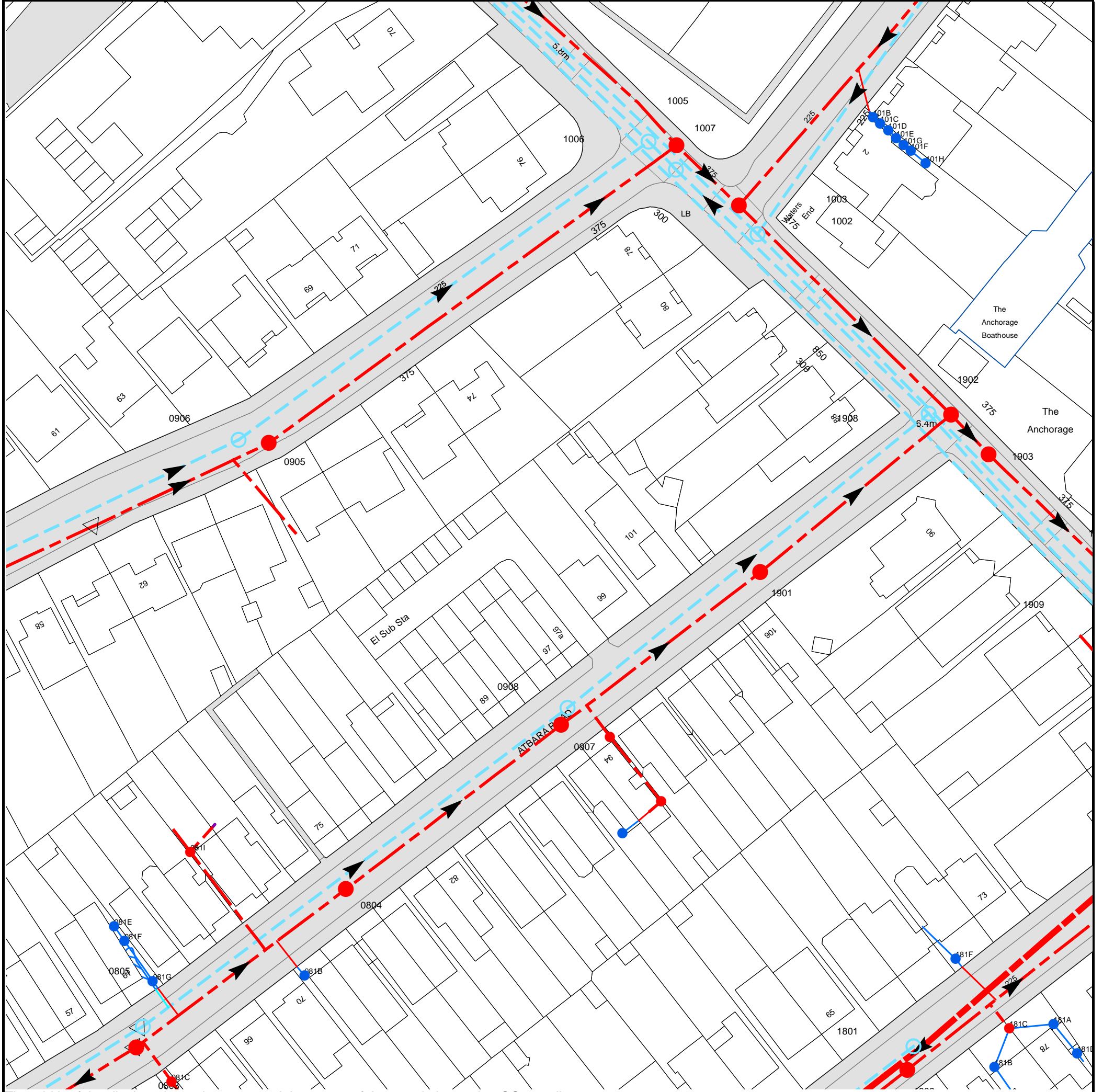
| <u>Storage Estimate</u> | | |
|---|--------------------------------------|---------------------------------------|
| Return Period (years) | <input type="text" value="100"/> | <input type="button" value="OK"/> |
| Climate Change (%) | <input type="text" value="40"/> | <input type="button" value="Cancel"/> |
| Impermeable Area (ha) | <input type="text" value="0.021"/> | <input type="button" value="Update"/> |
| Peak Discharge (l/s) | <input type="text" value="1.000"/> | |
| Infiltration Coefficient (m/hr) (leave blank if no infiltration) | <input type="text" value="0.00500"/> | <input type="button" value="Calc"/> |
| Required Storage (m ³) | <input type="button" value="Calc"/> | |
| from | <input type="text" value="5"/> | |
| to | <input type="text" value="8"/> | |
| With infiltration (m ³) | | |
| from | <input type="text" value="5"/> | |
| to | <input type="text" value="8"/> | |

10.5 Appendix 5 – Drainage

10.5.1 Drainage Asset Search

PDF to follow this page.

Asset Location Search Sewer Map - ALS/ALS Standard/2024 5001962



The width of the displayed area is 200 m and the centre of the map is located at OS coordinates 517083,170948

The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.

Based on the Ordnance Survey Map (2020) with the Sanction of the controller of H.M. Stationery Office, License no. 100019345 Crown Copyright Reserved.

NB. Levels quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates that no survey information is available
















| Manhole Reference | Manhole Cover Level | Manhole Invert Level |
|-------------------|---------------------|----------------------|
| 1006 | n/a | n/a |
| 1007 | n/a | n/a |
| 1005 | n/a | n/a |
| 1003 | n/a | n/a |
| 1002 | n/a | n/a |
| 1901 | n/a | n/a |
| 101B | n/a | n/a |
| 101C | n/a | n/a |
| 101D | n/a | n/a |
| 101E | n/a | n/a |
| 101G | n/a | n/a |
| 101F | n/a | n/a |
| 101H | n/a | n/a |
| 1908 | n/a | n/a |
| 1902 | n/a | n/a |
| 1903 | n/a | n/a |
| 191A | n/a | n/a |
| 081E | n/a | n/a |
| 081F | n/a | n/a |
| 0803 | n/a | n/a |
| 0805 | n/a | n/a |
| 081G | n/a | n/a |
| 081I | n/a | n/a |
| 0906 | n/a | n/a |
| 0905 | n/a | n/a |
| 081B | n/a | n/a |
| 0804 | n/a | n/a |
| 0907 | n/a | n/a |
| 0908 | n/a | n/a |
| 09ZX | n/a | n/a |
| 08ZT | n/a | n/a |
| 18ZY | n/a | n/a |
| 1803 | n/a | n/a |
| 1801 | n/a | n/a |
| 181F | n/a | n/a |
| 181B | n/a | n/a |
| 181C | n/a | n/a |
| 181A | n/a | n/a |
| 181D | n/a | n/a |
| 081C | n/a | n/a |

The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.









Asset Location Search - Sewer Key

Public Sewer Types (Operated and maintained by Thames Water)

-  **Foul Sewer:** A sewer designed to convey waste water from domestic and industrial sources to a treatment works.
-  **Surface Water Sewer:** A sewer designed to convey surface water (e.g. rain water from roofs, yards and car parks) to rivers or watercourses.
-  **Combined Sewer:** A sewer designed to convey both waste water and surface water from domestic and industrial sources to a treatment works.
-  Storm Sewer
-  Sludge Sewer
-  Foul Trunk Sewer
-  Surface Trunk Sewer
-  Combined Trunk Sewer
-  Foul Rising Main
-  Surface Water Rising Main
-  Combined Rising Main
-  Vacuum
-  Thames Water Proposed
-  Vent Pipe
-  Gallery

Other Sewer Types (Not operated and maintained by Thames Water)

-  Sewer
-  Culverted Watercourse
-  Proposed
-  Decommissioned Sewer
-  Content of this drainage network is currently unknown
-  Ownership of this drainage network is currently unknown

Notes:

- 1) All levels associated with the plans are to Ordnance Datum Newlyn.
- 2) All measurements on the plan are metric.
- 3) Arrows (on gravity fed sewers) or flecks (on rising mains) indicate the direction of flow.
- 4) Most private pipes are not shown on our plans, as in the past, this information has not been recorded.

Sewer Fittings

A feature in a sewer that does not affect the flow in the pipe. Example: a vent is a fitting as the function of a vent is to release excess gas.

-  Air Valve
-  Meter
-  Dam Chase
-  Vent
-  Fitting

Operational Controls

A feature in a sewer that changes or diverts the flow in the sewer. Example: A hydrobrake limits the flow passing downstream.

-  Ancillary
-  Drop Pipe
-  Control Valve
-  Weir





End Items

End symbols appear at the start or end of a sewer pipe. Examples: an Undefined End at the start of a sewer indicates that Thames Water has no knowledge of the position of the sewer upstream of that symbol. Outfall on a surface water sewer indicates that the pipe discharges into a stream or river.

-  Inlet
-  Outfall
-  Undefined End




Other Symbols

Symbols used on maps which do not fall under other general categories.

-  Change of Characteristic Indicator
-  Public / Private Pumping Station
-  Invert Level
-  Summit

Areas

Lines denoting areas of underground surveys, etc.

-  Agreement
-  Chamber
-  Operational Site

Ducts or Crossings

-  Casement
 -  Conduit Bridge
 -  Subway
 -  Tunnel
- Ducts may contain high voltage cables. Please check with Thames Water.

5) 'ns' or '0' on a manhole indicates that data is unavailable.

6) The text appearing alongside a sewer line indicates the internal diameter of the pipe in millimeters. Text next to a manhole indicates the manhole reference number and should not be taken as a measurement. If you are unsure about any text or symbology, please contact Property Searches on 0800 009 4540.

10.5.2 Thames Water Drainage Enquiry (2016)

PDF to follow this page.

Residential

The Law Society's CON29DW
Drainage & Water Enquiry



Property
Searches

PALI
27
Woodstock Road
Croydon
CR0 8YD

| | |
|-------------------------|---------------------------------------|
| Search address supplied | 99, Atbara Road, Teddington, TW11 9PA |
| Your reference | 5989 |
| Our reference | DWS/DWS Standard/2016_3333104 |
| Received date | 20 May 2016 |
| Search date | 20 May 2016 |

Important information – changes effective from 9 May ...

The content of the Law Society's CON29DW is being updated to reflect changes to legislation impacting the water industry. In summary, from 9th May the key changes to both the CON29DW and CommercialDW enquiries will be as follows:

1. Inclusion of details on private pumping stations (Q. 2.4.1 and 2.5.1)
2. Impact of sustainable drainage systems (SUDs) on newly adopted sewerage networks (Q. 2.2)
3. Removal of water quality information as this is not property specific; however this information will still be available on individual water companies' web sites (was Q. 3.3)
4. Provision of water hardness information (will become the new Q. 3.5)

For further information please visit www.thameswater-propertysearches.co.uk



Thames Water Utilities Ltd
Property Searches, PO Box 3189, Slough SL1 4WW
DX 151280 Slough 13



searches@thameswater.co.uk
www.thameswater-propertysearches.co.uk



0845 070 9148

CON29DW
DRAINAGE AND WATER ENQUIRY



Residential

CON29DW Drainage & Water Enquiry



Property Searches

Question

Summary Answer

Maps

| | | |
|-----|---|--------------|
| 1.1 | Where relevant, please include a copy of an extract from the public sewer map. | Map Provided |
| 1.2 | Where relevant, please include a copy of an extract from the map of waterworks. | Map Provided |

Drainage

| | | |
|-------|--|-----------------|
| 2.1 | Does foul water from the property drain to a public sewer? | Connected |
| 2.2 | Does surface water from the property drain to a public sewer? | Connected |
| 2.3 | Is a surface water drainage charge payable? | Charge Payable |
| 2.4 | Does the public sewer map indicate any public sewer, disposal main or lateral drain within the boundaries of the property? | No |
| 2.4.1 | Does the public sewer map indicate any public pumping station or any other ancillary apparatus within the boundaries of the property? | No |
| 2.5 | Does the public sewer map indicate any public sewer within 30.48 metres (100 feet) of any buildings within the property? | Yes |
| 2.5.1 | Does the public sewer map indicate any public pumping station or any other ancillary apparatus within the 50metres of any buildings within the property? | No |
| 2.6 | Are any sewers or lateral drains serving, or which are proposed to serve the property, the subject of an existing adoption agreement or an application for such an agreement? | No |
| 2.7 | Has a sewerage undertaker approved or been consulted about any plans to erect a building or extension on the property over or in the vicinity of a public sewer, disposal main or drain? | No |
| 2.8 | Is the building which is or forms part of the property, at risk of internal flooding due to overloaded public sewers? | Not At Risk |
| 2.9 | Please state the distance from the property to the nearest boundary of the nearest sewage treatment works. | 3.54 Kilometres |

Water

| | | |
|-----|--|-----------|
| 3.1 | Is the property connected to mains water supply? | Connected |
| 3.2 | Are there any water mains, resource mains or discharge pipes within the boundaries of the property? | No |
| 3.3 | Is any water main or service pipe serving or which is proposed to serve the property, the subject of an existing adoption agreement or an application for such an agreement? | No |
| 3.4 | Is the property at risk of receiving low water pressure or flow? | No |
| 3.5 | What is the classification of the water supply for the property? | Hard |
| 3.6 | Please include details of the location of any water meter serving the property. | No Meter |

Charging

| | | |
|-------|--|--------------|
| 4.1.1 | Who are the sewerage undertakers for the area? | Thames Water |
| 4.1.2 | Who are the water undertakers for the area? | Thames Water |
| 4.2 | Who bills the property for sewerage services? | Thames Water |
| 4.3 | Who bills the property for water services? | Thames Water |
| 4.4 | What is the current basis for charging for sewerage and/or water services at the property? | See Details |
| 4.5 | Will the basis for charging for sewerage and water services at the property change as a consequence of a change of occupation? | No |

Residential

CON29DW Drainage & Water Enquiry



Property
Searches

Search address supplied: 99, Atbara Road, Teddington, TW11 9PA

Any new owner or occupier will need to contact Thames Water on 0800 316 9800 or log onto our website www.thameswater.co.uk and complete our online form to change the water and drainage services bills to their name.

The following records were searched in compiling this report: - the Map of Public Sewers, the Map of Waterworks, Water and Sewer billing records, Adoption of Public Sewer records, Building Over Public Sewer records, the Register of Properties subject to Internal Foul Flooding, the Register of Properties subject to Poor Water Pressure and the Drinking Water Register. Thames Water Utilities Ltd (TWUL), Clearwater Court, Vastern Road, Reading RG1 8DB, holds all of these.

TWUL, trading as Property Searches, are responsible in respect of the following:-

- (i) any negligent or incorrect entry in the records searched;
- (ii) any negligent or incorrect interpretation of the records searched;
- (iii) and any negligent or incorrect recording of that interpretation in the search report
- (iv) compensation payments

Please refer to the attached Terms & Conditions.



Thames Water Property Searches is an Executive member of CoPSO (Council of Property Search Organisations).

Residential

CON29DW Drainage & Water Enquiry



Property Searches

Interpretation of CON29DW Drainage and Water Search

Appendix 1 contains definitions of terms and expressions used in this report.

For your guidance:

- Thames Water Property Searches Complaints Procedure:
 - Thames Water Property Searches offers a robust complaints procedure. Complaints can be made by telephone, in writing, by email (searches@thameswater.co.uk) or through our website (www.thameswater-propertysearches.co.uk)

As a minimum standard Thames Water Property Searches will:

- endeavour to resolve any contact or complaint at the time of receipt. If this isn't possible, we will advise of timescales;
- investigate and research the matter in detail to identify the issue raised (in some cases third party consultation will be required);
- provide a response to the customer within 10 working days of receipt of the complaint;
- provide compensation, if no response or acknowledgment that we are investigating the case is given within 10 working days of receipt of the complaint;
- keep you informed of the progress and, depending on the scale of investigation required, update with new timescales as necessary;
- provide an amended search, free of charge, if required;
- provide a refund if we find your complaint to be justified; take the necessary action within our power to put things right.

If you want us to liaise with a third party on your behalf, just let us know.

If you are still not satisfied with the outcome provided we will refer the matter to a Senior Manager for resolution who will respond again within 5 working days.

If you remain dissatisfied with our final response you may refer your complaint for consideration under The Property Ombudsman scheme (TPOs). Please refer to the final page of the search for further details.

Residential

CON29DW Drainage & Water Enquiry



Property
Searches

Maps

1.1 – Where relevant, please include a copy of an extract from the public sewer map.

A copy of an extract of the public sewer map is included, showing the public sewers, disposal mains and lateral drains in the vicinity of the property.

For your guidance:

- The Water Industry Act 1991 defines Public Sewers as those which Thames Water have responsibility for. Other assets and rivers, watercourses, ponds, culverts or highway drains may be shown for information purposes only.
- The company is not generally responsible for rivers, watercourses, ponds, culverts or highway drains. If any of these are shown on the copy extract they are shown for information only.
- Any private sewers or lateral drains which are indicated on the extract of the public sewer map as being subject to an agreement under Section 104 of the Water Industry Act 1991 are not an 'as constructed' record. It is recommended these details be checked with the developer.
- Assets other than public sewers may be shown on the copy extract, for information.

1.2 – Where relevant, please include a copy of an extract from the map of waterworks.

A copy of an extract of the map of waterworks is included, showing water mains, resource mains or discharge pipes in the vicinity of the property.

For your guidance:

- The "water mains" in this context are those, which are vested in and maintainable by the water company under statute.
- Assets other than public water mains may be shown on the plan, for information only.
- Water companies are not responsible for private supply pipes connecting the property to the public water main and do not hold details of these. These may pass through land outside of the control of the seller, or may be shared with adjacent properties. The buyer may wish to investigate whether separate rights or easements are needed for their inspection, repair or renewal.
- If an extract of the public water main record is enclosed, this will show known public water mains in the vicinity of the property. It should be possible to estimate the likely length and route of any private water supply pipe connecting the property to the public water network.

Drainage

2.1 – Does foul water from the property drain to a public sewer?

Records indicate that foul water from the property drains to a public sewer.

For your guidance:

- Water companies are not responsible for any private drains that connect the property to the public sewerage system and do not hold details of these. The property owner will normally have sole responsibility for private drains serving the property. These may pass through land outside the control of the seller and the buyer may wish to investigate whether separate rights or easements are needed for their inspection, repair or renewal.
- If foul water does not drain to the public sewerage system, the property may have private facilities in the form of a cesspit, septic tank or other type of treatment plant.
- An extract from the public sewer map is enclosed. This will show known public sewers in the vicinity of the property and it should be possible to estimate the likely length and route of any private drains and/or sewers connecting the property to the public sewerage system.

2.2 – Does surface water from the property drain to a public sewer?

Records indicate that surface water from the property drains to a public sewer.

For your guidance:

- Sewerage Undertakers are not responsible for any private drains that connect the property to the public sewerage system, and do not hold details of these.
- The property owner will normally have sole responsibility for private drains serving the property. These private drains may pass through land outside of the control of the seller and the buyer may wish to investigate whether separate rights or easements are needed for their inspection, repair or renewal.
- In some cases, 'Sewerage Undertakers' records do not distinguish between foul and surface water connections to the public sewerage system.
- At the time of privatisation in 1989, Sewerage Undertakers were sold with poorly-kept records of sewerage infrastructure. The records did not always show which properties were connected for surface water drainage purposes. Accordingly, billing records have been used to provide an answer for this element of the drainage and water search.
- Due to the potential inadequacy of 'Sewerage Undertakers' infrastructure records with respect to surface water drainage, it is the customer's responsibility to inform the Sewerage Undertaker that they do not receive the surface water drainage service. If on inspection, the buyer finds that surface water from the property does not drain to a public sewer, then the property may be eligible for a rebate of the surface water drainage charge. For further information, please contact Thames Water on Tel: 0800 316 9800, or refer to the website at www.thameswater.co.uk.
- If surface water from the property does not drain to the public sewerage system, the property may have private facilities in the form of a soakaway or private connection to a watercourse.
- An extract from the public sewer map is enclosed. This will show known public sewers in the vicinity of the property and it should be possible to estimate the likely length and route of any private drains and/or sewers connecting the property to the public sewerage system.

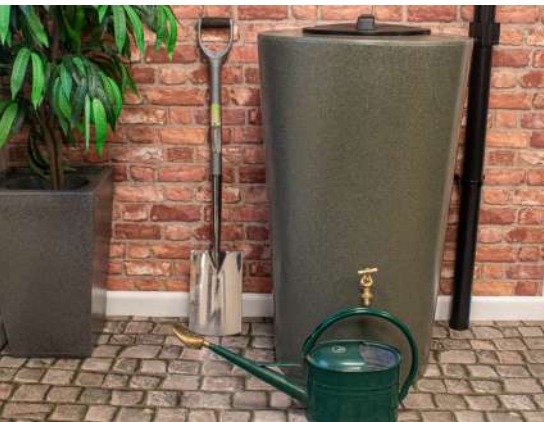
10.6 Appendix 6 – SuDS Suitability Assessment

| SuDS Technique | Typical Uses | Potential Issues | Potential Suitability |
|---|---|--|--|
| Rainwater harvesting | Capture of rainwater into a tank(s) for use (usually non-potable) such as irrigation, toilet flushing, vehicle or plant cleansing. | Care is needed to prevent the development of bacteria, algae and insect infestation. | Suitable – Rainwater Butt |
| Infiltration: Soakaways Infiltrations trenches and basins | Infiltration components are used to capture surface water runoff and allow it to infiltrate (soak) and filter through to the subsoil layer, into the groundwater. | Limited Space away from Foundations; Contamination; Could increase flood risk. Maintenance | Suitable – Partially |
| Green/brown /blue roofs | Used on flat or shallow pitched roofs to provide a durable roof covering which also provides thermal insulation, amenity space, biodiversity habitat as well as attenuation of rainwater. | Maintenance - Ensuring safe access | Suitable – Partially |
| Raingardens | Creation of planted landscaped areas to allow the diversion of a portion of rainwater from either downpipes or surrounding paved surfaces. Raingardens can either allow infiltration into the ground or have tanked systems for water retention. | Space Required; Require maintenance; | Suitable - Partially |
| Permeable pavements / surfaces | Permeable hard surfaces that allow rainwater to pass through either into the ground or to tanked systems. Good as interception storage. | Potential impact of saturation on pavement stability to be considered. May require extensive use of impermeable membranes and under-drainage. Maintenance required. | Suitable – Partial infiltration – Connection to other SuDS features/discharge point; |
| Swales | Dry ditches used as landscape features to allow the storage and infiltration of rainwater. Often used as linear features alongside roads, footpaths or rail lines but capable of being integrated into the design of many open spaces. | Finding available space in proposed site layout | Unsuitable - Space |
| Detention basin/ponds | Landscape features designed to store and in some cases infiltrate rainwater. Detentions basins are usually dry, whereas a pond should retain water. These features need areas of open space but can often be combined with other sustainable drainage techniques. | Potential health and safety issues. Finding available space in proposed site layout | Unsuitable - Space |
| Storage tanks/ Geocellular storage | Usually below ground level, they attenuate rainwater for later slow release back into the drainage system. | Pumping may sometimes be required to empty the tank into the drainage system | Suitable |
| Oversized piping | Using larger than necessary pipework creates additional space to store rainwater. | Lacks the wider benefits of the green infrastructure-based techniques | Suitable |

10.7 Appendix 7 – Details of Proposed Of SuDS

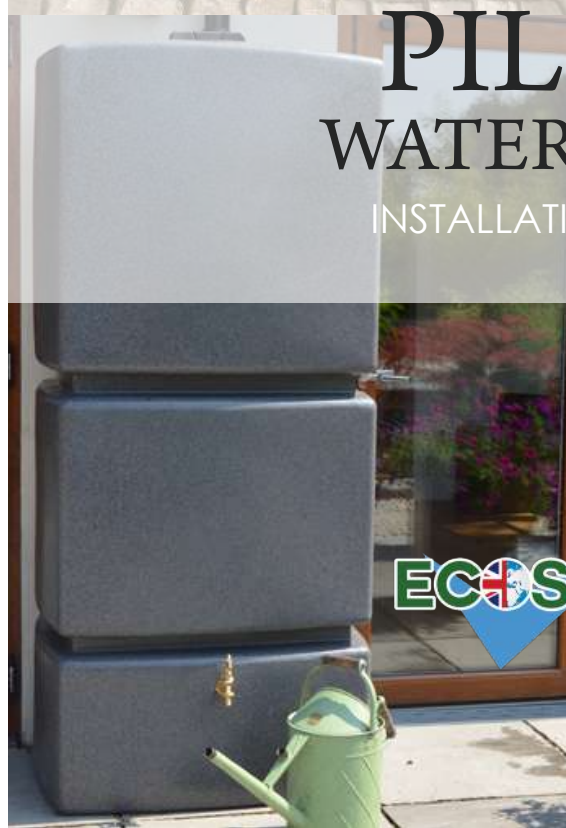
10.7.1 Rainwater Butt

PDF to follow this page.



PILLAR WATER BUTTS

INSTALLATION GUIDE



Ecosure
Efills Ltd
Unit 1, Whiting Way
Melbourn, Royston
SG8 6NA

Phone: 01763 261781
Email: sales@ecosure.co.uk
Website: www.ecosure.co.uk



EC+SURE

THANK YOU

Thank you for purchasing the Ecosure Pillar Water Butt. We hope that you are happy with your purchase.

Although your water butt has been tested in accordance with our quality control procedures, please check it thoroughly to ensure that no damage has occurred in transit and report any damage within 48 hours of delivery.

PLEASE NOTE

The hole at the front of the 525 litre mini pillar water butt is part of the manufacturing process and is not intended to be used as an inlet or outlet. It is covered when the lid is in place.



IMPORTANT SAFETY INSTRUCTIONS.

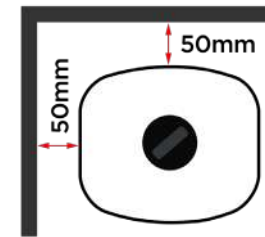
- When fixing your tap or valve to the brass moulded outlets, use 4 or 5 layers of PTFE tape and **DO NOT OVERTIGHTEN**. Hand tighten only; do not use a spanner or wrench.
- When using any power tools, be aware of others around you and wear suitable PPE.

PILLAR WATER BUTT INSTALLATION GUIDE

- a. The water butt must be sited on a flat, level paved or concrete base.



- b. Please leave at least a 50mm gap all around the water butt. This will allow for the natural expansion of the water butt when full of water. In particular, be sure to leave at least 50mm between the centre of the back of the water butt and any wall it is sited against.



- c. Choose which threaded outlet you wish to use and drill out the plastic behind the brass insert using a hole-saw or a spade bit. **Be careful not to damage the outlet itself.**

- d. When fixing a tap or a hose connector to a threaded outlet, use PTFE tape and do not overtighten. If the tap points in the wrong direction after tightening, more tape is required. We recommend about 5 full turns of PTFE tape as a good starting point.

- e. Rainwater diverters can be installed approximately 40mm below the top of the water butt and away from edges and corners. Please remember to keep the connecting hose running from the water butt to the down-pipe level, to act as an overflow.

10.7.2 SuDS Planters

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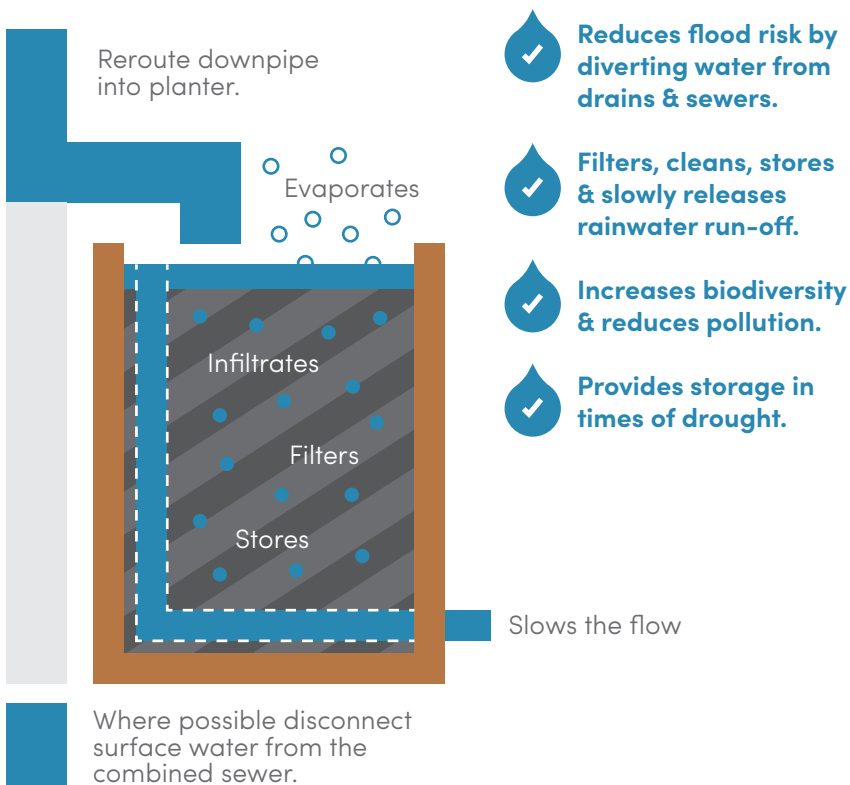
Meet the SuDSPlanter



SuDSPlanter is a uniquely designed rain garden which captures rainwater runoff from roofs, rather than leaving it to flow into the drains and sewers, potentially overloading the system. It's a cleaner, greener more sustainable way to guard against today's increasing risk of flooding and contamination.

The SuDSPlanter provides water storage in dry or drought conditions, as well as storm storage designed to cope in wet environments. This makes the planter ideal for our changing weather patterns, combatting the increasing flood risk and water scarcity which we face.

How it works



The SuDSPlanter is designed to capture rainwater run-off from roofs by rerouting the downpipe into the planter instead of directly into the drains. The planter is made up of a series of layers, acting as both a sponge and a natural filter, attenuating flow and removing sediment and bird poo as the water soaks through to the reservoir below.

Our specially designed growing media provides the perfect environment for plants to thrive; nutrient and water retention, filtration and soil volume to sustain plant growth in both wet and dry conditions.

Options



Recycled lumber

These are manufactured using a plastic coated metal frame with recycled plastic lumber infills. All materials are 100% recycled or recyclable.

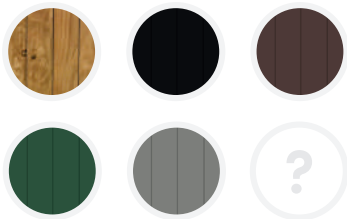
Sizes

1200mm x 600mm x 950mm

1600mm x 600mm x 950mm

2000mm x 600mm x 950mm

Colours



Bespoke colours available on request.



100% recycled materials.



No treatment required prior to use.



Minimum 15 year life expectancy.



Fully recyclable at the end of its use.



Graffiti resistant.

Installation

For DIY installations, we provide an instruction manual with your planter, which has handy maintenance tips too. If you would like us to install your SuDSPlanter for you, simply ask us when you place your order



Solid timber

Our timber planters are made from the finest water resistant softwoods naturally impregnated with natural oils to reduce the need for tanalith.

Sizes

1200mm x 600mm x 950mm

1600mm x 600mm x 950mm

Colours



Bespoke colours available on request.



UK sourced, FSC accredited wood.



No treatment required prior to use.



Minimum 15 year life expectancy.



Fully recyclable at the end of its use.

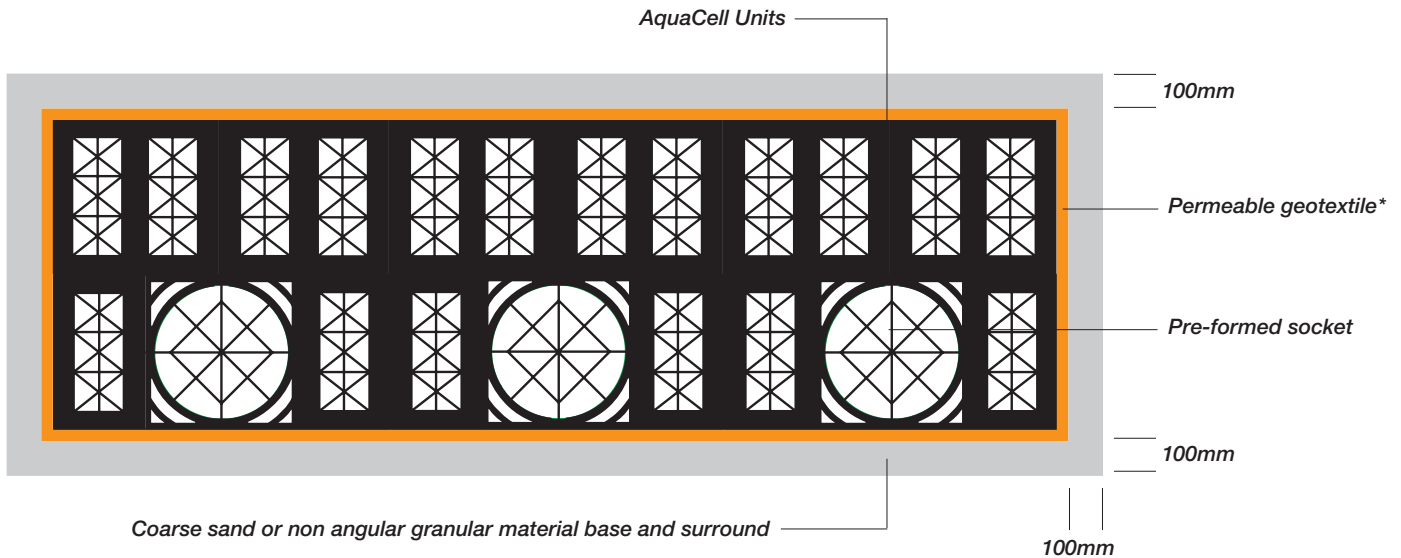
Planting

Your SuDSPlanter is a great way to increase biodiversity, as it works best with as wide a variety of plants as possible. For the best results, choose from our list of suitable plants, or we can supply you with a selection of young plants for establishing: simply ask when you place your order.

10.7.3 Geocellular Storage

PDF to follow this page.

Guidance Note 1 – Typical Soakaway Installation Method



Example shows the use of AquaCell Eco. However, a soakaway can also be installed as shown using either of the other versions of AquaCell units (Prime, Core or Plus) as appropriate.

* The geotextile should be selected according to specific site conditions. Typically, however, a 300g non-woven material will be suitable. Specialist advice should be sought if surrounding soil characteristics exhibit a high degree of fines/low infiltration capacity and/or there is a high risk of damage from ground contaminants.

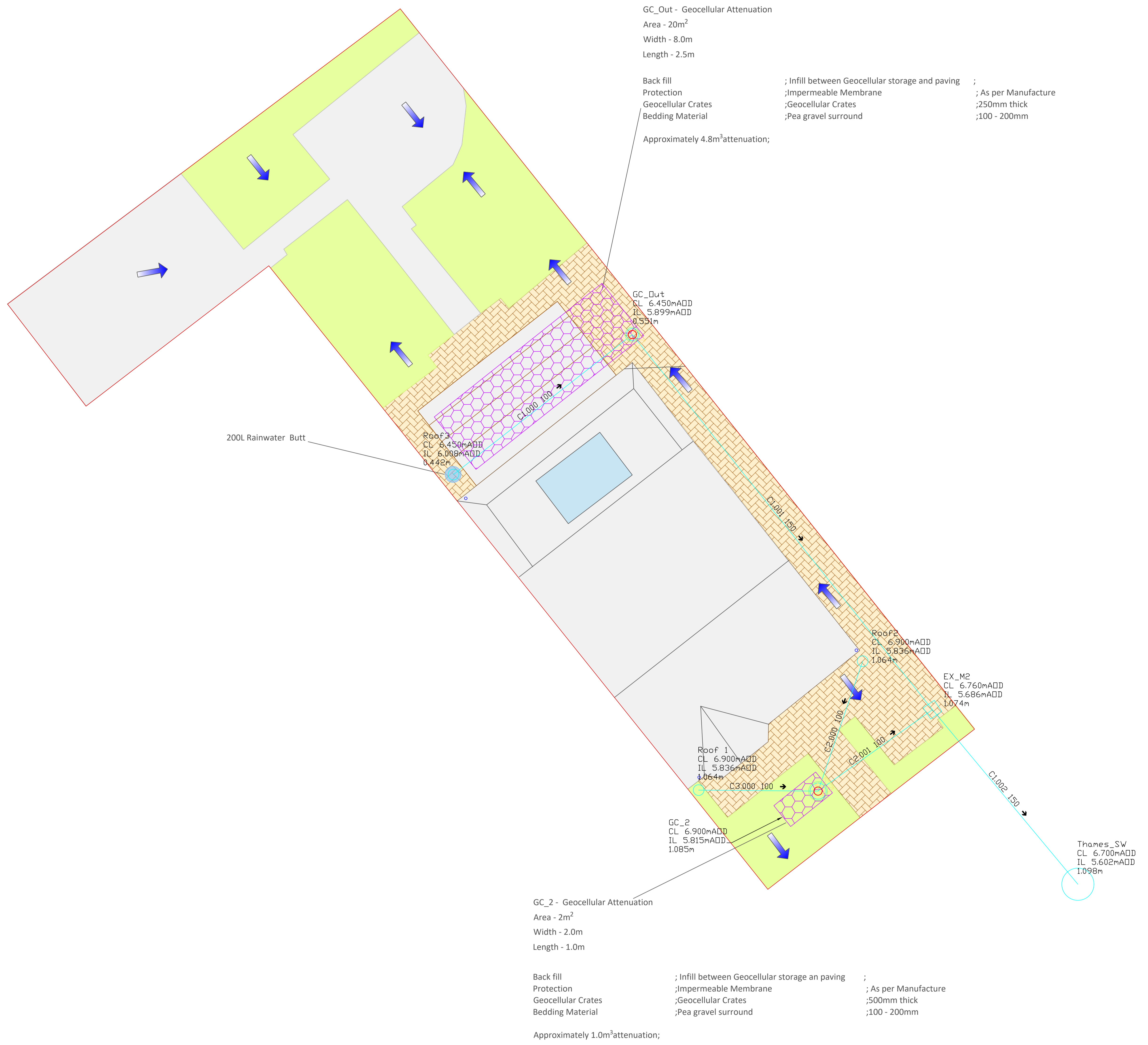
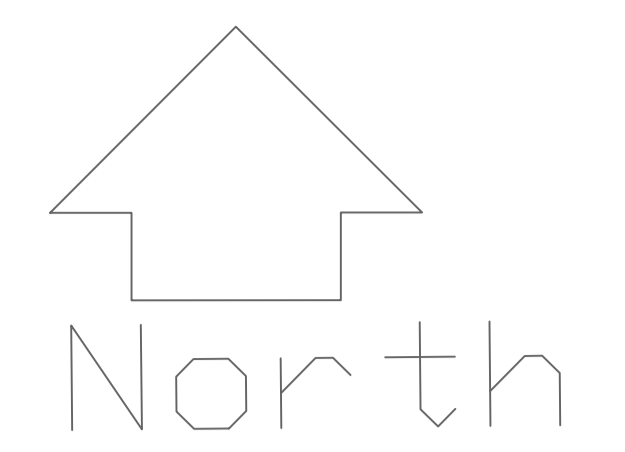
Typical Installation Procedure

1. Excavate the trench to the required depth ensuring that the plan area is slightly greater than that of the AquaCell units.
2. Lay 100mm bed of coarse sand or non angular granular material, level and compact.
3. Lay the geotextile* over the base and up the sides of the trench.
4. Lay the AquaCell units parallel with each other. In multiple layer applications, wherever possible, continuous vertical joints should be avoided. AquaCell units can be laid in a 'brick bonded' formation (i.e. to overlap the joints below). For single layer applications use the AquaCell Clips and for multi layers use the AquaCell Clips and the AquaCell Shear Connectors (vertical rods).
5. Fix the Adaptors to the AquaCell units as required and connect pipework.
6. In order to prevent silt from entering the tank, clogging inlet pipework and reducing storage capacity, it is recommended that the Domestic Silt Trap (6LB300) or the standard Silt Trap (6LB600) is installed prior to the inlet pipework.
7. Wrap and overlap the geotextile covering the entire AquaCell structure.
8. Lay 100mm of coarse sand or non angular granular material between the trench walls and the AquaCell structure and compact.
9. Lay 100mm of coarse sand or non angular granular material over the geotextile and compact.
10. Backfill with suitable material.
11. Rainwater from roof areas may discharge directly into the soakaway but rainwater from carparks must discharge through a catchpit manhole and/or a petrol interceptor.

10.8 Appendix 7 - Drainage Modelling

10.8.1 Drainage Layout

PDF to follow this page.



Project :SWDS - 2024 - 000036
 Site :99 Atbara Road,
 :Teddington
 :TW11 9PA
 Company :STM Environmental
 Client :Jamie and Beverley McDaid
 Issue :No.1.0
 By :Georgia Travers

Map Legend

| | | | | | |
|--|----------------------------------|--|--------------------------------------|--|-----------------------|
| | Surface Water Manhole | | Soft Landscaping | | Surface Water Pipe |
| | Surface Water Inspection Manhole | | Permeable Paving | | Perforated Pipe |
| | Flow Control Chamber | | Hardstanding (Impermeable Catchment) | | Slot Drainage Channel |
| | Rainwater Down Pipe | | Geocellular Storage | | Overflow Flow Route |
| | Rainwater Butt | | | | |

10.8.2 Drainage Results

PDF to follow this page.

Design Settings

| | | | |
|-----------------------|-------------------|--------------------------------------|---------------|
| Rainfall Methodology | FSR | Maximum Time of Concentration (mins) | 30.00 |
| Return Period (years) | 100 | Maximum Rainfall (mm/hr) | 50.0 |
| Additional Flow (%) | 0 | Minimum Velocity (m/s) | 1.00 |
| FSR Region | England and Wales | Connection Type | Level Soffits |
| M5-60 (mm) | 20.000 | Minimum Backdrop Height (m) | 0.200 |
| Ratio-R | 0.400 | Preferred Cover Depth (m) | 1.200 |
| CV | 0.750 | Include Intermediate Ground | ✓ |
| Time of Entry (mins) | 5.00 | Enforce best practice design rules | x |

Adoptable Manhole Type

| | | | |
|-----------------------|----------------------|-----------------------|----------------------|
| Max Width (mm) | Diameter (mm) | Max Width (mm) | Diameter (mm) |
| 374 | 1200 | 749 | 1500 |
| 499 | 1350 | 900 | 1800 |

>900 Link+900 mm

| | | | |
|----------------------|----------------------|----------------------|----------------------|
| Max Depth (m) | Diameter (mm) | Max Depth (m) | Diameter (mm) |
| 1.500 | 1050 | 99.999 | 1200 |

Circular Link Type

| | | | |
|---------|----------|---------------------|----|
| Shape | Circular | Auto Increment (mm) | 75 |
| Barrels | 1 | Follow Ground | x |

Available Diameters (mm)

100 | 150

Nodes

| Name | Area (ha) | T of E (mins) | Cover Level (m) | Diameter (mm) | Width (mm) | Easting (m) | Northing (m) | Depth (m) |
|-----------|-----------|---------------|-----------------|---------------|------------|-------------|--------------|-----------|
| Roof3 | 0.016 | 5.00 | 6.450 | 400 | | 517081.188 | 170946.540 | 0.692 |
| EX_M2 | | | 6.760 | 500 | 500 | 517099.372 | 170937.337 | 1.074 |
| Thames_SW | | | 6.700 | 1200 | | 517104.795 | 170930.827 | 1.098 |
| GC_Out | | | 6.450 | 450 | | 517088.279 | 170951.651 | 0.801 |
| GC_2 | | | 6.900 | 600 | | 517095.103 | 170934.301 | 1.335 |
| Roof 1 | 0.002 | 5.00 | 6.900 | 400 | | 517090.649 | 170934.338 | 1.064 |
| Roof2 | 0.003 | 5.00 | 6.900 | 400 | | 517096.768 | 170939.143 | 1.064 |

Links

| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
|-------|---------|-----------|------------|-------------|-----------|-----------|----------|-------------|----------|---------------|--------------|
| 1.000 | Roof3 | GC_Out | 8.741 | 0.600 | 6.008 | 5.899 | 0.109 | 80.0 | 100 | 5.17 | 50.0 |
| 1.001 | GC_Out | EX_M2 | 18.110 | 0.600 | 5.900 | 5.686 | 0.214 | 84.6 | 150 | 5.45 | 50.0 |
| 2.000 | Roof2 | GC_2 | 5.120 | 0.600 | 5.836 | 5.815 | 0.021 | 243.8 | 100 | 5.17 | 50.0 |
| 3.000 | Roof 1 | GC_2 | 4.454 | 0.600 | 5.836 | 5.815 | 0.021 | 212.1 | 100 | 5.14 | 50.0 |
| 2.001 | GC_2 | EX_M2 | 5.238 | 0.600 | 5.815 | 5.686 | 0.129 | 40.6 | 100 | 5.25 | 50.0 |
| 1.002 | EX_M2 | Thames_SW | 8.472 | 0.600 | 5.686 | 5.602 | 0.084 | 100.9 | 150 | 5.59 | 50.0 |

| Name | Vel (m/s) | Cap (l/s) | Flow (l/s) | US Depth (m) | DS Depth (m) | Σ Area (ha) | Σ Add Inflow (l/s) | Pro Depth (mm) | Pro Velocity (m/s) |
|-------|-----------|-----------|------------|--------------|--------------|-------------|--------------------|----------------|--------------------|
| 1.000 | 0.861 | 6.8 | 2.2 | 0.342 | 0.451 | 0.016 | 0.0 | 39 | 0.764 |
| 1.001 | 1.093 | 19.3 | 2.2 | 0.400 | 0.924 | 0.016 | 0.0 | 34 | 0.722 |
| 2.000 | 0.488 | 3.8 | 0.4 | 0.964 | 0.985 | 0.003 | 0.0 | 22 | 0.316 |
| 3.000 | 0.524 | 4.1 | 0.3 | 0.964 | 0.985 | 0.002 | 0.0 | 18 | 0.293 |
| 2.001 | 1.213 | 9.5 | 0.7 | 0.985 | 0.974 | 0.005 | 0.0 | 18 | 0.704 |
| 1.002 | 1.000 | 17.7 | 2.8 | 0.924 | 0.948 | 0.021 | 0.0 | 41 | 0.736 |

Pipeline Schedule






| Link | Length (m) | Slope (1:X) | Dia (mm) | Link Type | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) |
|-------|------------|-------------|----------|-----------|-----------|-----------|--------------|-----------|-----------|--------------|
| 1.000 | 8.741 | 80.0 | 100 | Circular | 6.450 | 6.008 | 0.342 | 6.450 | 5.899 | 0.451 |
| 1.001 | 18.110 | 84.6 | 150 | Circular | 6.450 | 5.900 | 0.400 | 6.760 | 5.686 | 0.924 |
| 2.000 | 5.120 | 243.8 | 100 | Circular | 6.900 | 5.836 | 0.964 | 6.900 | 5.815 | 0.985 |
| 3.000 | 4.454 | 212.1 | 100 | Circular | 6.900 | 5.836 | 0.964 | 6.900 | 5.815 | 0.985 |
| 2.001 | 5.238 | 40.6 | 100 | Circular | 6.900 | 5.815 | 0.985 | 6.760 | 5.686 | 0.974 |
| 1.002 | 8.472 | 100.9 | 150 | Circular | 6.760 | 5.686 | 0.924 | 6.700 | 5.602 | 0.948 |

| Link | US Node | Dia (mm) | Width (mm) | Node Type | MH Type | DS Node | Dia (mm) | Width (mm) | Node Type | MH Type |
|-------|---------|----------|------------|-----------|-----------|-----------|----------|------------|-----------|-----------|
| 1.000 | Roof3 | 400 | | Manhole | Adoptable | GC_Out | 450 | | Manhole | Adoptable |
| 1.001 | GC_Out | 450 | | Manhole | Adoptable | EX_M2 | 500 | 500 | Manhole | Adoptable |
| 2.000 | Roof2 | 400 | | Manhole | Adoptable | GC_2 | 600 | | Manhole | Adoptable |
| 3.000 | Roof 1 | 400 | | Manhole | Adoptable | GC_2 | 600 | | Manhole | Adoptable |
| 2.001 | GC_2 | 600 | | Manhole | Adoptable | EX_M2 | 500 | 500 | Manhole | Adoptable |
| 1.002 | EX_M2 | 500 | 500 | Manhole | Adoptable | Thames_SW | 1200 | | Manhole | Adoptable |

Manhole Schedule

| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Width (mm) | Connections | Link | IL (m) | Dia (mm) | |
|-----------|-------------|--------------|--------|-----------|----------|------------|-------------|------|--------|----------|-----|
| Roof3 | 517081.188 | 170946.540 | 6.450 | 0.692 | 400 | | | | | | |
| EX_M2 | 517099.372 | 170937.337 | 6.760 | 1.074 | 500 | 500 | | 0 | 1.000 | 6.008 | 100 |
| | | | | | | | | 1 | 2.001 | 5.686 | 100 |
| Thames_SW | 517104.795 | 170930.827 | 6.700 | 1.098 | 1200 | | | 2 | 1.001 | 5.686 | 150 |
| | | | | | | | | 0 | 1.002 | 5.686 | 150 |
| Thames_SW | 517104.795 | 170930.827 | 6.700 | 1.098 | 1200 | | | 1 | 1.002 | 5.602 | 150 |
| | | | | | | | | | | | |

Manhole Schedule

| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Width (mm) | Connections | Link | IL (m) | Dia (mm) |
|--------|-------------|--------------|--------|-----------|----------|------------|--|----------------|----------------|------------|
| GC_Out | 517088.279 | 170951.651 | 6.450 | 0.801 | 450 | |  1 | 1.000 | 5.899 | 100 |
| GC_2 | 517095.103 | 170934.301 | 6.900 | 1.335 | 600 | |  1 2 | 1.001 2.000 | 5.900 5.815 | 150 100 |
| Roof 1 | 517090.649 | 170934.338 | 6.900 | 1.064 | 400 | |  0 | 2.001 | 5.815 | 100 |
| Roof2 | 517096.768 | 170939.143 | 6.900 | 1.064 | 400 | |  0 | 3.000 | 5.836 | 100 |
| | | | | | | |  0 | 2.000 | 5.836 | 100 |

Simulation Settings

| | | | |
|------------------------|-------------------|---|------|
| Rainfall Methodology | FSR | Additional Storage (m ³ /ha) | 20.0 |
| FSR Region | England and Wales | Check Discharge Rate(s) | ✓ |
| M5-60 (mm) | 20.000 | 1 year (l/s) | 4.2 |
| Ratio-R | 0.400 | 30 year (l/s) | 9.8 |
| Summer CV | 0.750 | 100 year (l/s) | 12.4 |
| Analysis Speed | Normal | Check Discharge Volume | ✓ |
| Skip Steady State | x | 100 year 360 minute (m ³) | 13 |
| Drain Down Time (mins) | 240 | | |

Storm Durations

15 | 60 | 360 | 2160

| Return Period (years) | Climate Change (CC %) | Additional Area (A %) | Additional Flow (Q %) |
|-----------------------|-----------------------|-----------------------|-----------------------|
| 1 | 0 | 0 | 0 |
| 30 | 0 | 0 | 0 |
| 100 | 0 | 0 | 0 |
| 100 | 40 | 0 | 0 |

Pre-development Discharge Rate

| | | | |
|------------------------|------------|------------------------------|------|
| Site Makeup | Brownfield | Time of Concentration (mins) | 5.00 |
| Brownfield Method | MRM | Betterment (%) | 0 |
| Contributing Area (ha) | 0.028 | Q 1 year (l/s) | 4.2 |
| PIMP (%) | 100 | Q 30 year (l/s) | 9.8 |
| CV | 0.750 | Q 100 year (l/s) | 12.4 |

Pre-development Discharge Volume

| | | | | | |
|------------------------|------------|-----------------------|-------|---------------------------------|-------|
| Site Makeup | Brownfield | CV | 0.750 | Betterment (%) | 0 |
| Brownfield Method | MRM | Return Period (years) | 100 | PR | 0.750 |
| Contributing Area (ha) | 0.028 | Climate Change (%) | 0 | Runoff Volume (m ³) | 13 |
| PIMP (%) | 100 | Storm Duration (mins) | 360 | | |

Node GC Out Online Orifice Control

| | | | | | |
|--------------------------|-------|-------------------|-------|-----------------------|-------|
| Flap Valve | x | Design Depth (m) | 0.350 | Discharge Coefficient | 0.600 |
| Replaces Downstream Link | ✓ | Design Flow (l/s) | 1.0 | | |
| Invert Level (m) | 5.900 | Diameter (m) | 0.028 | | |

Node GC_2 Online Orifice Control

| | | | | | |
|--------------------------|-------|-------------------|-------|-----------------------|-------|
| Flap Valve | x | Invert Level (m) | 5.815 | Diameter (m) | 0.021 |
| Downstream Link | 2.001 | Design Depth (m) | 1.000 | Discharge Coefficient | 0.600 |
| Replaces Downstream Link | ✓ | Design Flow (l/s) | 1.0 | | |

Node GC Out Depth/Area Storage Structure

| | | | | | |
|-----------------------------|---------|---------------|------|---------------------------|-------|
| Base Inf Coefficient (m/hr) | 0.00500 | Safety Factor | 2.0 | Invert Level (m) | 5.899 |
| Side Inf Coefficient (m/hr) | 0.00500 | Porosity | 0.95 | Time to half empty (mins) | 77 |

| Depth (m) | Area (m ²) | Inf Area (m ²) | Depth (m) | Area (m ²) | Inf Area (m ²) | Depth (m) | Area (m ²) | Inf Area (m ²) |
|-----------|------------------------|----------------------------|-----------|------------------------|----------------------------|-----------|------------------------|----------------------------|
| 0.000 | 20.0 | 12.0 | 0.250 | 20.0 | 24.0 | 0.251 | 0.0 | 24.0 |

Node GC_2 Depth/Area Storage Structure

| | | | | | |
|-----------------------------|---------|---------------|------|---------------------------|-------|
| Base Inf Coefficient (m/hr) | 0.00500 | Safety Factor | 2.0 | Invert Level (m) | 5.815 |
| Side Inf Coefficient (m/hr) | 0.00500 | Porosity | 0.95 | Time to half empty (mins) | 14 |

| Depth (m) | Area (m ²) | Inf Area (m ²) | Depth (m) | Area (m ²) | Inf Area (m ²) | Depth (m) | Area (m ²) | Inf Area (m ²) |
|-----------|------------------------|----------------------------|-----------|------------------------|----------------------------|-----------|------------------------|----------------------------|
| 0.000 | 2.0 | 6.0 | 0.500 | 2.0 | 6.0 | 0.501 | 0.0 | 7.0 |

Other (defaults)

| | | | | | |
|----------------------|-------|-----------------------|-------|--------------------------|-------|
| Entry Loss (manhole) | 0.250 | Entry Loss (junction) | 0.000 | Apply Recommended Losses | x |
| Exit Loss (manhole) | 0.250 | Exit Loss (junction) | 0.000 | Flood Risk (m) | 0.300 |

Approval Settings

| | | | |
|----------------------------------|---------|--|-------|
| Node Size | ✓ | Proportional Velocity | ✓ |
| Node Losses | ✓ | Return Period (years) | 100 |
| Link Size | ✓ | Minimum Proportional Velocity (m/s) | 0.750 |
| Minimum Diameter (mm) | 150 | Maximum Proportional Velocity (m/s) | 3.000 |
| Link Length | ✓ | Surcharged Depth | ✓ |
| Maximum Length (m) | 100.000 | Return Period (years) | 100 |
| Coordinates | ✓ | Maximum Surcharged Depth (m) | 0.100 |
| Accuracy (m) | 1.000 | Flooding | ✓ |
| Crossings | ✓ | Return Period (years) | 30 |
| Cover Depth | ✓ | Time to Half Empty | ✓ |
| Minimum Cover Depth (m) | 1.200 | Return Period (years) | 60 |
| Maximum Cover Depth (m) | 3.000 | Discharge Rates | ✓ |
| Backdrops | ✓ | 1 year (l/s) | 2.0 |
| Minimum Backdrop Height (m) | 0.200 | 30 year (l/s) | 2.0 |
| Maximum Backdrop Height (m) | 1.500 | 100 year (l/s) | 2.0 |
| Full Bore Velocity | ✓ | Discharge Volume | ✓ |
| Minimum Full Bore Velocity (m/s) | 1.000 | 100 year +40% 360 minute (m ³) | 20 |
| Maximum Full Bore Velocity (m/s) | 3.000 | | |

Rainfall

| Event | Peak Intensity (mm/hr) | Average Intensity (mm/hr) | Event | Peak Intensity (mm/hr) | Average Intensity (mm/hr) |
|----------------------------|-------------------------------|----------------------------------|-------------------------------------|-------------------------------|----------------------------------|
| 1 year 15 minute summer | 109.521 | 30.991 | 100 year 15 minute summer | 348.738 | 98.681 |
| 1 year 60 minute summer | 48.435 | 12.800 | 100 year 60 minute summer | 153.288 | 40.510 |
| 1 year 360 minute summer | 14.169 | 3.646 | 100 year 360 minute summer | 40.484 | 10.418 |
| 1 year 2160 minute summer | 3.574 | 0.988 | 100 year 2160 minute summer | 9.021 | 2.493 |
| 30 year 15 minute summer | 268.706 | 76.035 | 100 year +40% CC 15 minute summer | 488.233 | 138.153 |
| 30 year 60 minute summer | 116.589 | 30.811 | 100 year +40% CC 60 minute summer | 214.603 | 56.713 |
| 30 year 360 minute summer | 31.221 | 8.034 | 100 year +40% CC 360 minute summer | 56.677 | 14.585 |
| 30 year 2160 minute summer | 7.160 | 1.979 | 100 year +40% CC 2160 minute summer | 12.630 | 3.490 |

Results for 1 year Critical Storm Duration. Lowest mass balance: 100.00%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m ³) | Flood (m ³) | Status |
|------------------|-----------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|--------|
| 15 minute summer | Roof3 | 9 | 6.051 | 0.043 | 2.1 | 0.0367 | 0.0000 | OK |
| 60 minute summer | EX_M2 | 42 | 5.704 | 0.018 | 0.5 | 0.0044 | 0.0000 | OK |
| 60 minute summer | Thames_SW | 42 | 5.619 | 0.017 | 0.5 | 0.0000 | 0.0000 | OK |
| 60 minute summer | GC_Out | 43 | 5.952 | 0.053 | 1.4 | 1.0067 | 0.0000 | OK |
| 60 minute summer | GC_2 | 41 | 5.869 | 0.054 | 0.4 | 0.1175 | 0.0000 | OK |
| 60 minute summer | Roof 1 | 38 | 5.869 | 0.033 | 0.2 | 0.0054 | 0.0000 | OK |
| 60 minute summer | Roof2 | 40 | 5.869 | 0.033 | 0.3 | 0.0060 | 0.0000 | OK |

| Link Event (Upstream Depth) | US Node | Link | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m ³) | Discharge Vol (m ³) |
|-----------------------------|---------|--------------|-----------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute summer | Roof3 | 1.000 | GC_Out | 2.1 | 1.070 | 0.312 | 0.0205 | |
| 60 minute summer | EX_M2 | 1.002 | Thames_SW | 0.5 | 0.439 | 0.029 | 0.0098 | 1.8 |
| 60 minute summer | GC_Out | Orifice | EX_M2 | 0.3 | | | | |
| 60 minute summer | GC_Out | Infiltration | | 0.0 | | | | |
| 60 minute summer | GC_2 | Orifice | EX_M2 | 0.2 | | | | |
| 60 minute summer | GC_2 | Infiltration | | 0.0 | | | | |
| 60 minute summer | Roof 1 | 3.000 | GC_2 | 0.2 | 0.173 | 0.045 | 0.0146 | |
| 60 minute summer | Roof2 | 2.000 | GC_2 | 0.3 | 0.334 | 0.068 | 0.0167 | |

Results for 30 year Critical Storm Duration. Lowest mass balance: 100.00%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m ³) | Flood (m ³) | Status |
|------------------|-----------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 15 minute summer | Roof3 | 10 | 6.080 | 0.072 | 5.3 | 0.0611 | 0.0000 | OK |
| 60 minute summer | EX_M2 | 44 | 5.709 | 0.023 | 0.9 | 0.0058 | 0.0000 | OK |
| 60 minute summer | Thames_SW | 44 | 5.625 | 0.023 | 0.9 | 0.0000 | 0.0000 | OK |
| 60 minute summer | GC_Out | 47 | 6.032 | 0.133 | 3.5 | 2.5396 | 0.0000 | OK |
| 60 minute summer | GC_2 | 41 | 5.952 | 0.137 | 0.7 | 0.2999 | 0.0000 | SURCHARGED |
| 60 minute summer | Roof 1 | 41 | 5.952 | 0.116 | 0.4 | 0.0190 | 0.0000 | SURCHARGED |
| 60 minute summer | Roof2 | 41 | 5.952 | 0.116 | 0.7 | 0.0212 | 0.0000 | SURCHARGED |

| Link Event (Upstream Depth) | US Node | Link | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m ³) | Discharge Vol (m ³) |
|-----------------------------|---------|--------------|-----------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute summer | Roof3 | 1.000 | GC_Out | 5.3 | 1.178 | 0.778 | 0.0510 | |
| 60 minute summer | EX_M2 | 1.002 | Thames_SW | 0.9 | 0.517 | 0.050 | 0.0145 | 4.7 |
| 60 minute summer | GC_Out | Orifice | EX_M2 | 0.6 | | | | |
| 60 minute summer | GC_Out | Infiltration | | 0.0 | | | | |
| 60 minute summer | GC_2 | Orifice | EX_M2 | 0.3 | | | | |
| 60 minute summer | GC_2 | Infiltration | | 0.0 | | | | |
| 60 minute summer | Roof 1 | 3.000 | GC_2 | 0.2 | 0.131 | 0.056 | 0.0348 | |
| 60 minute summer | Roof2 | 2.000 | GC_2 | 0.5 | 0.334 | 0.130 | 0.0401 | |

Results for 100 year Critical Storm Duration. Lowest mass balance: 100.00%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m ³) | Flood (m ³) | Status |
|------------------|-----------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 15 minute summer | Roof3 | 10 | 6.097 | 0.089 | 6.8 | 0.0760 | 0.0000 | OK |
| 60 minute summer | EX_M2 | 45 | 5.711 | 0.025 | 1.0 | 0.0063 | 0.0000 | OK |
| 60 minute summer | Thames_SW | 45 | 5.627 | 0.025 | 1.0 | 0.0000 | 0.0000 | OK |
| 60 minute summer | GC_Out | 49 | 6.075 | 0.176 | 4.6 | 3.3795 | 0.0000 | SURCHARGED |
| 60 minute summer | GC_2 | 42 | 6.009 | 0.194 | 0.9 | 0.4233 | 0.0000 | SURCHARGED |
| 60 minute summer | Roof 1 | 42 | 6.009 | 0.173 | 0.6 | 0.0282 | 0.0000 | SURCHARGED |
| 60 minute summer | Roof2 | 42 | 6.009 | 0.173 | 0.9 | 0.0315 | 0.0000 | SURCHARGED |

| Link Event (Upstream Depth) | US Node | Link | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m ³) | Discharge Vol (m ³) |
|-----------------------------|---------|--------------|-----------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute summer | Roof3 | 1.000 | GC_Out | 6.7 | 1.203 | 0.991 | 0.0634 | |
| 60 minute summer | EX_M2 | 1.002 | Thames_SW | 1.0 | 0.542 | 0.059 | 0.0164 | 6.2 |
| 60 minute summer | GC_Out | Orifice | EX_M2 | 0.7 | | | | |
| 60 minute summer | GC_Out | Infiltration | | 0.0 | | | | |
| 60 minute summer | GC_2 | Orifice | EX_M2 | 0.4 | | | | |
| 60 minute summer | GC_2 | Infiltration | | 0.0 | | | | |
| 60 minute summer | Roof 1 | 3.000 | GC_2 | 0.3 | 0.228 | 0.077 | 0.0348 | |
| 60 minute summer | Roof2 | 2.000 | GC_2 | 0.6 | 0.327 | 0.160 | 0.0401 | |

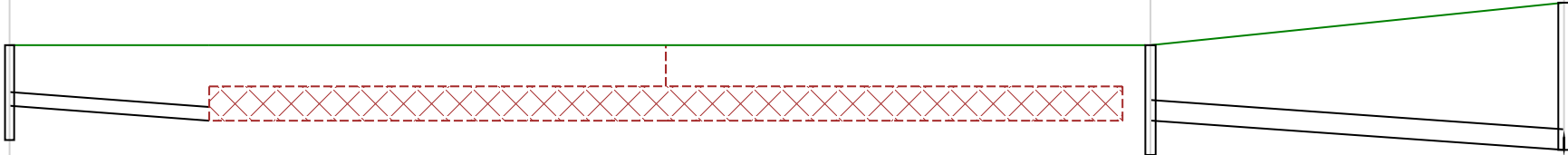
Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%

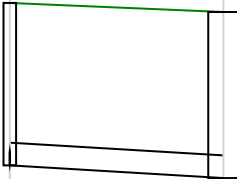
| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m ³) | Flood (m ³) | Status |
|------------------|-----------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 15 minute summer | Roof3 | 11 | 6.244 | 0.236 | 9.6 | 0.2005 | 0.0000 | FLOOD RISK |
| 60 minute summer | EX_M2 | 51 | 5.714 | 0.028 | 1.3 | 0.0070 | 0.0000 | OK |
| 60 minute summer | Thames_SW | 51 | 5.629 | 0.027 | 1.3 | 0.0000 | 0.0000 | OK |
| 60 minute summer | GC_Out | 52 | 6.164 | 0.265 | 6.1 | 4.8016 | 0.0000 | FLOOD RISK |
| 60 minute summer | GC_2 | 44 | 6.102 | 0.287 | 1.2 | 0.6276 | 0.0000 | SURCHARGED |
| 60 minute summer | Roof 1 | 44 | 6.103 | 0.267 | 0.8 | 0.0435 | 0.0000 | SURCHARGED |
| 60 minute summer | Roof2 | 44 | 6.103 | 0.267 | 1.2 | 0.0485 | 0.0000 | SURCHARGED |

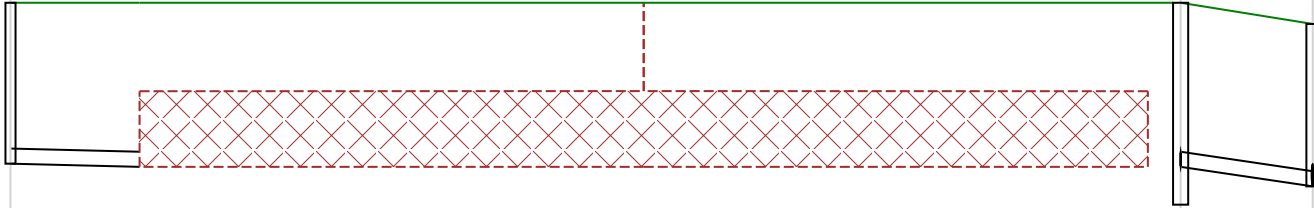
| Link Event (Upstream Depth) | US Node | Link | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m ³) | Discharge Vol (m ³) |
|-----------------------------|---------|--------------|-----------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute summer | Roof3 | 1.000 | GC_Out | 9.0 | 1.182 | 1.335 | 0.0684 | |
| 60 minute summer | EX_M2 | 1.002 | Thames_SW | 1.3 | 0.575 | 0.073 | 0.0190 | 8.6 |
| 60 minute summer | GC_Out | Orifice | EX_M2 | 0.8 | | | | |
| 60 minute summer | GC_Out | Infiltration | | 0.0 | | | | |
| 60 minute summer | GC_2 | Orifice | EX_M2 | 0.5 | | | | |
| 60 minute summer | GC_2 | Infiltration | | 0.0 | | | | |
| 60 minute summer | Roof 1 | 3.000 | GC_2 | 0.4 | 0.273 | 0.107 | 0.0348 | |
| 60 minute summer | Roof2 | 2.000 | GC_2 | 0.8 | 0.323 | 0.213 | 0.0401 | |

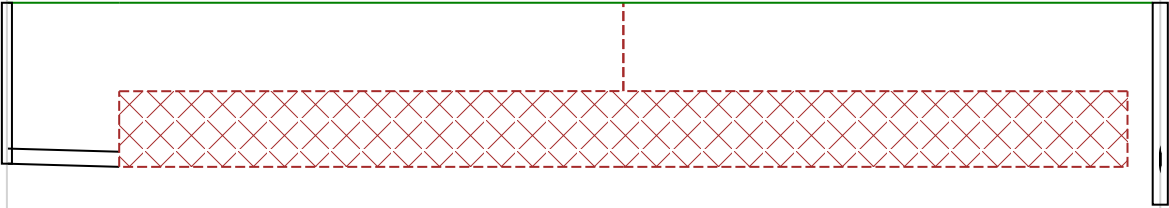
10.8.3 Drainage Sections

PDF to follow this page.

| Node Name | Roof3 | | GC_Out | EX_M2 |
|------------------|--|-------|--------|-------|
| A4 drawing |  | | | |
| Hor Scale 300 | | | | |
| Ver Scale 50 | | | | |
| Datum (m) 3.000 | | | | |
| Link Name | | | | |
| Section Type | 100mm | 150mm | | |
| Slope (1:X) | 80.0 | 84.6 | | |
| Cover Level (m) | 6.450 | | 6.450 | 6.760 |
| Invert Level (m) | 6.008 | 5.899 | 5.900 | 5.686 |
| Length (m) | 8.741 | | 18.110 | |

| Node Name | EX_M2 | Thames_SW |
|---|---|-----------|
| <p>A4 drawing</p> <p>Hor Scale 300</p> <p>Ver Scale 50</p> <p>Datum (m) 3.000</p> |  | |
| Link Name | 1.002 | |
| Section Type | 150mm | |
| Slope (1:X) | 100.9 | |
| Cover Level (m) | 6.760 | 6.700 |
| Invert Level (m) | 5.686 | 5.602 |
| Length (m) | 8.472 | |

| Node Name | Roof2 | | GC_2 | EX_M2 |
|--|--|------------------|-------|-------|
| A4 drawing Hor Scale 300 Ver Scale 50 Datum (m) 3.000 |  | | | |
| | Link Name | 2.000 | 2.001 | |
| | Section Type | 100mm | 100mm | |
| | Slope (1:X) | 243.8 | 40.6 | |
| | Cover Level (m) | 6.900 | 6.900 | 6.760 |
| Invert Level (m) | 5.836 5.815 | 5.815 5.686 | | |
| Length (m) | 5.120 | 5.238 | | |

| Node Name | Roof 1 | GC_2 |
|---|--|-------|
| <p>A4 drawing</p> <p>Hor Scale 300</p> <p>Ver Scale 50</p> <p>Datum (m) 3.000</p> |  | |
| Link Name | 3.000 | |
| Section Type | 100mm | |
| Slope (1:X) | 212.1 | |
| Cover Level (m) | 6.900 | 6.900 |
| Invert Level (m) | 5.836 | 5.815 |
| Length (m) | 4.454 | |

10.9 Appendix 8 – SuDS Maintenance Manual

All maintenance activities will be the responsibility of Jamie and Beverley McDaid. They will appoint a management company to undertake the general maintenance duties within the site and will join service agreements with the suppliers and manufactures of the SuDS/Pumps when required.

The information presented below is taken from the CIRIA SuDS Manual (Report c753) and [SuDS](#). Further details on installation and maintenance can be found detailed below and online.

10.9.1 Geo-Cellular Maintenance

| Maintenance Schedule | Required Action | Typical Frequency | Responsibility |
|-------------------------------|---|---|--|
| Regular maintenance | Inspect for sediment and debris in pre-treatment components and floor of inspection tube or chamber and inside of concrete manhole rings. | Annually. | will be responsible for setting up the management company. |
| | Cleaning of gutters and any filters on downpipes. | Annually (or as required based on inspections). | |
| | Trimming any roots that may be causing blockages. | Annually (or as required). | |
| Occasional maintenance | Remove sediment and debris from manhole, storage structure and components and floor of inspection tube or chamber and inside of concrete manhole rings. | As required, based on inspections. | |
| Remedial actions | Reconstruct geocellular and/or replace or clean void fill, if performance failure occurs | As required | will be responsible for setting up the management company. |
| | Replacement of clogged geotextile (will require reconstruction of soakaway). | As required. | |
| Monitoring | Inspect silt raps and note rate of sediment accumulation. | Monthly in the first year and then annually. | |
| | Check soakaway to ensure emptying is occurring. | Annually. | |

Maintenance will usually be carried out manually, although a suction tanker can be used for sediment / debris removal for large systems. If maintenance is not undertaken for long periods, deposits can become hard-packed and require considerable effort to remove.

Replacement of the geocellular units will be necessary if the system becomes blocked with silt. Effective monitoring will give information on changes in infiltration rate and provide a warning of potential failure in the long term.

Areas draining to infiltration components should be regularly swept to prevent silt being washed off the surface. This will minimize the need for maintenance.

Maintenance responsibility should be placed with an appropriate organisation, and maintenance schedules should be developed during the design phase.

10.9.2 SuDS Planters Maintenance

| Maintenance Schedule | Required Action | Typical Frequency | Responsibility |
|----------------------|--|--|--|
| Regular maintenance | Inspect for sediment and debris in inlet and outlet components | Quarterly; As required. | CompanyName will be responsible for setting up the management company. |
| | Inspection & Cleaning of gutters and any filters on downpipes feeding into rain gardens as required. | Quarterly; As required. | |
| | Remove, replace and maintain vegetation as required; Ensuring cuttings are removed to prevent debris build up; Weeding of flower bed to maintain the desired vegetation, density and biodiversity - Vegetation management | Monthly inspections during Spring / Summer Autumn / Winter - As required. | |
| Remedial actions | Replace dead vegetation as required. Cut back vegetation as required. | As required. | |
| Monitoring | Inspect silt traps / discharge points and note rate of sediment accumulation and ensure no erosion pathways forming. | Monthly in the first year and then annually. | |
| | Check Planters are emptying as required following a storm event occurring. | After storms; When possible. | |

Maintenance will be carried out manually. All monitoring and maintenance will be carried out by the appointed estate management company that undertakes the general landscaping maintenance.

10.9.3 SuDS Rain Water Butt Maintenance

| Maintenance Schedule | Required Action | Typical Frequency | Responsibility |
|----------------------|---|---|--|
| Regular maintenance | Inspect for sediment and debris in inlet and outlet components; | Quarterly; As required. Increase freq. to Monthly during Autumn; | will be responsible for setting up the management company. |
| | Inspection & Cleaning of gutters and any filters on downpipes feeding into the Rain Water Butts. | Quarterly; Increase freq. to Monthly during Autumn; | |
| Remedial actions | Cleaning of the water butt. Fully drain the water butt and clear out debris and enable access; Scrub out the inside of the butt or tank with a coarse brush, if accessible, using a proprietary cleaning product such as Just Water Butt Cleaner or garden disinfectant; Rinse with clean water; Cleaning of Gutters; Clean or fit a new filter; | Annually; Or as required. | |
| Remedial actions | Use water/empty water butts - to clean, water plants (inside & out); Empty water Butt more frequently during the winter, to allow for storage during storms and to keep the water fresh; | Once every two weeks; as required | |

Maintenance will be carried out manually. All monitoring and maintenance will be carried out by the appointed estate management company that undertakes the general landscaping maintenance.

10.9.4 Flow Control Maintenance

| Maintenance Schedule | Required Action | Typical Frequency | Responsibility |
|----------------------|---|--|--|
| Regular maintenance | Inspect for sediment and debris; | Quarterly; As required. | will be responsible for setting up the management company. |
| | Inspection & Cleaning of SuDS components upstream of flow control element. | Quarterly; Increase freq. to Monthly during Autumn; | |
| Remedial actions | Removal of debris and sediment; | Annually; Or as required. | |
| Remedial actions | Replacement of parts; Manhole cover, filters or components of flow control device; | As required; | |
| Monitoring | Ensure flow control device is function correctly during and after storm events; Check water levels up stream and downstream of flow control device | Monthly; During 1 st year of installation or during and after storm event; When possible Reduce to Quarterly following the 1 st year; | |
| | Check for damage to flow control components | Annually; | |
| | Check for securely fitting manhole lid; Ensures debris cannot enter the system unfiltered; | Annually; | |